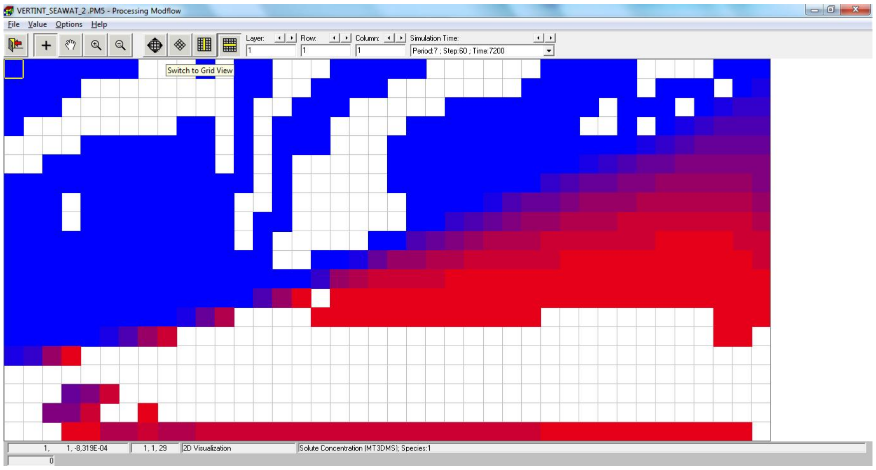
ULTIMATE



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Column: 1

Simulation Time: Period:7 ; Step:60 ; Time:7200

1, 1, -8,319E-04

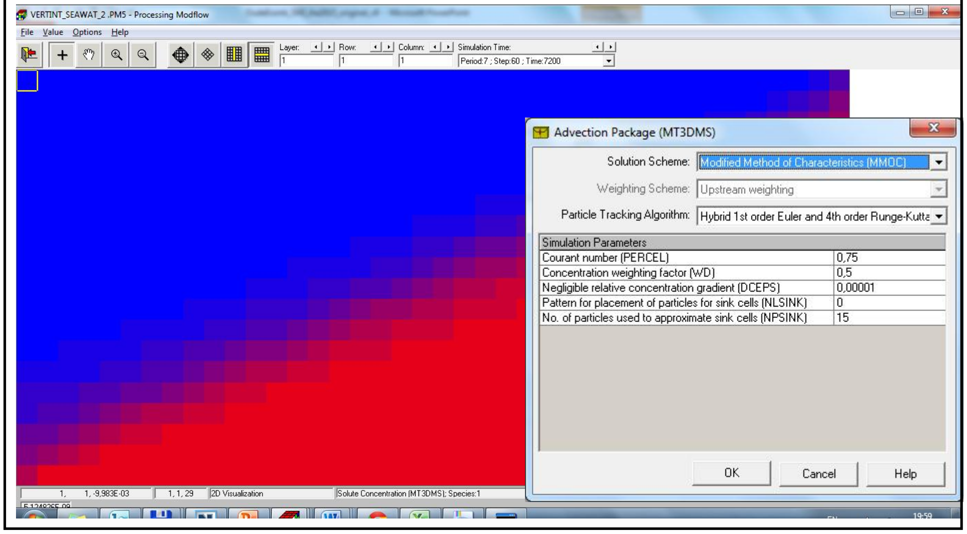
1, 1, 29

2D Visualization

Solute Concentration (MT3DMS); Species:1

0

MMOC, NPLANE=0



Layer: 1

Row: 1

Column: 1

Simulation Time: Period:7 ; Step:60 ; Time:7200

Advection Package (MT3DMS)

Solution Scheme: Modified Method of Characteristics (MMOC)

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for placement of particles for sink cells (NLSINK)	0
No. of particles used to approximate sink cells (NPSINK)	15

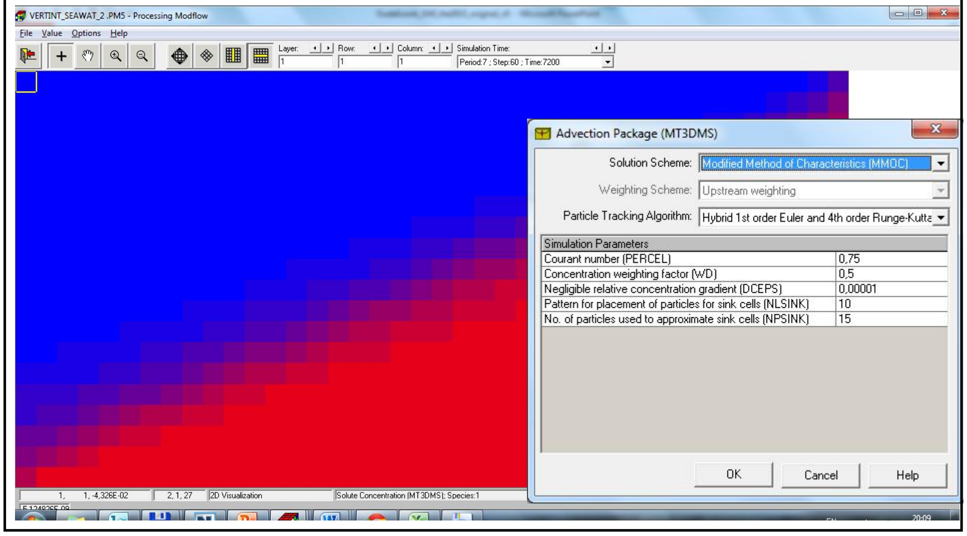
1, 1, -9,983E-03

1, 1, 29

2D Visualization

Solute Concentration (MT3DMS); Species:1

MMOC, NPLANE=10



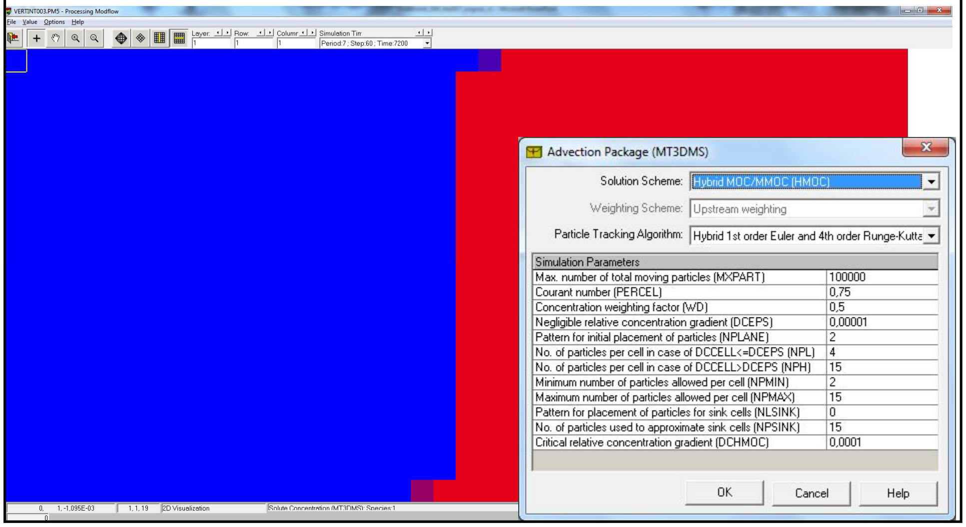
Solution Scheme: Modified Method of Characteristics (MMOC)

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for placement of particles for sink cells (NLSINK)	10
No. of particles used to approximate sink cells (NPSINK)	15

HMOC



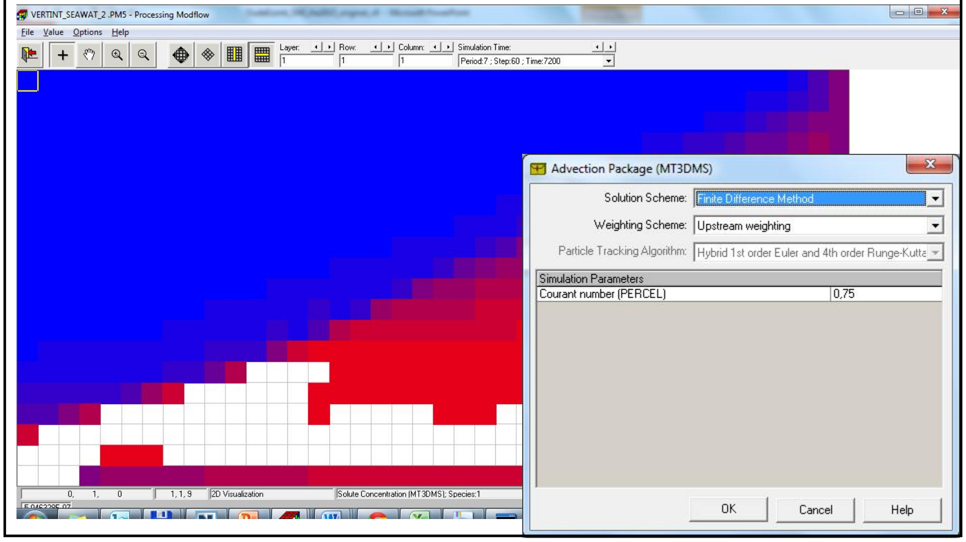
Solution Scheme: Hybrid MOC/MMOC (HMOC)

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Max. number of total moving particles (MXPART)	100000
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for initial placement of particles (NPLANE)	2
No. of particles per cell in case of DCCELL<=DCEPS (NPL)	4
No. of particles per cell in case of DCCELL>DCEPS (NPH)	15
Minimum number of particles allowed per cell (NPMIN)	2
Maximum number of particles allowed per cell (NPMAX)	15
Pattern for placement of particles for sink cells (NLSINK)	0
No. of particles used to approximate sink cells (NPSINK)	15
Critical relative concentration gradient (DCHMOC)	0,0001

Finite Difference Method



Advection Package (MT3DMS)

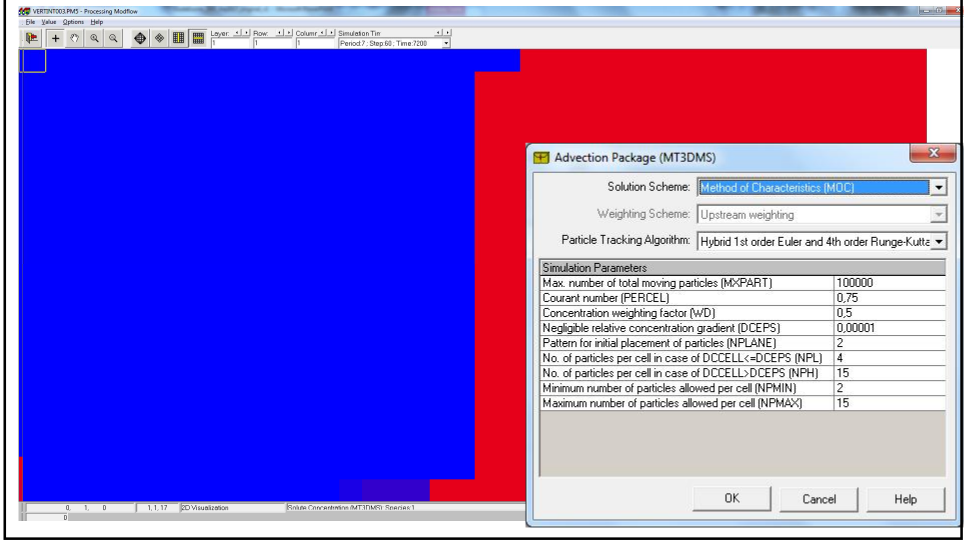
Solution Scheme: Finite Difference Method

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Courant number (PERCEL)	0,75

MOC



Advection Package (MT3DMS)

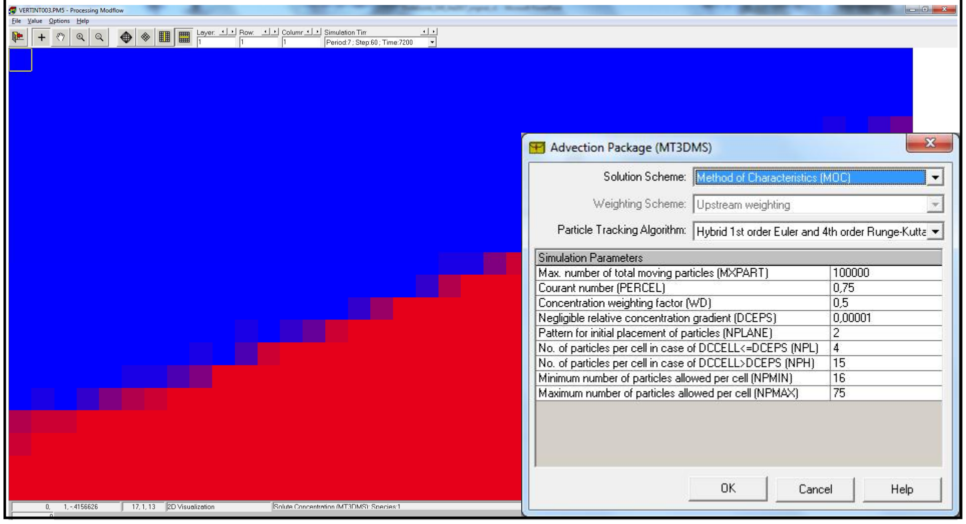
Solution Scheme: Method of Characteristics (MOC)

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Max. number of total moving particles (MXPART)	100000
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for initial placement of particles (NPLANE)	2
No. of particles per cell in case of DCCELL<=DCEPS (NPL)	4
No. of particles per cell in case of DCCELL>DCEPS (NPH)	15
Minimum number of particles allowed per cell (NPMIN)	2
Maximum number of particles allowed per cell (NPMAX)	15

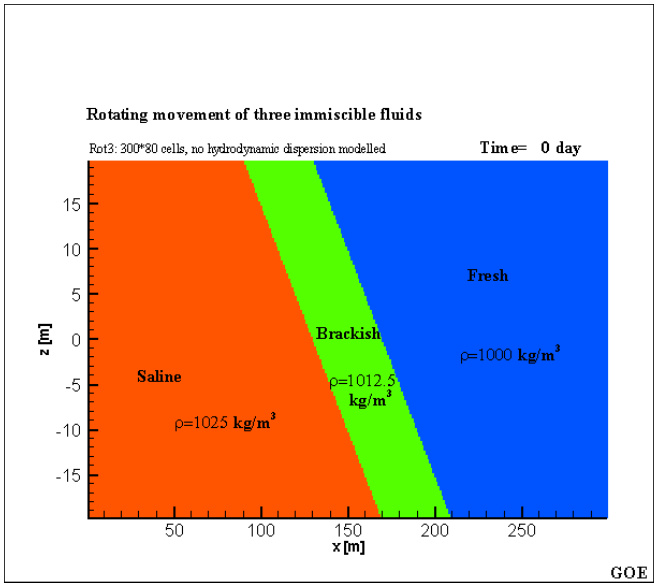
MOC



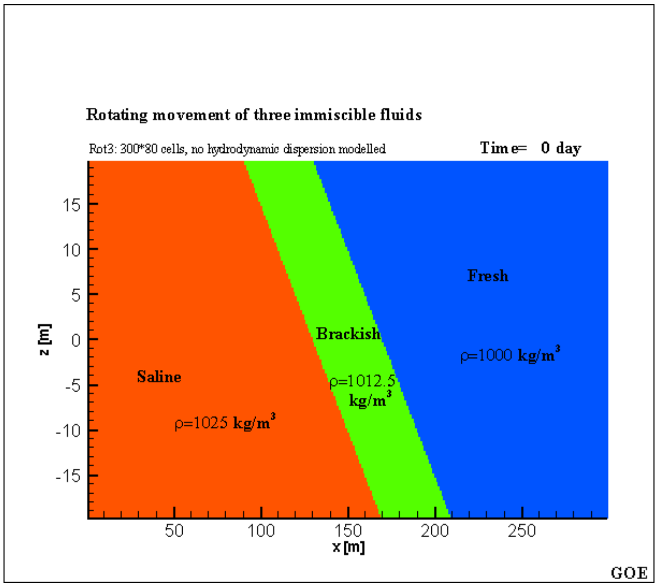
Solution Scheme: Method of Characteristics (MOC)
Weighting Scheme: Upstream weighting
Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Max. number of total moving particles (MXPART)	100000
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for initial placement of particles (NPLANE)	2
No. of particles per cell in case of DCCELL<=DCEPS (NPL)	4
No. of particles per cell in case of DCCELL>DCEPS (NPH)	15
Minimum number of particles allowed per cell (NPMIN)	16
Maximum number of particles allowed per cell (NPMAX)	75

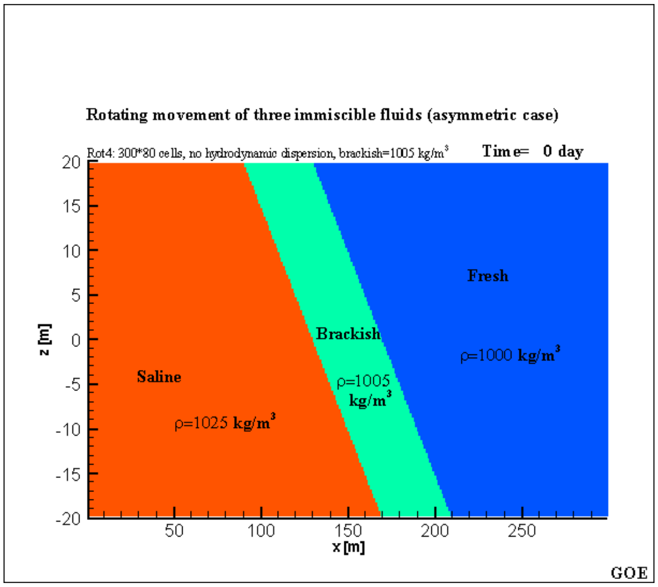
Rotating immiscible interfaces



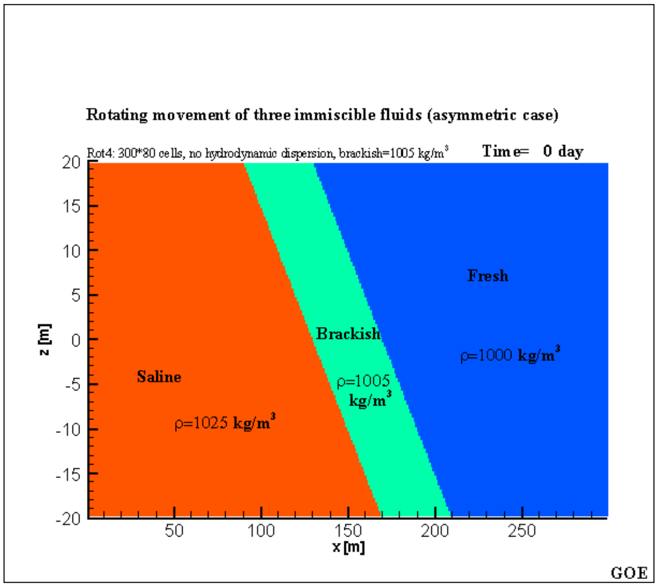
Rotating immiscible interfaces



Rotating immiscible interfaces (asymmetric)

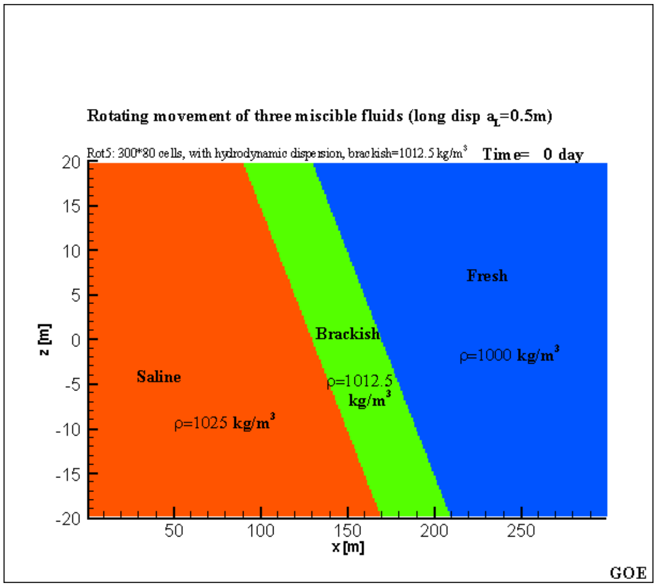


Rotating immiscible interfaces (asymmetric)

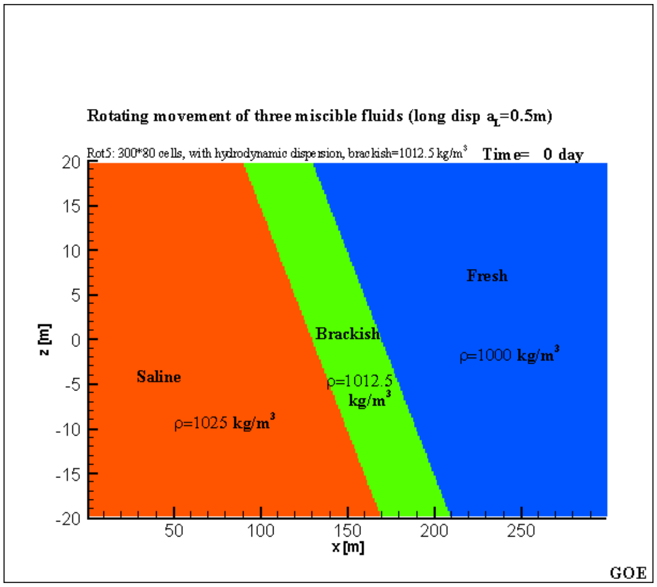


Bakker, M., Oude Essink, G.H.P. & Langevin, C. 2004. The rotating movement of three immiscible fluids, J. of Hydrology 287, 270-278

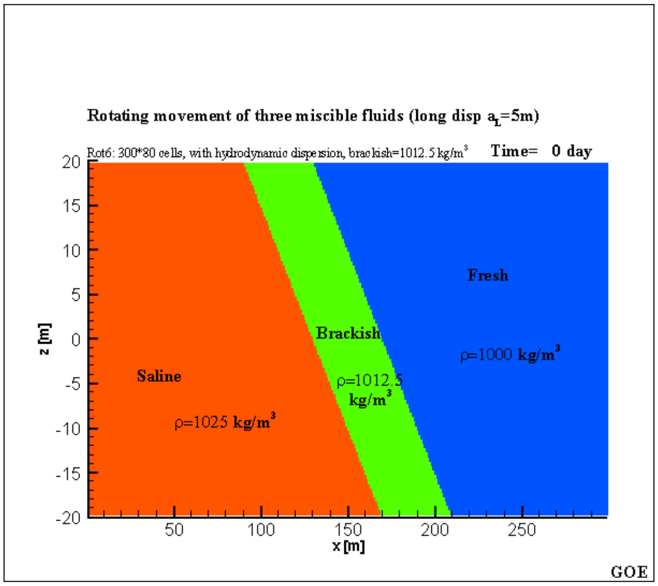
Rotating interfaces with dispersion α_L=0.5m



Rotating interfaces with dispersion α_L=0.5m

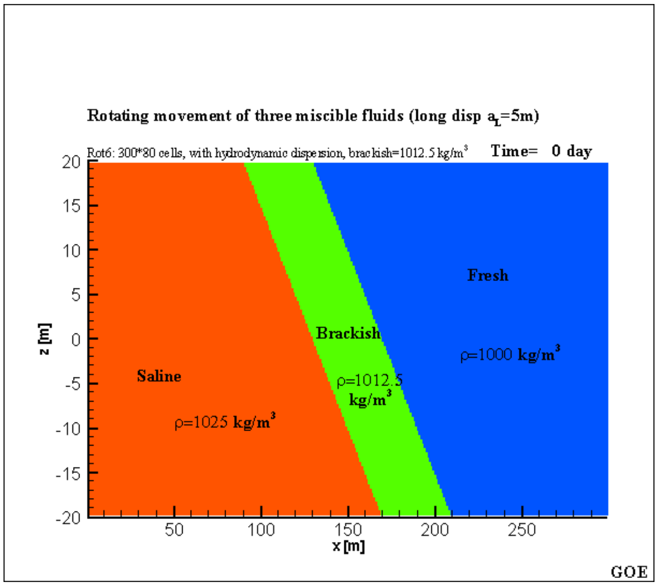


Rotating interfaces with dispersion α_L=5m



cases

Rotating interfaces with dispersion α_L=5m



Salt water pocket in a fresh environment

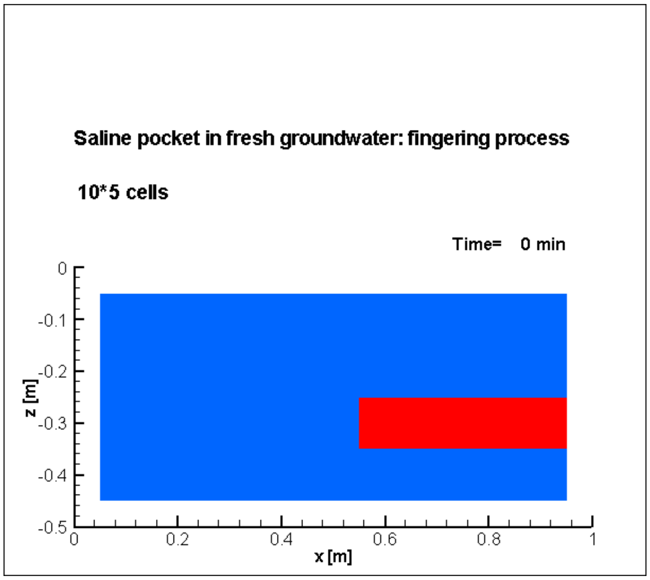
Grid convergence

Time step

cases

Salt water pocket in a fresh environment (I)

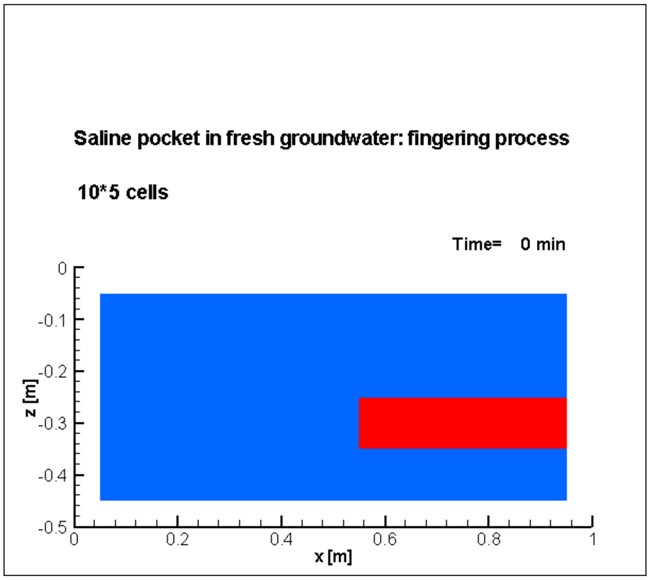
Effect of discretisation on a 'salt lake problem'



cases

Salt water pocket in a fresh environment (I)

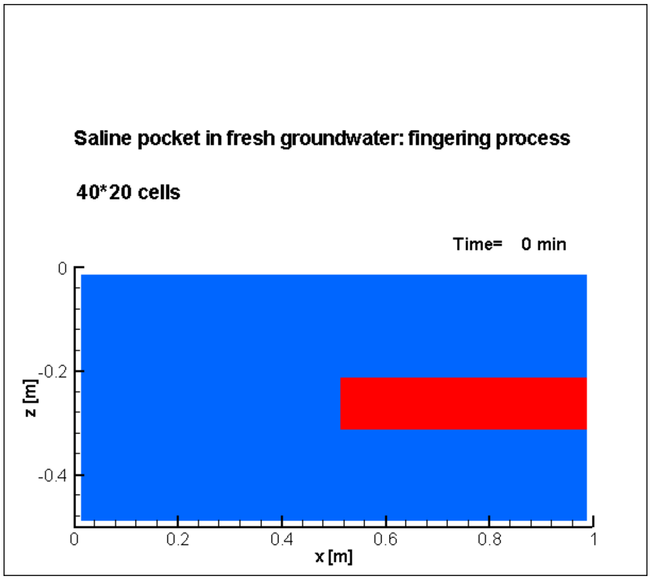
Effect of discretisation on a 'salt lake problem'



cases

Salt water pocket in a fresh environment (II)

Effect of discretisation



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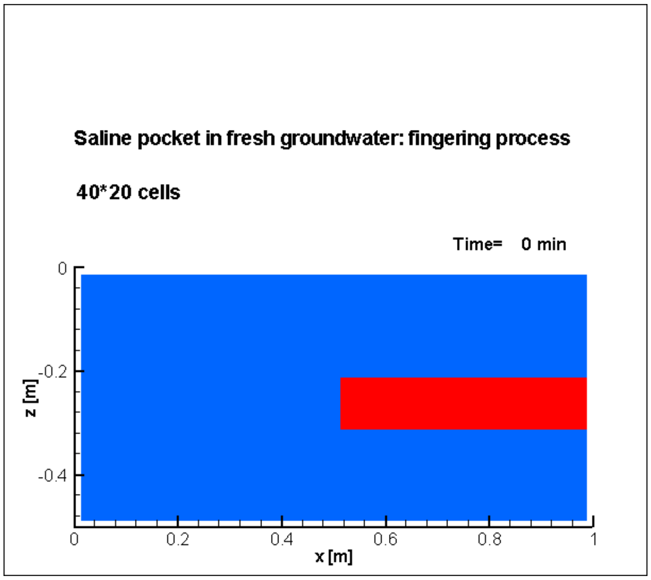
cases

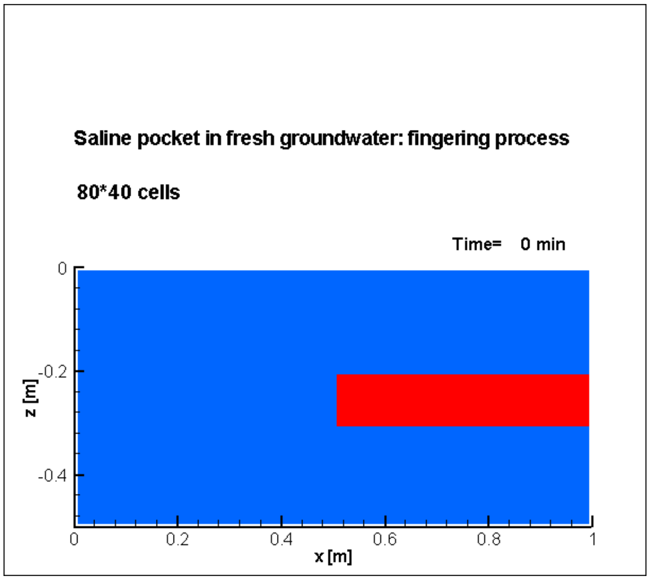
Salt water pocket in a fresh environment (II)

Effect of discretisation



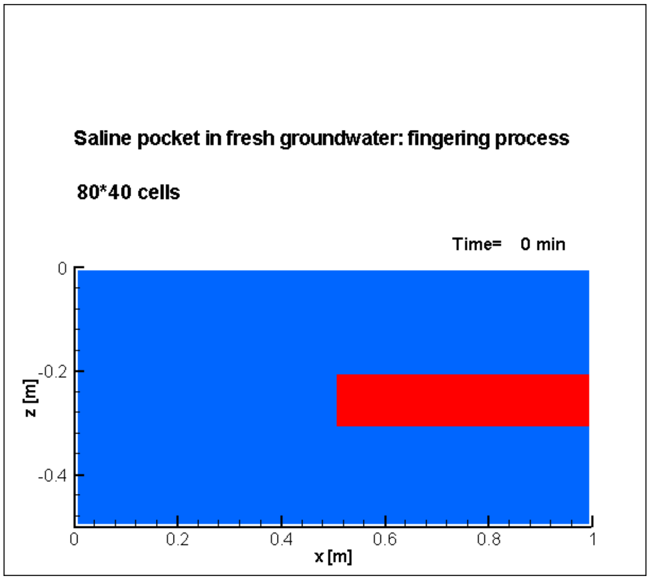
Salt water pocket in a fresh environment (III)

Effect of discretisation



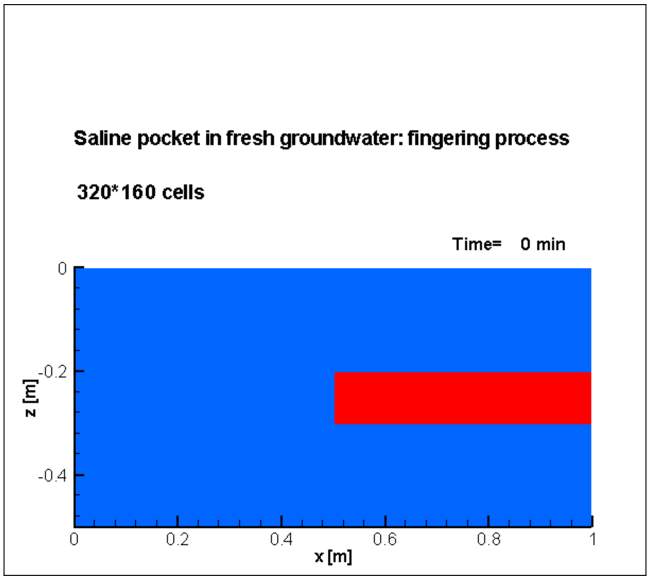
Salt water pocket in a fresh environment (III)

Effect of discretisation



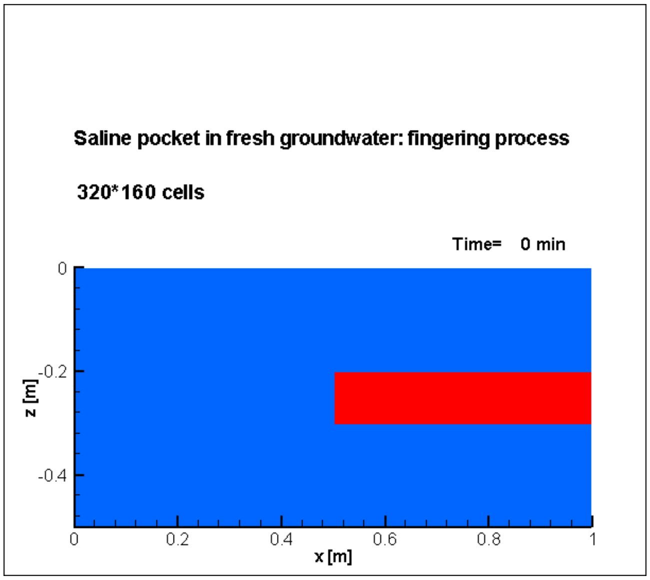
Salt water pocket in a fresh environment (IV)

Effect of discretisation



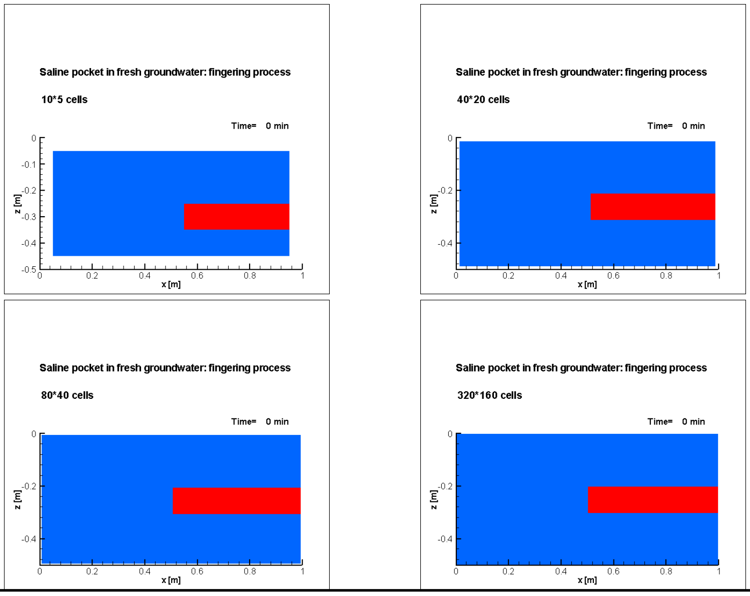
Salt water pocket in a fresh environment (IV)

Effect of discretisation

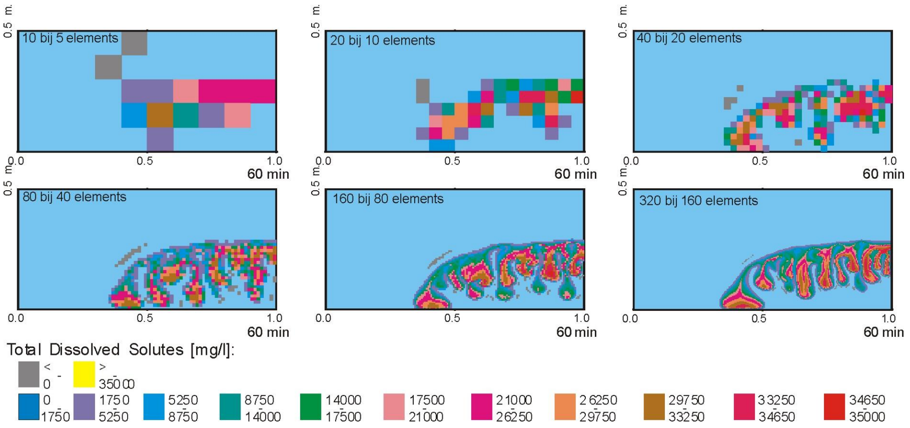


Salt water pocket in a fresh environment (V)

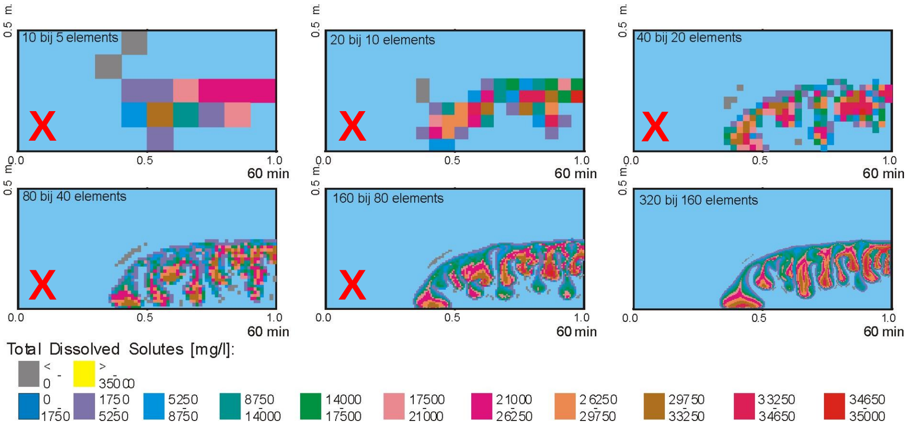
Effect of discretisation



Effect of size model cell on physical process



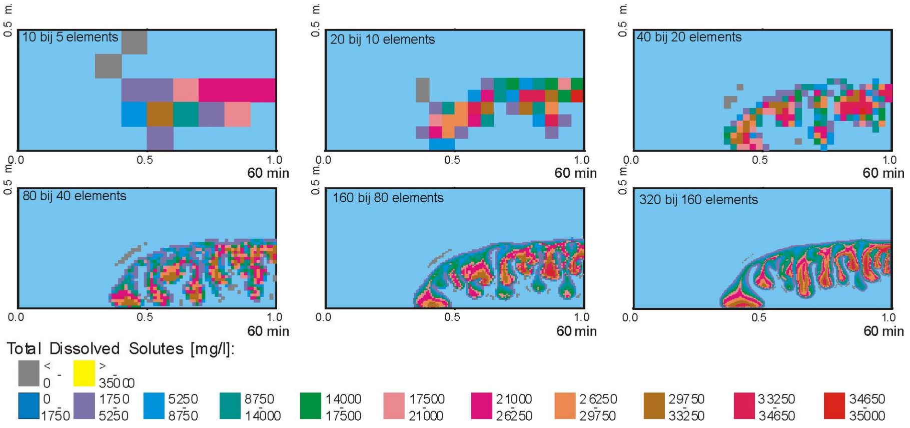
Effect of size model cell on physical process



X= LOUSY models for predicting exact number of salt water fingers

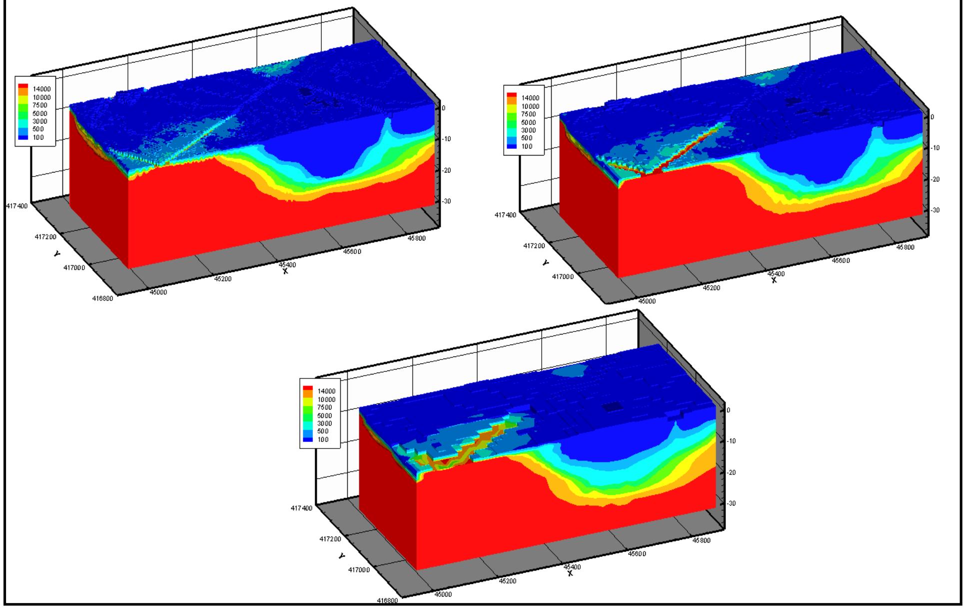
---

Effect of size model cell on physical process

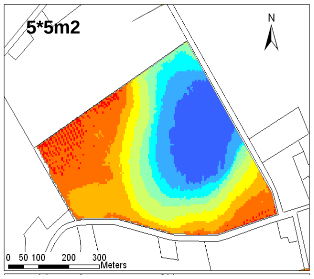


BUT: all models are GOOD for predicting moment of touching bottom!

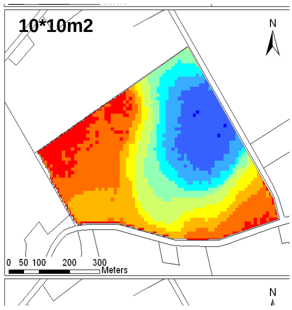
Different model scales: 5, 10, 25m2

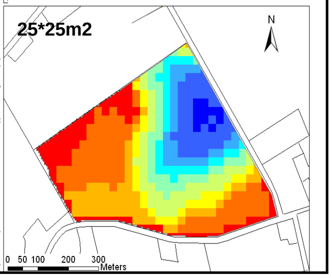


Different model scales

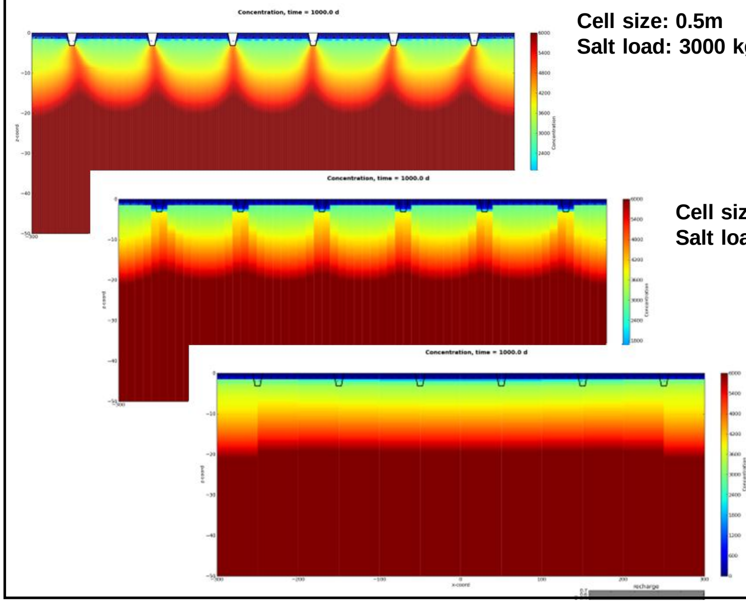


Which one is good enough?





Upscaling issues: upconing under ditch



Cell size: 0.5m
Salt load: 3000 kg/d

Cell size: 10m
Salt load: 1750 kg/d

Cel size: 50m
Salt load: 2000 kg/d

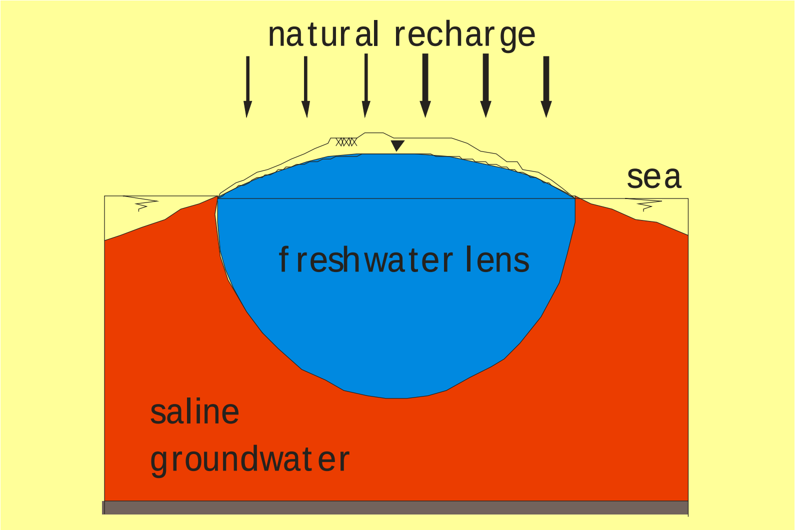
α_L=0.01m

Salt water pocket in a fresh environment (VI)

Conclusion:

- For some physical processes, a large number of cells is necessary
- Check always grid convergence!

Evolution of a freshwater lens



Question:

How long does it take before the volume of a freshwater lens is filled?:

a. 5 years
b. 25 years
c. 100 years
d. 500 years

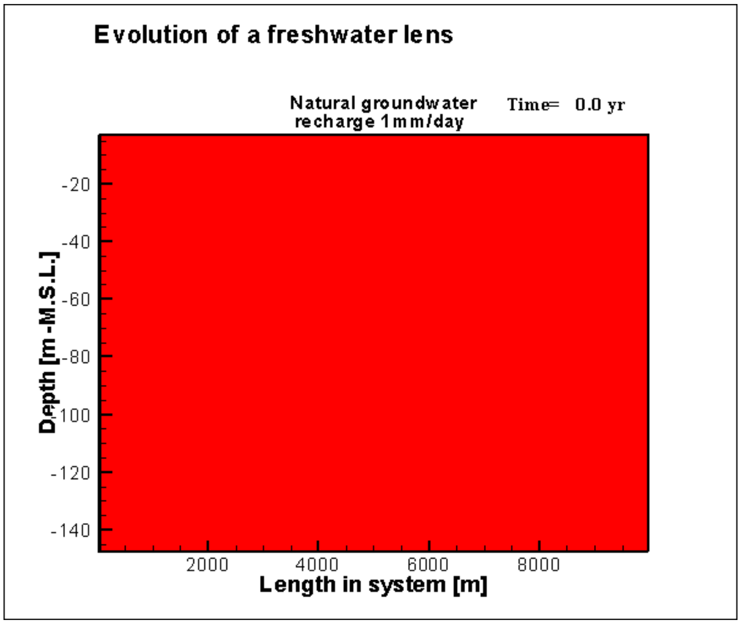
T = **specific time scale**

T = **time period before the lens has reached 95% of its final form**

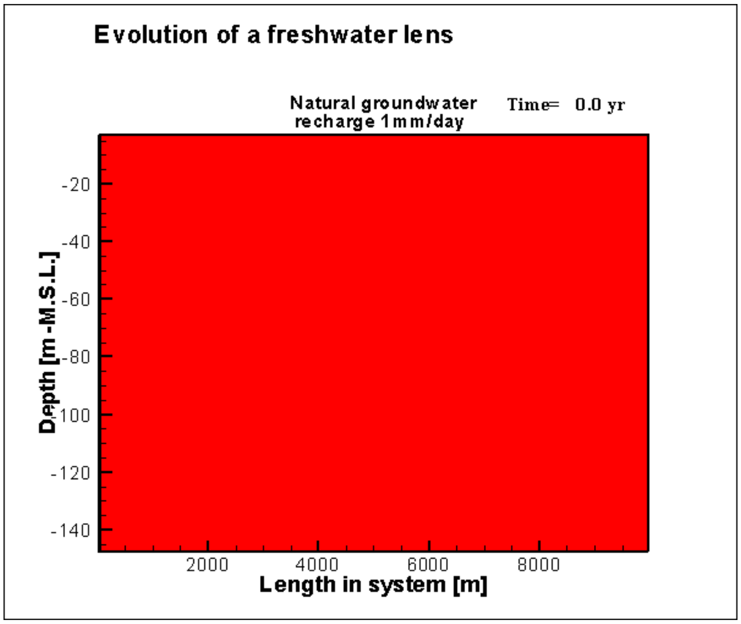
In the Netherlands: T = 75-200 jaar,

depends on:
- width dune area
- natural groundwater recharge
- hydraulic conductivity soil

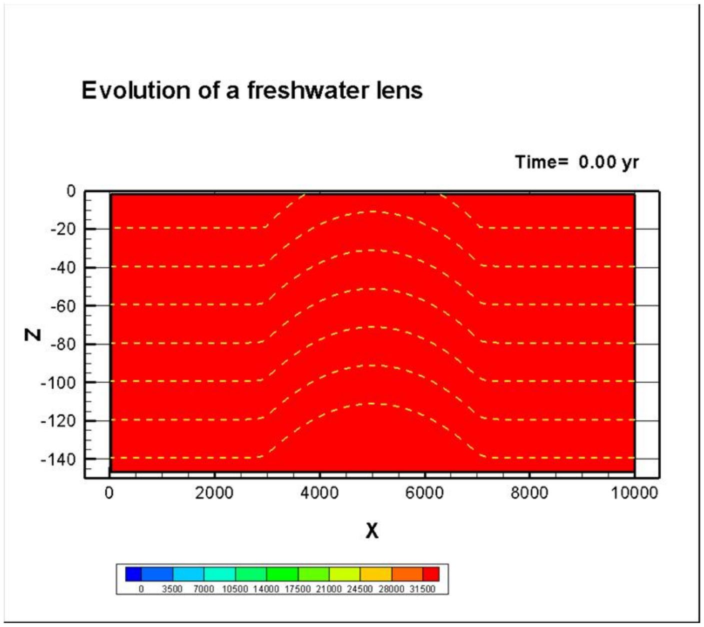
Concept: evolution freshwater lens (not Griend!)



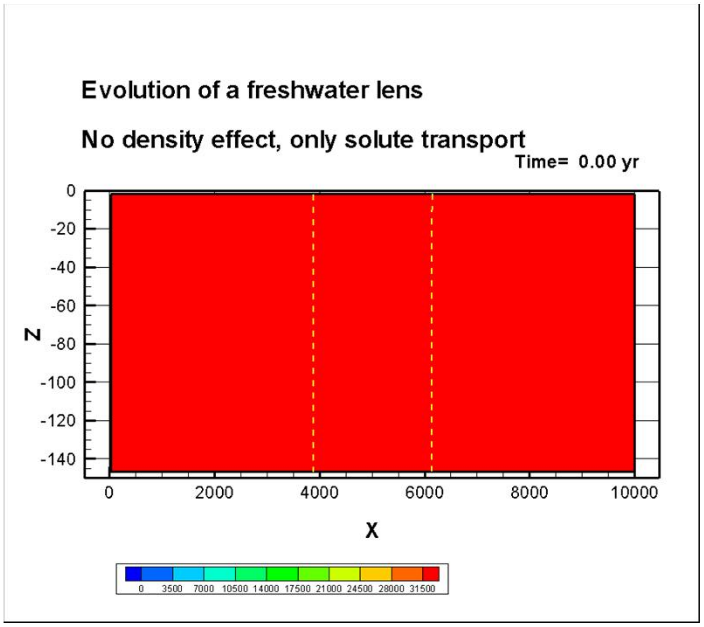
Concept: evolution freshwater lens (not Griend!)



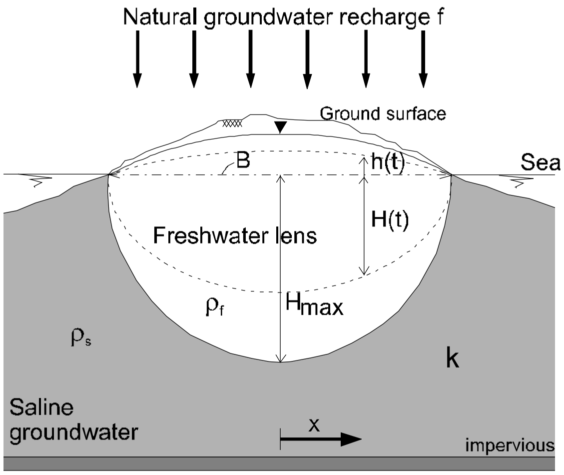
Evolution freshwater lens



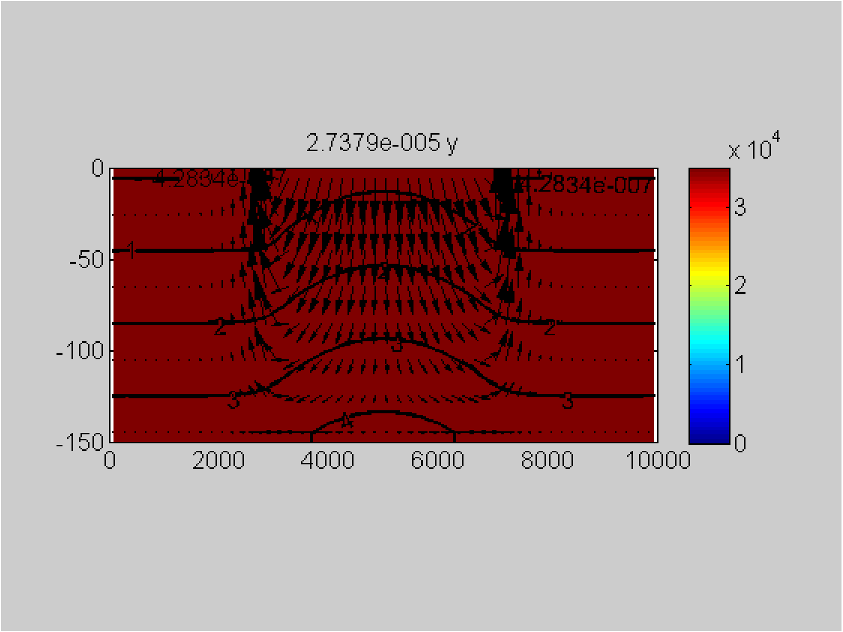
Evolution freshwater lens: no density effects



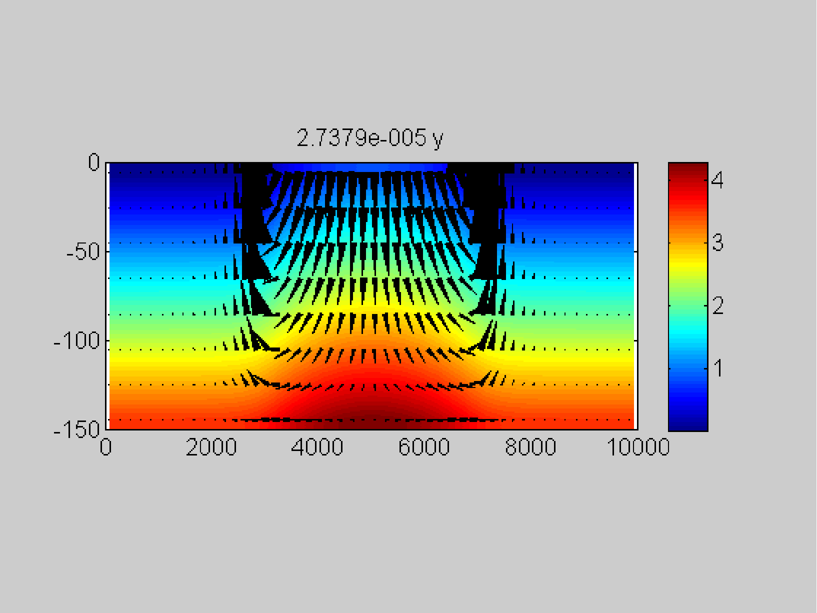
Case 2: Development of a freshwater lens



Evolution lens



Evolution freshwater head

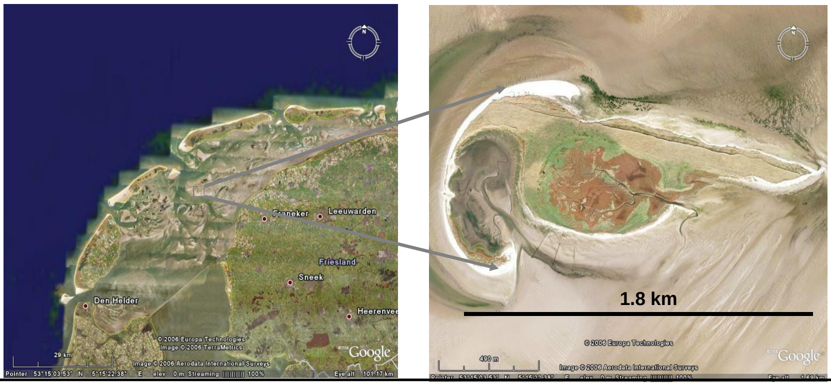


Evolution freshwater head

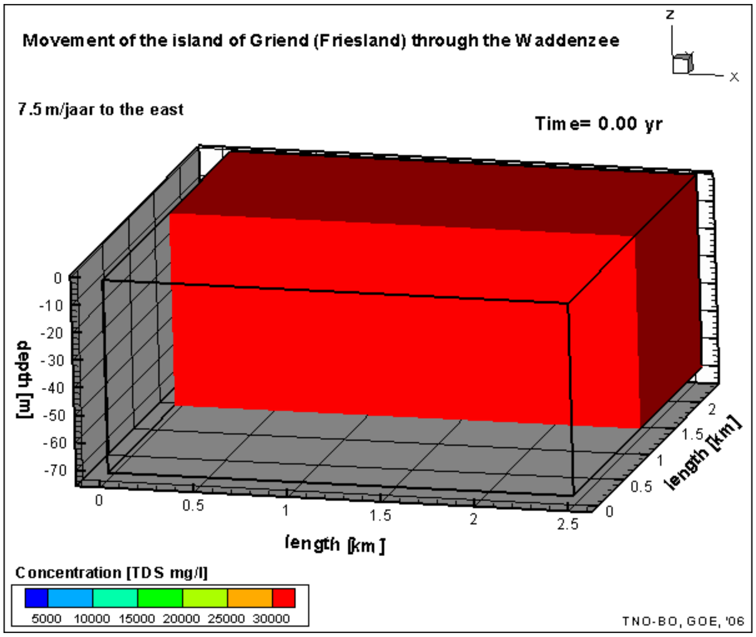
The island of Griend

Issues:

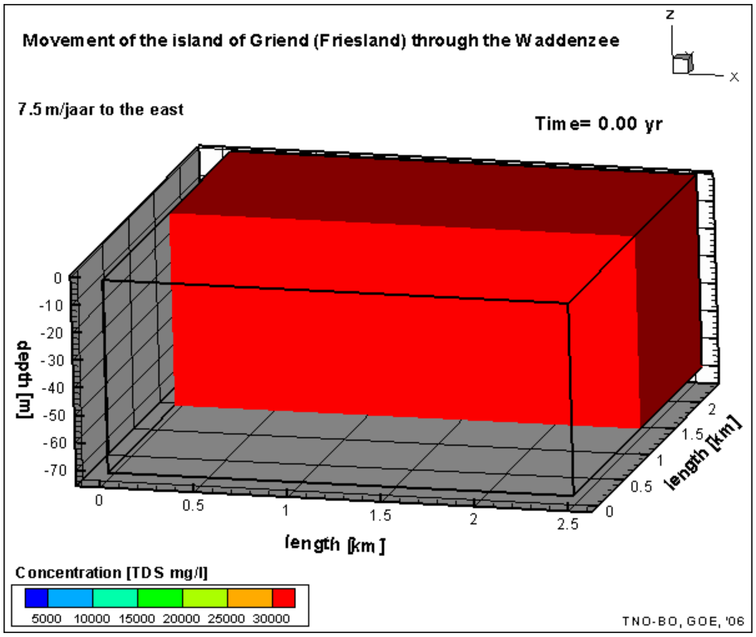
1. Small island moves ~7.5m per year to the east
2. Effect on the volume of the freshwater lens:
   - Can a lens be developed?
   - What is the thickness of the lens?



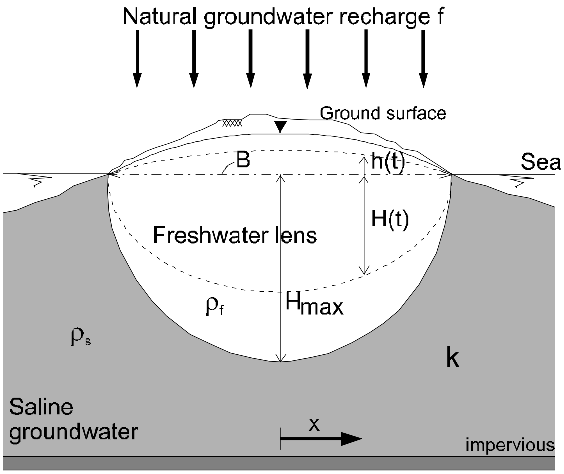
Movement of De Griend and creation of the lens



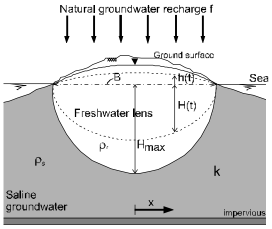
Movement of De Griend and creation of the lens



Case 2: Development of a freshwater lens

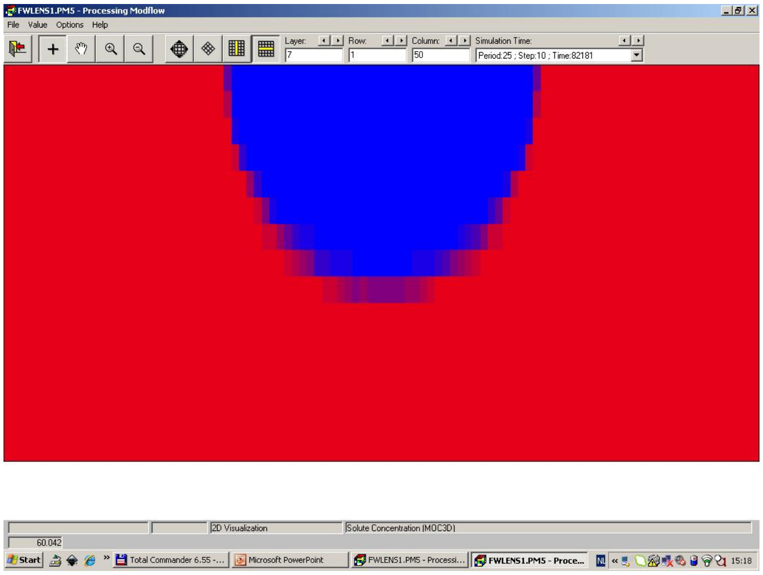


Case 2: Development of a freshwater lens



Parameters			
Layers	15	K_{hor}	20 m/d
Rows	1	T	200 m/d
Columns	100	Anisotropy K_{hor}/K_{ver}	10
Δx	100 m	ne	0.35
Δy	10 m	αL	0 m
Δz	10 m	αT	0 m
Stress periods	10	recharge	360 mm/y
Initial concentration	35000 mg/l	Recharge concentration	0 mg/l
bouyancy	0.025		

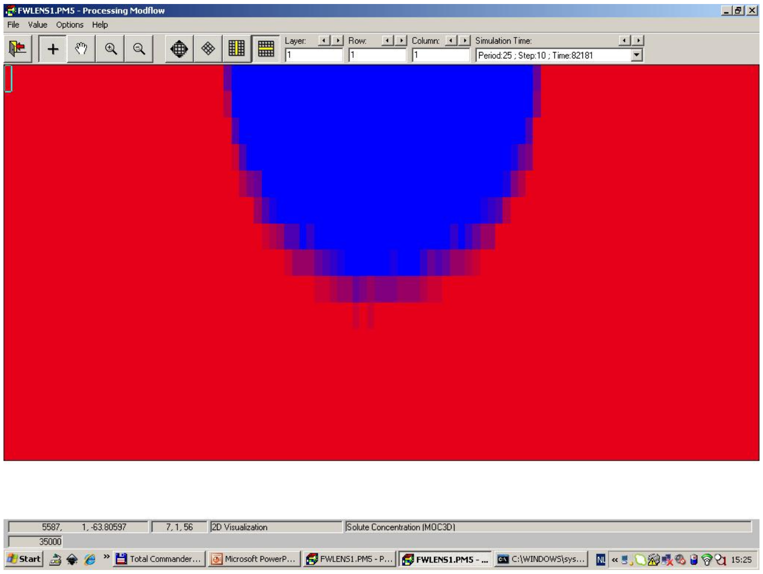
MOCDENS3D, no disp, 16part


FWLENS1.PM5 - Processing Modflow

Layer: 7
Row: 1
Column: 50
Simulation Time: Period:25 ; Step:10 ; Time:82181

2D Visualization
Solute Concentration (MOC3D)
60.042

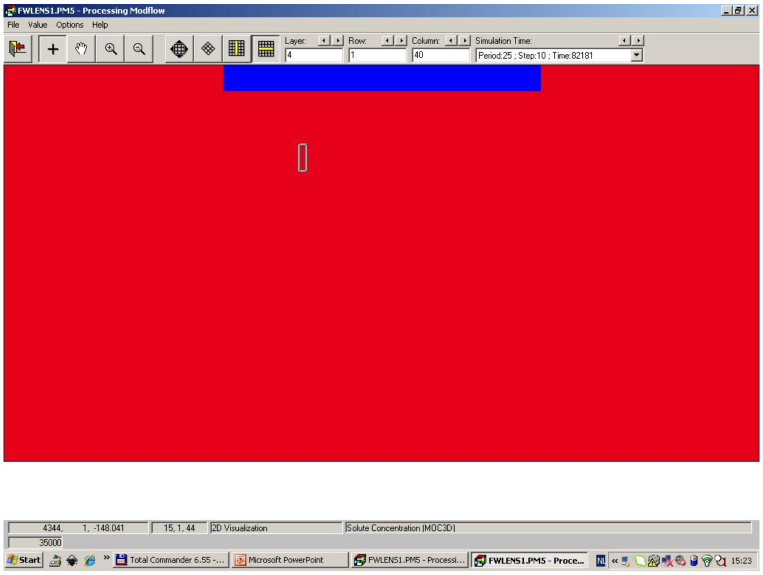
MOCDENS3D, no disp, 4part



Layer: 1
Row: 1
Column: 1
Simulation Time: Period:25 ; Step:10 ; Time:82181

5587, 1, -63.80597 | 7, 1, 56 | 2D Visualization | Solute Concentration (MOC3D)
35000

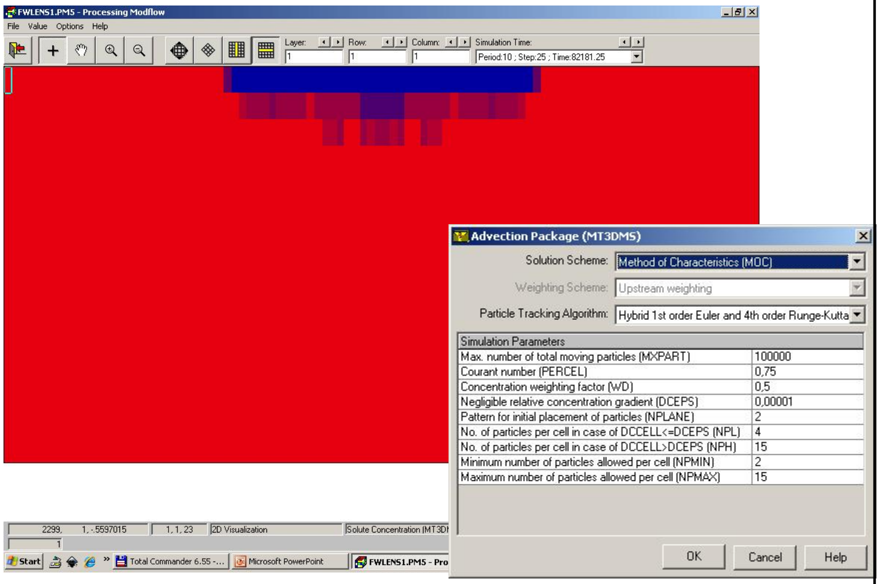
MOCDENS3D, no disp, 1part



Layer: 4
Row: 1
Column: 40
Simulation Time: Period:25 ; Step:10 ; Time:82181

4344, 1, -148.041 | 15, 1, 44 | 2D Visualization | Solute Concentration (MOC3D)
35000

SEAWAT, MOC, NPLANE=2



Advection Package (MT3DMS)

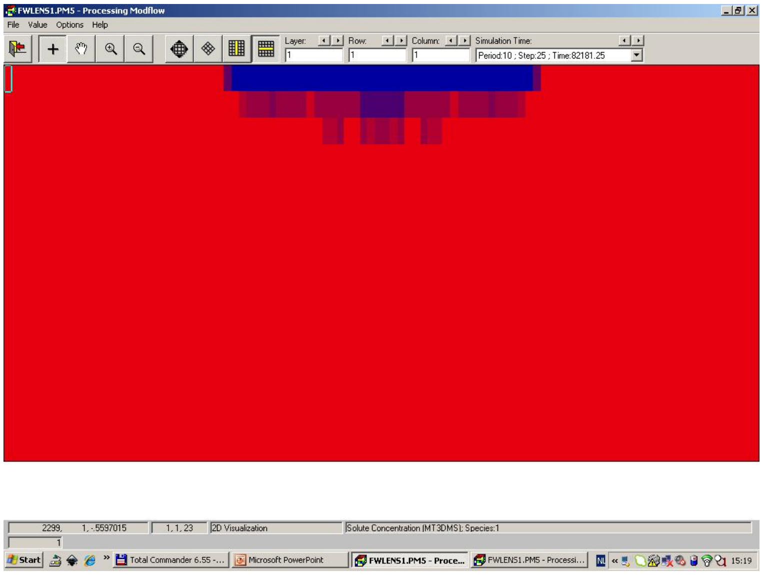
Solution Scheme: Method of Characteristics (MOC)

Weighting Scheme: Upstream weighting

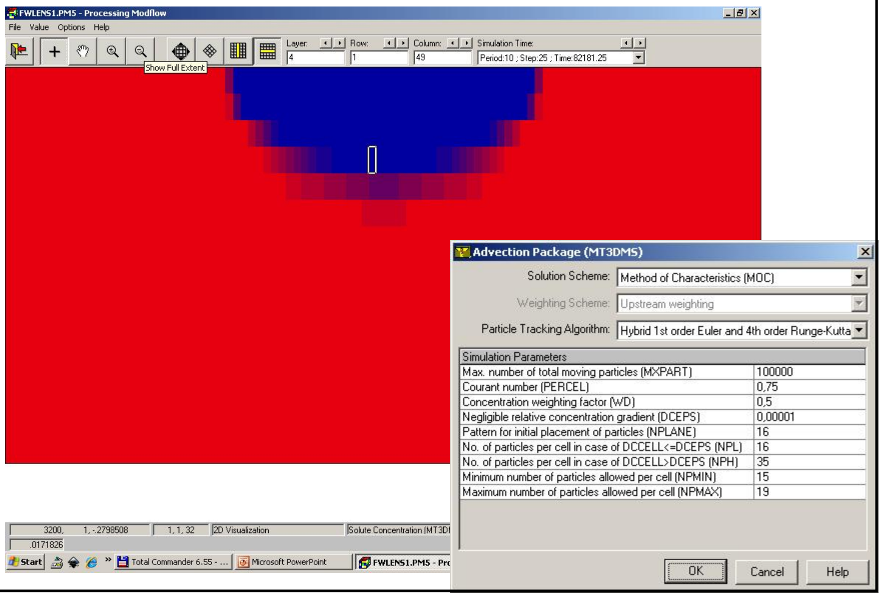
Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Max. number of total moving particles (MXPART)	100000
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for initial placement of particles (NPLANE)	2
No. of particles per cell in case of DCCELL<=DCEPS (NPL)	4
No. of particles per cell in case of DCCELL>DCEPS (NPH)	15
Minimum number of particles allowed per cell (NPMIN)	2
Maximum number of particles allowed per cell (NPMAX)	15

SEAWAT, MOC, 4.NPLANE=16



SEAWAT, MOC, 20sec, NPLANE=16, etc.



Advection Package (MT3DMS)

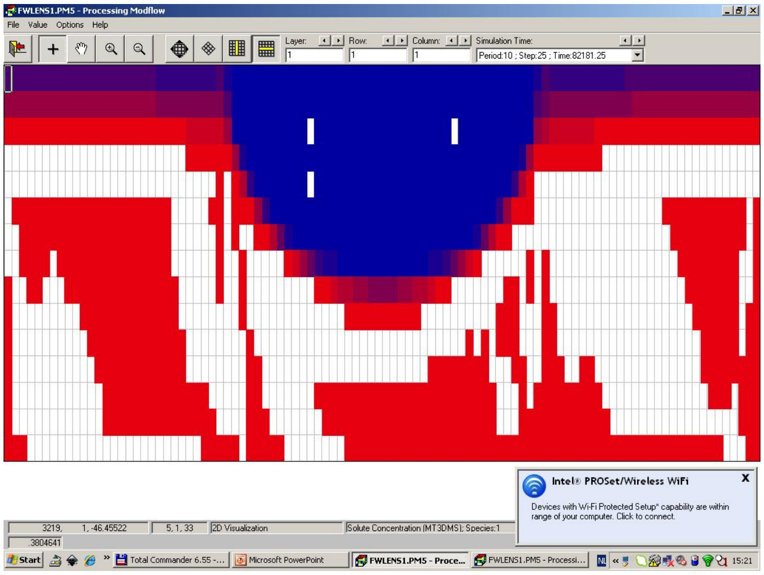
Solution Scheme: Method of Characteristics (MOC)

Weighting Scheme: Upstream weighting

Particle Tracking Algorithm: Hybrid 1st order Euler and 4th order Runge-Kutta

Simulation Parameters	
Max. number of total moving particles (MXPART)	100000
Courant number (PERCEL)	0,75
Concentration weighting factor (WD)	0,5
Negligible relative concentration gradient (DCEPS)	0,00001
Pattern for initial placement of particles (NPLANE)	16
No. of particles per cell in case of DCCELL<=DCEPS (NPL)	16
No. of particles per cell in case of DCCELL>DCEPS (NPH)	35
Minimum number of particles allowed per cell (NPMIN)	15
Maximum number of particles allowed per cell (NPMAX)	19

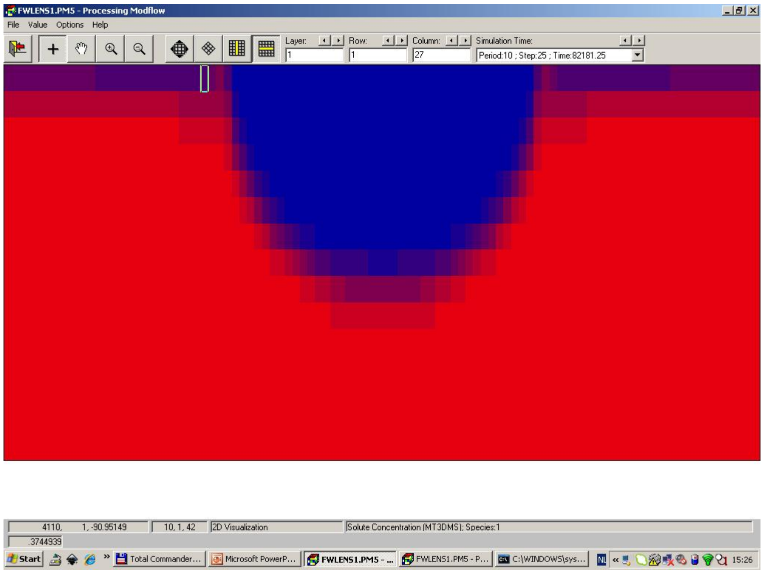
SEAWAT, ULTIMATE, 16.56sec



Intel® PROSet/Wireless WiFi

Devices with Wi-Fi Protected Setup* capability are within range of your computer. Click to connect.

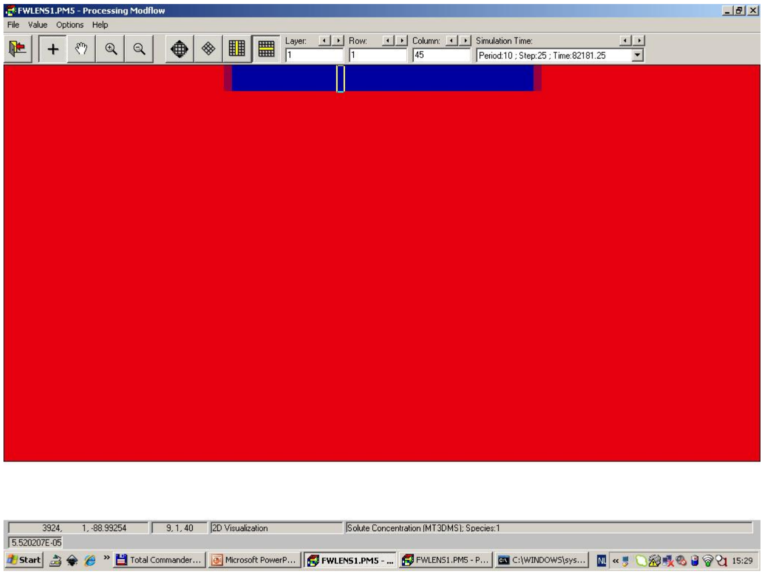
SEAWAT, MMOC, 8.5sec



Layer: 1
Row: 1
Column: 27
Simulation Time: Period:10 ; Step:25 ; Time:82181.25

4110, 1, -90.95149
10, 1, 42
2D Visualization
Solute Concentration (MT3DMS); Species:1
.3744939

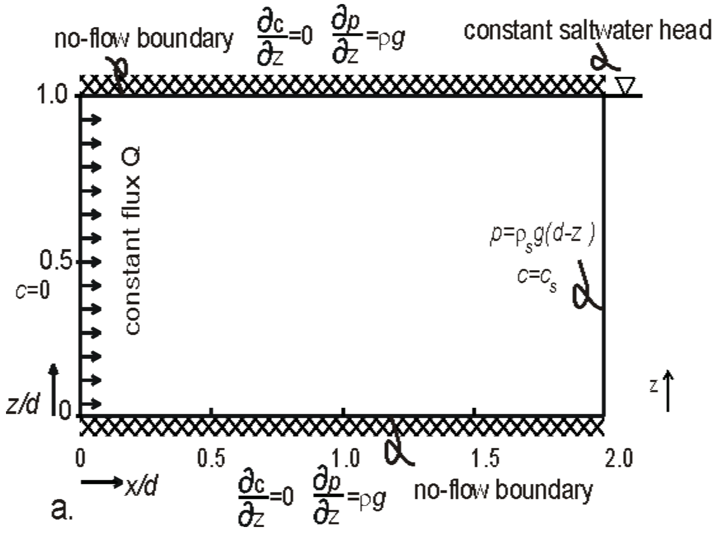
SEAWAT, HMOC, 6.8sec



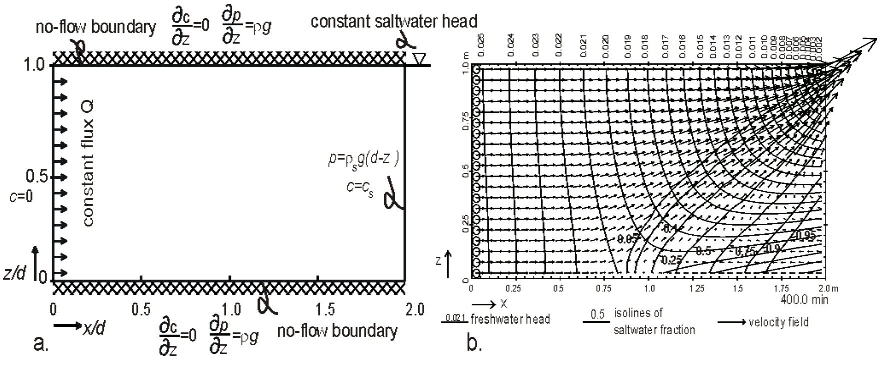
Layer: 1
Row: 1
Column: 45
Simulation Time: Period:10 ; Step:25 ; Time:82181.25

3924, 1, -88.99254
9, 1, 40
2D Visualization
Solute Concentration (MT3DMS); Species:1
5.520207E-05

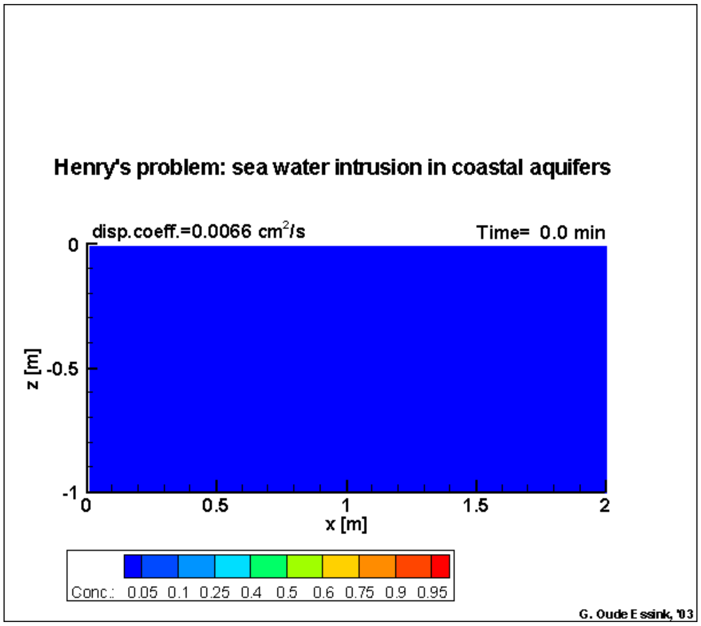
Henry’s problem (1964)



Henry’s problem



Henry's problem

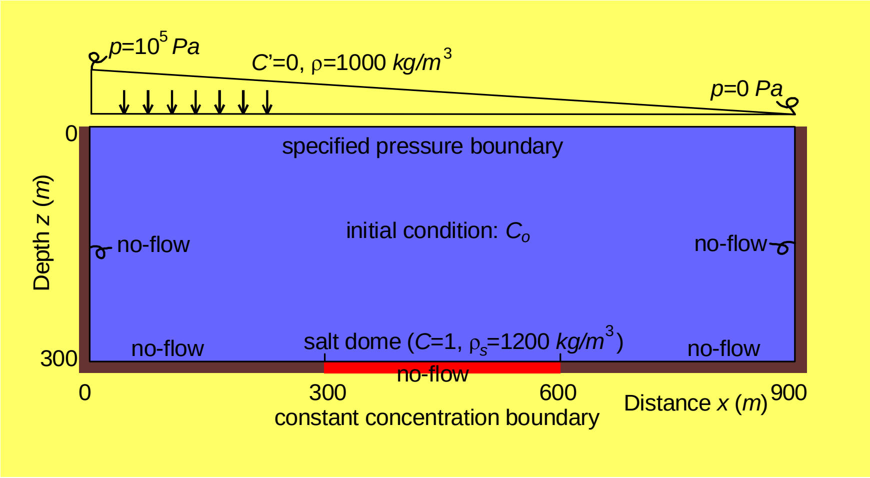


Henry's problem

Don't use the Henry problem as a variable-density benchmark, because even with a constant density model, the results are more or less the same!

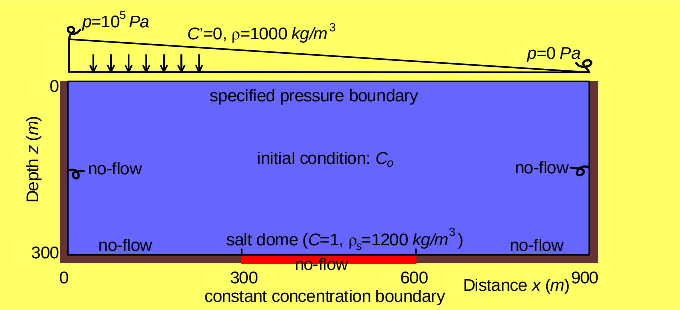
Hydrocoin:

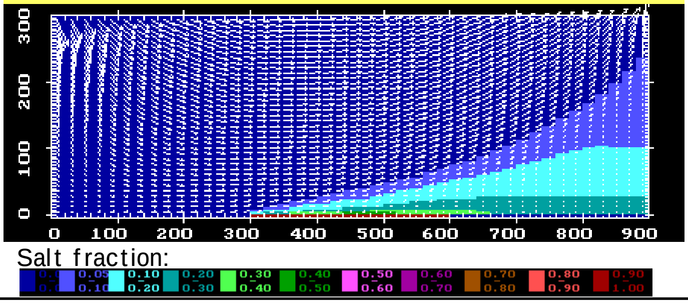
disposal of high-level nuclear waste
groundwater movement near salt domes
Gorleben salt dome, Germany



Hydrocoin:

groundwater movement near salt domes

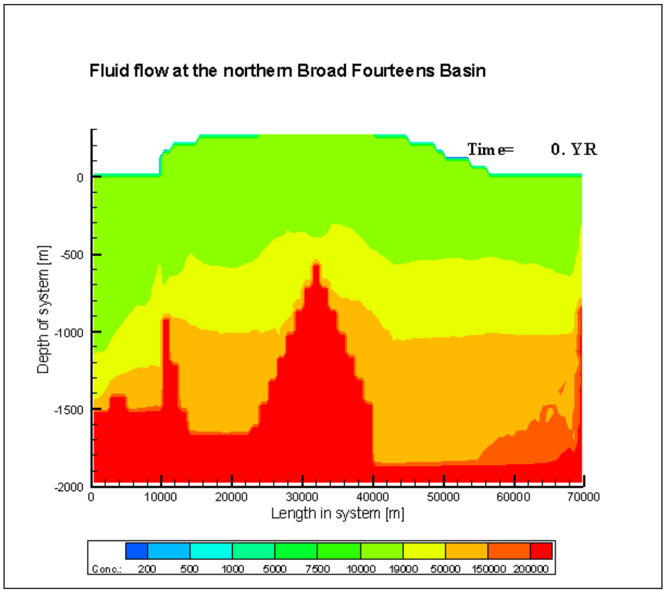




cases

Broad 14 Basin, North Sea

Geofluids'03, with L. Bouw



Bouw, L. & Oude Essink, G.H.P. 2003. Development of a freshwater lens in the inverted Broad Fourteens Basin, Netherlands offshore, J. of Geochemical Exploration (78-79), 321-325.

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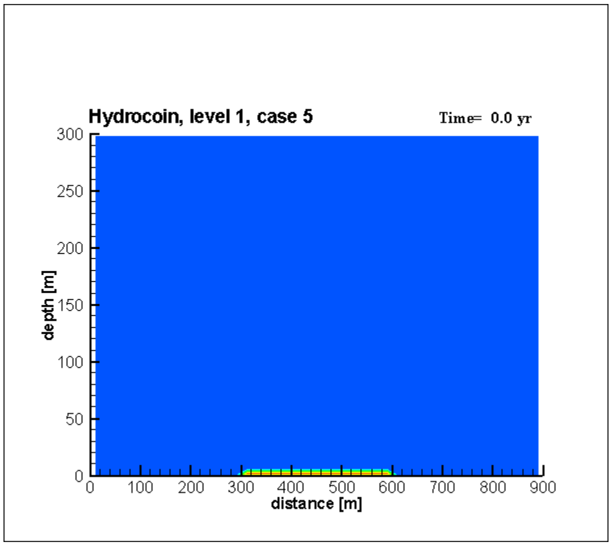
cases

Hydrocoin: effect of boundary condition (I)

supply of brine through advection and hydrodynamic dispersion

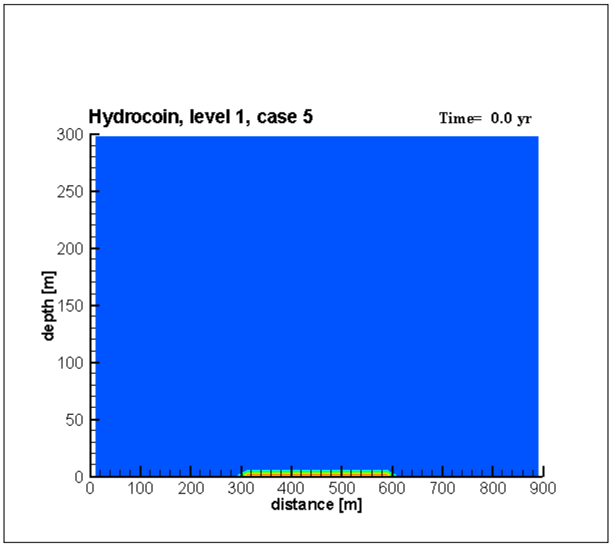


recirculation type

cases

Hydrocoin: effect of boundary condition (I)

supply of brine through advection and hydrodynamic dispersion

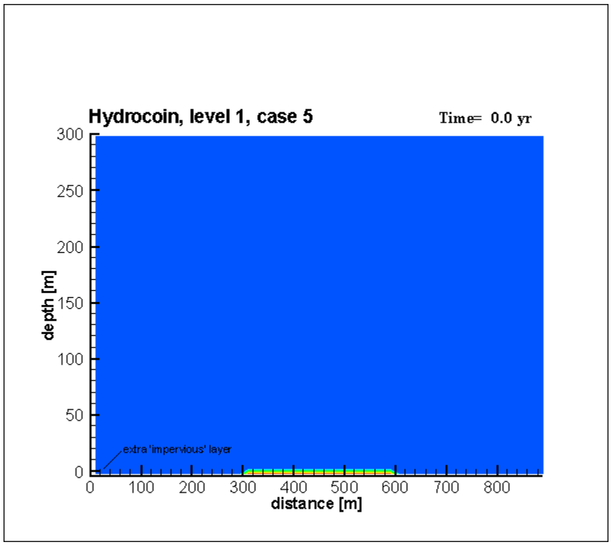


recirculation type

cases

Hydrocoin: effect of boundary condition (II)

supply of brine through only hydrodynamic dispersion

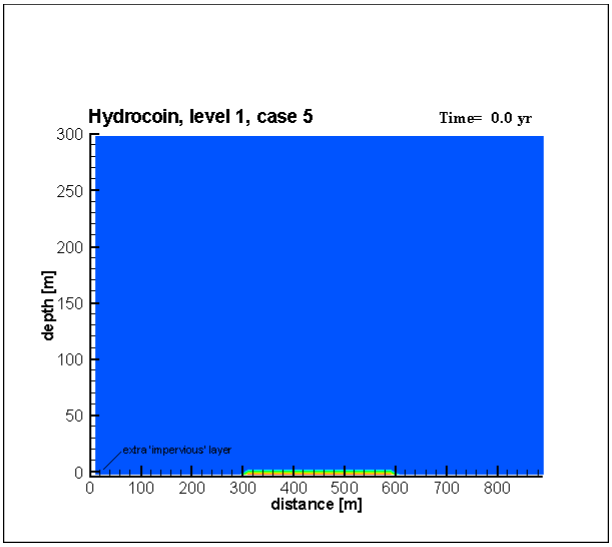


swept-forward type

cases

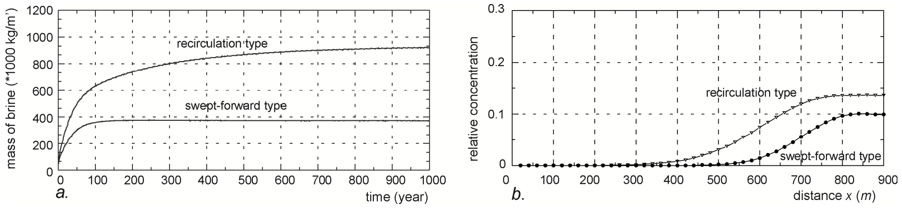
Hydrocoin: effect of boundary condition (II)

supply of brine through only hydrodynamic dispersion



swept-forward type

Hydrocoin: difference recirculation vs swept forward

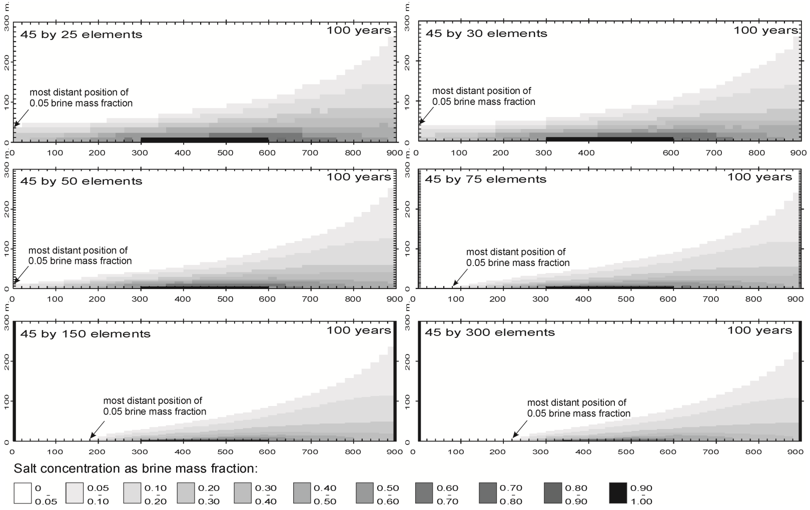


total mass of brine

brine conc at depth=200m

Lecture notes, p. 86-91

Hydrocoin: effect of vertical grid size



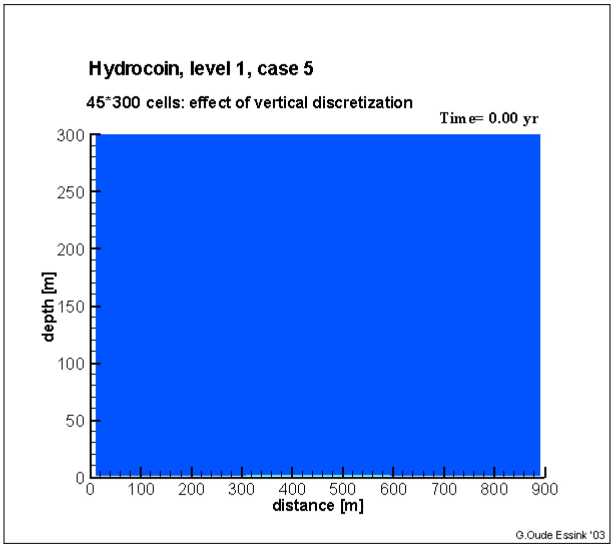
Recirculation type

---

cases

Hydrocoin: effect of vertical discretization (III)

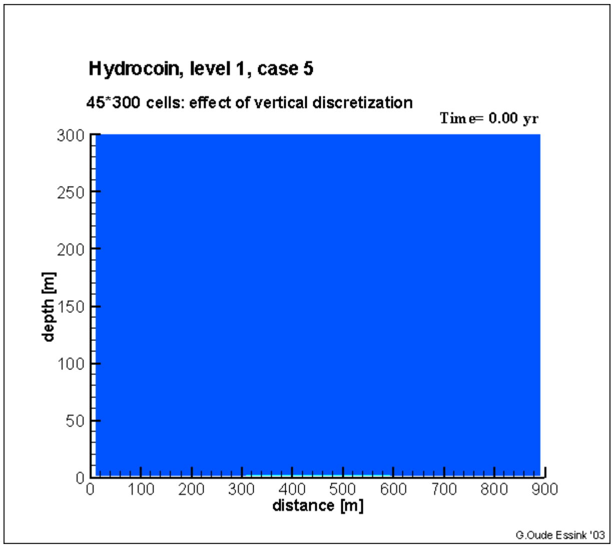
more vertical cells give better solution



like the swept-forward type

Hydrocoin: effect of vertical discretization (III)

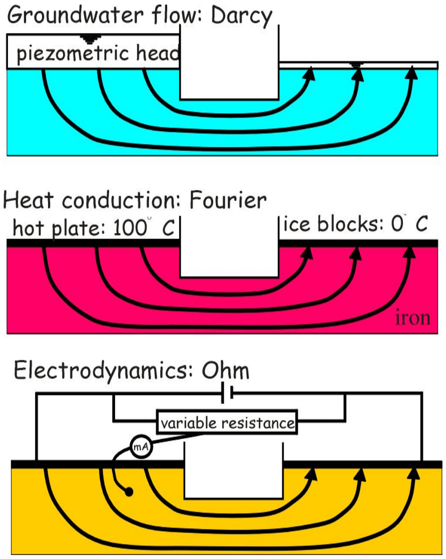
more vertical cells give better solution



like the swept-forward type

Analogy physical processes

Heat transport (analogy with solute transport)



$$q = -k \frac{\partial \phi}{\partial x}$$

$$h = -\lambda \frac{\partial T}{\partial x}$$

$$i = -\sigma \frac{\partial V}{\partial x}$$

Heat transport

Conduction and convection of heat

$$h = -\lambda_e \frac{\partial T}{\partial x} + n_e \rho c_f V T$$

heat flux — conduction (Fourier) — convection (fluid flow)

thermal conductivity [Joule/(ms ^{o}C)]

$$\lambda_e = n_e \lambda_{fluid} + (1 - n_e)\lambda_{solid}$$

continuity equation

$$-\frac{\partial h}{\partial x} = \rho' c' \frac{\partial T}{\partial t}$$

specific heat capacity [Joule/(kg ^{o}C)]

$$\rho' c' = n_e \rho c_{fluid} + (1 - n_e)\rho_{solid} c_{solid}$$

---

cases

Analogy solute and heat transport

Solute: advection-dispersion equation

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x_i}\left(D_{ij}\frac{\partial C}{\partial x_j}\right) - \frac{\partial}{\partial x_i}(CV_i) + \frac{(C - C)'W}{n_e}$$

Heat: convection-conduction equation

$$\rho' c' \frac{\partial T}{\partial t} = \frac{\partial}{\partial x_i}\left(\Lambda_{ij}\frac{\partial T}{\partial x_j}\right) - \rho c_f \frac{\partial T q_i}{\partial x_i} + \Gamma$$

Analogy heat and solute transport

Heat transport

Convection-conduction equation

$$\rho' c' \frac{\partial T}{\partial t} = \frac{\partial}{\partial x_i}\left(\Lambda_{ij}\frac{\partial T}{\partial x_j}\right) - \rho c_f \frac{\partial T q_i}{\partial x_i} + \Gamma$$

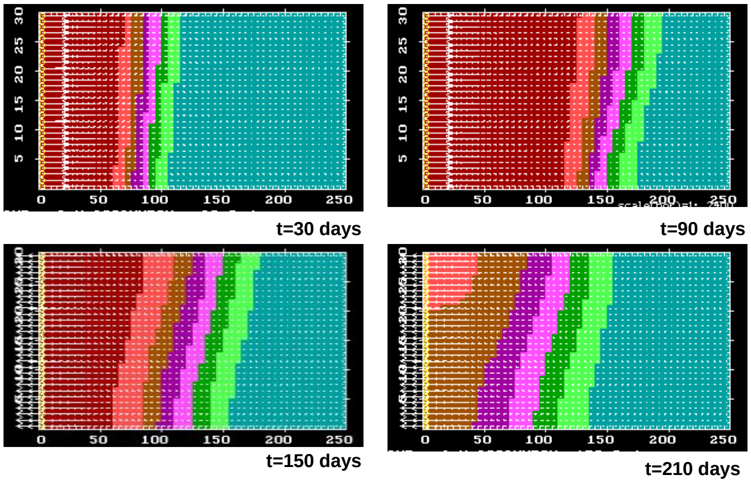
Equation of state: relation density & temperature

$$\rho_{i,j,k} = \rho_f (1-\alpha_f T_{i,j,k})$$

Analogy between solute and heat transport

Solute	Heat
C	T
R_d	$1+\frac{(1-n_e)\rho_s c_s}{n_e \rho c_f}$
D_m	$\frac{n_e \lambda_e + (1-n_e)\lambda_s}{n_e \rho c_f}$
λ	0

Energy storage in geothermal reservoirs



t=30 days

t=90 days

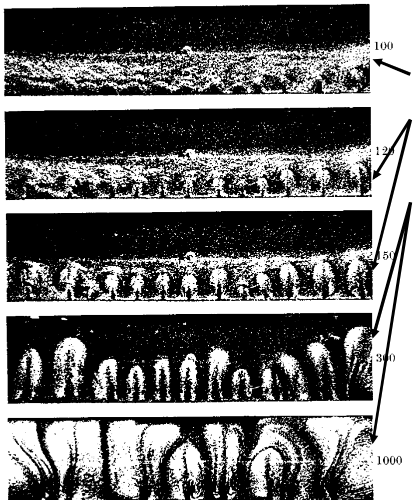
t=150 days

t=210 days

Temperature (degrees Celcius):

Elder problem (I)

It is originally a heat transport problem



Phases:

1. Stable growth diffusive boundary layer
2. Development flow cells embedded in boundary layer
3. Emergence of disturbances that grow into fingers

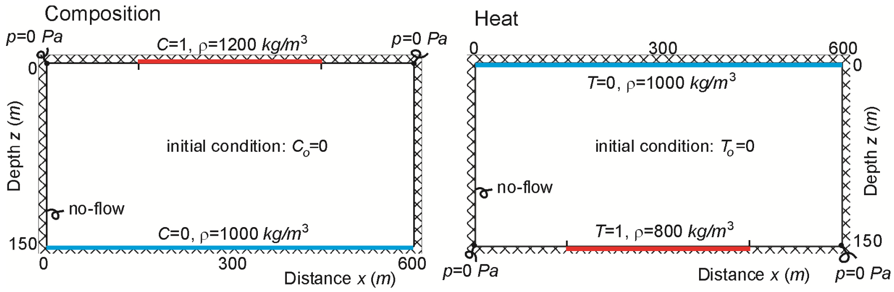
Convection of heat occurs when:

Rayleigh number > $4\pi^2$

Elder, J. Fluid Mech. 32, 69-96, 1968

Elder problem (II)

Anology composition and heat

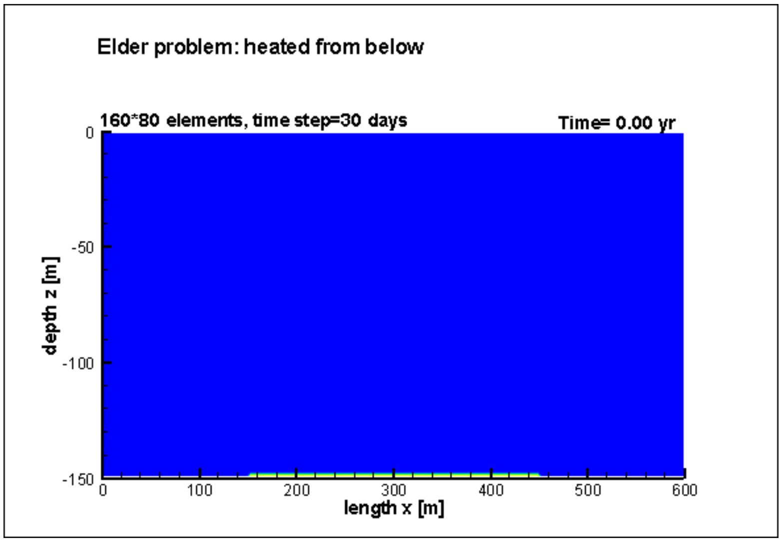


Lecture notes, p. 91-96

cases

Elder problem (III)

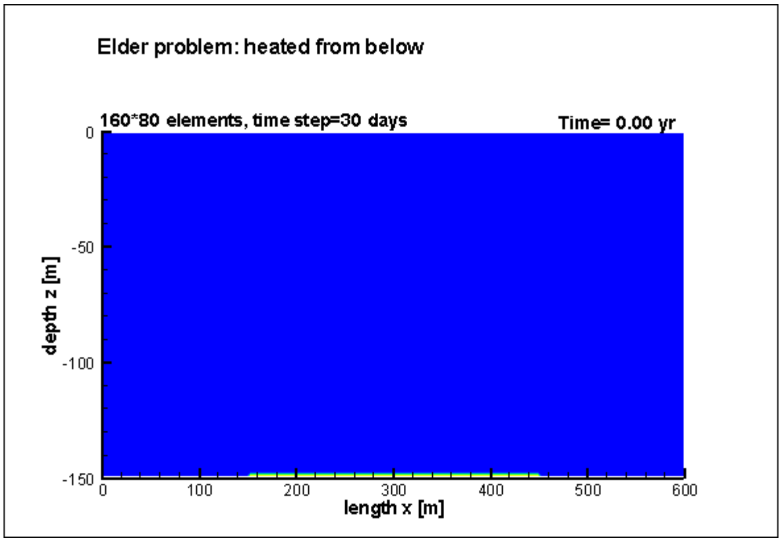
Development of convection cells (Rayleigh number=400)



cases

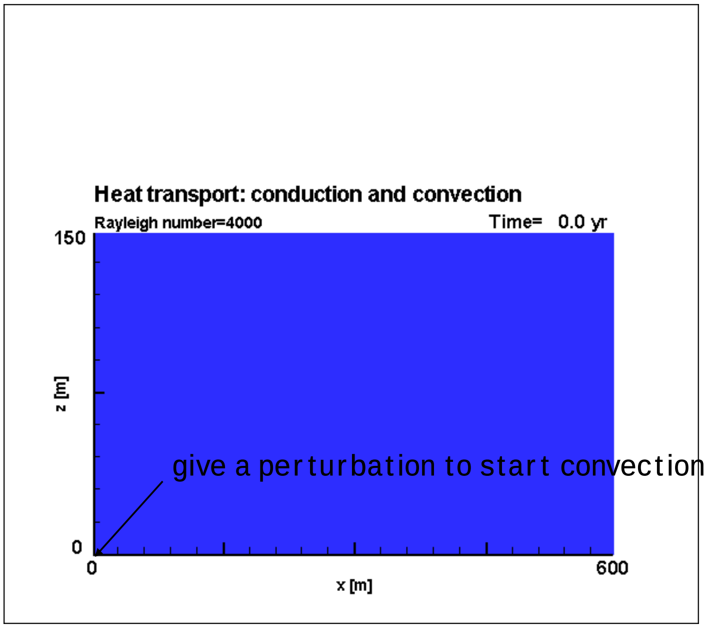
Elder problem (III)

Development of convection cells (Rayleigh number=400)



cases

Heat transport (Rayleigh number=4000)



give a perturbation to start convection

Impact of the 26-12-04 Tsunami on groundwater systems

Sri Lanka
Some days after December 26th, 2004

Impact of the 26-12-04 Tsunami on groundwater systems

Impression of relevant salinisation processes by conceptual models of salt water intrusion in coastal aquifers:

1. Fingering processes in the subsoil
2. Evolution of a freshwater lens after flooding by sea water
3. Freshwater lens in a coastal aquifer with a brackish lagoon

Next step:
quantifying processes in real situations, using topographic and hydrogeological data, and ending up with vulnerability maps

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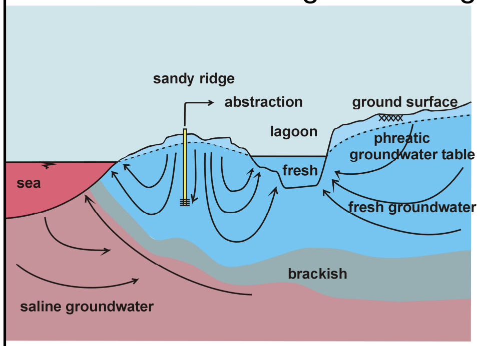
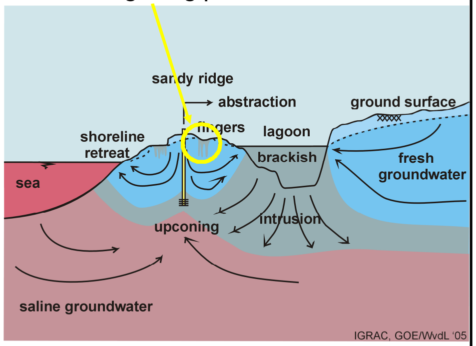
Concept 1: Fingering processes in the subsoil

Case Sri Lanka: lagoon setting



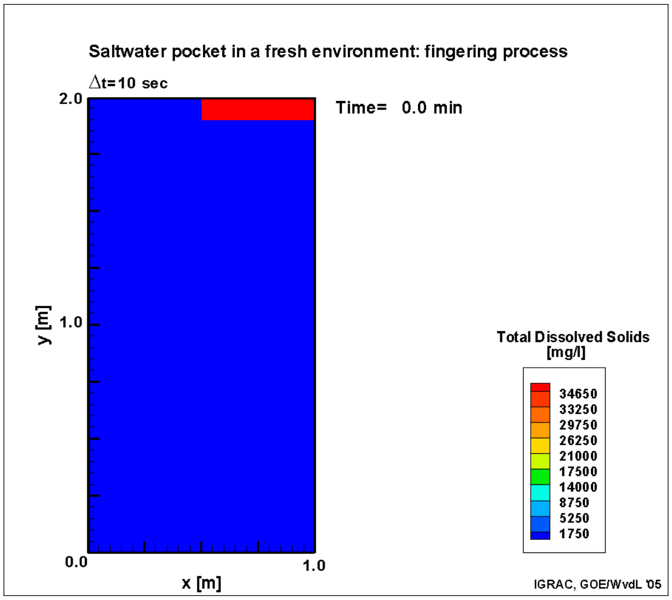
Before the Tsunami

fingering processes

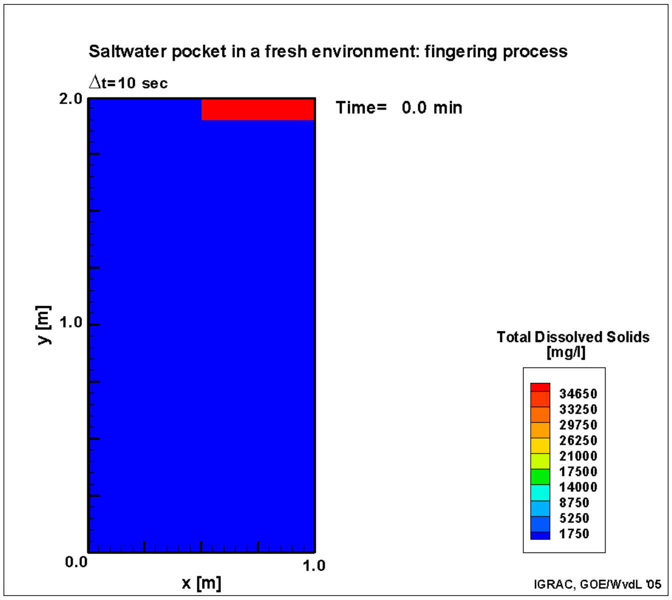


After the Tsunami

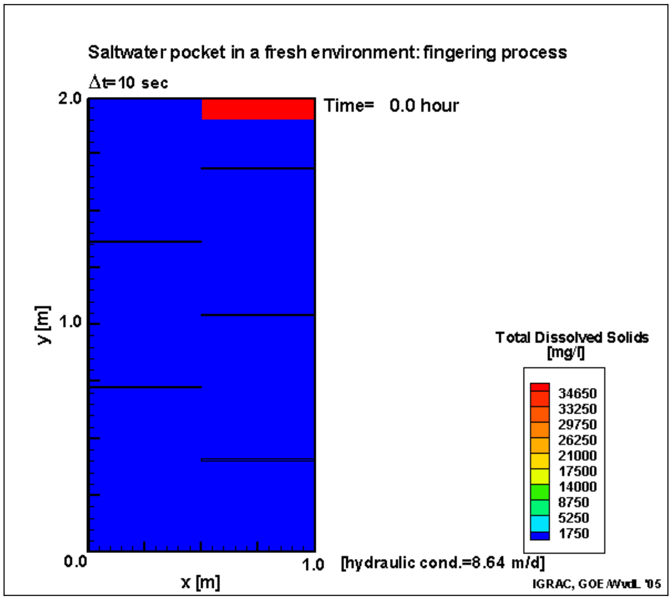
Concept 1: Fingering processes in the subsoil



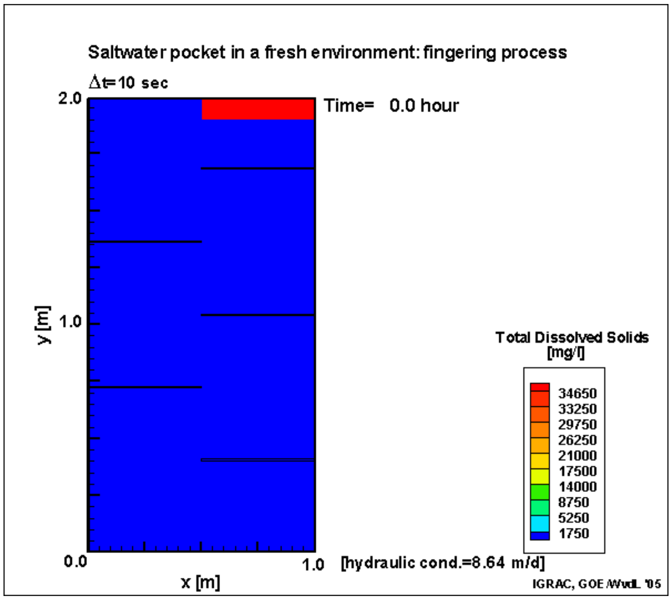
Concept 1: Fingering processes in the subsoil



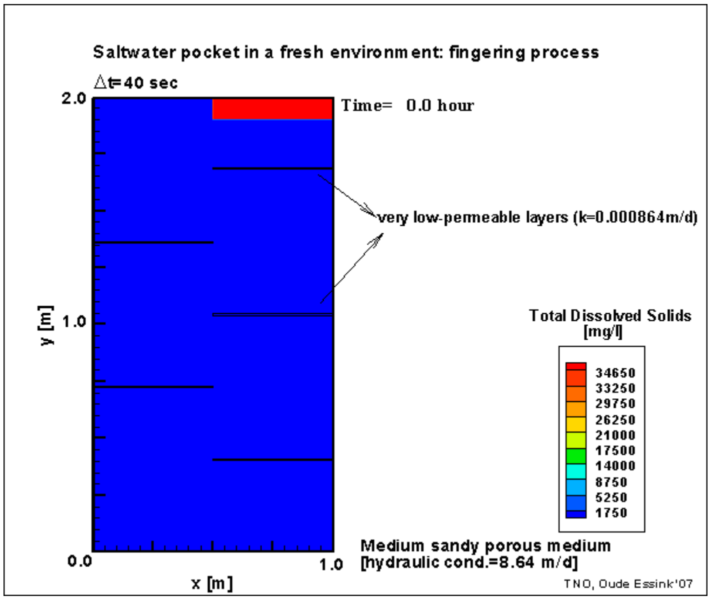
Concept 1: Fingering processes in the subsoil



Concept 1: Fingering processes in the subsoil

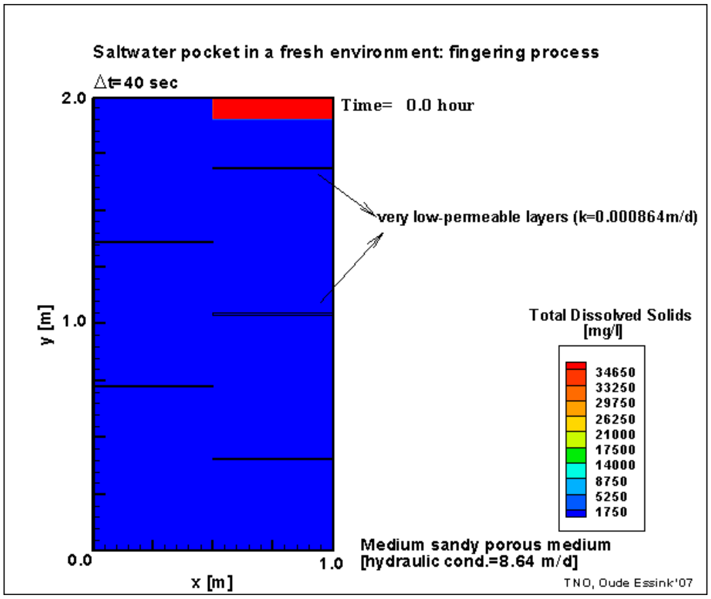


Concept 1: Fingering processes in the subsoil



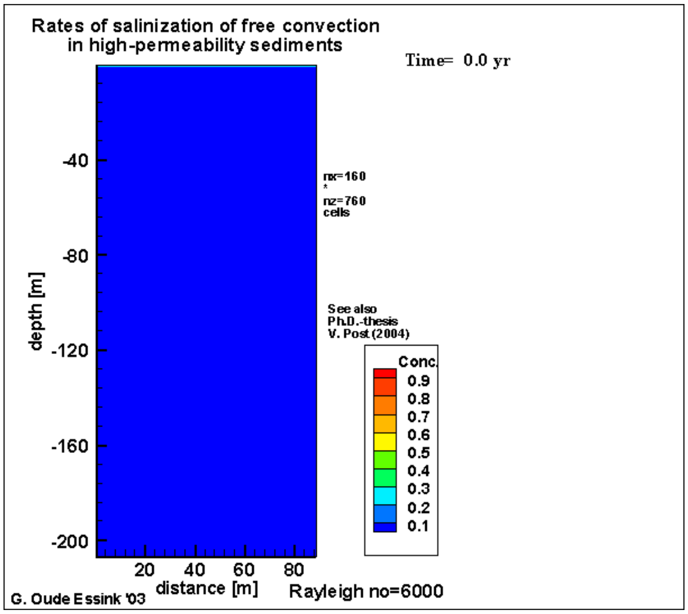
TNO, Oude Essink'07

Concept 1: Fingering processes in the subsoil

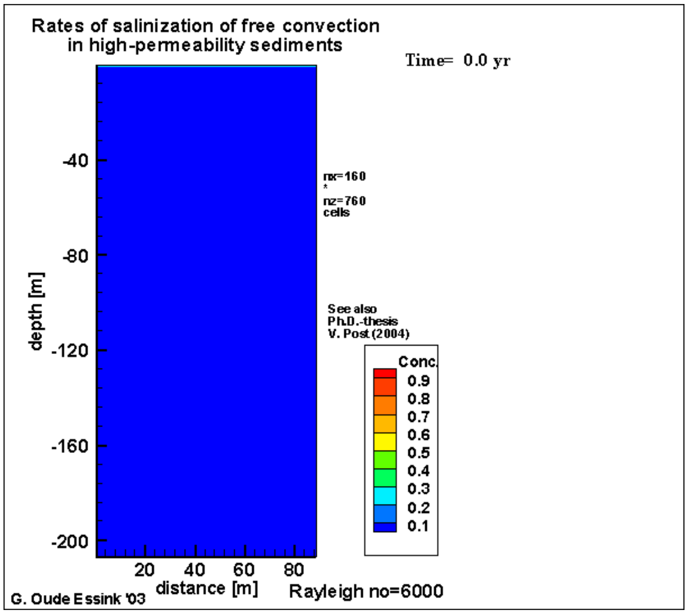


TNO, Oude Essink'07

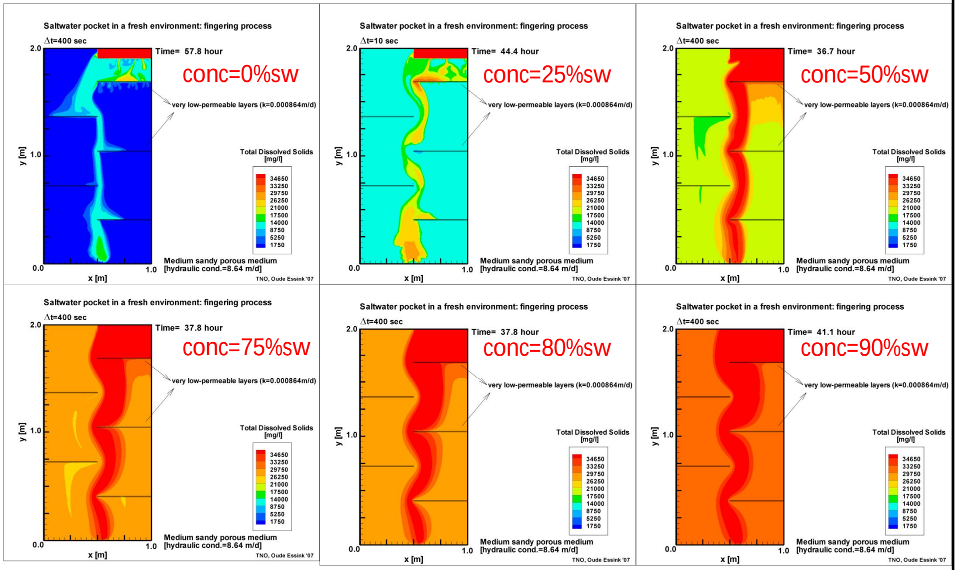
Concept 1: Fingering processes in the subsoil



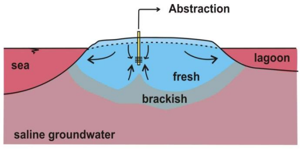
Concept 1: Fingering processes in the subsoil



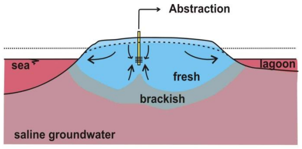
Fingering processes in the subsoil



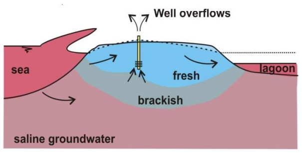
Concept 2: Evolution of a freshwater lens after flooding



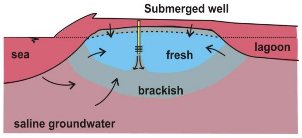
1. Before the Tsunami



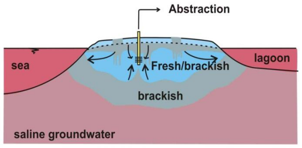
2. Just before the Tsunami:
Lowering of sea- and lagoonwater level



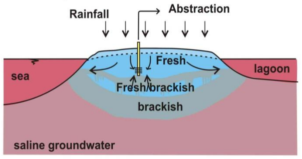
3. Just before the Tsunami:
Subsurface pressure wave precedes surface wave



4. During the Tsunami: Flooding of island,
mixing of water due to sudden pressure changes

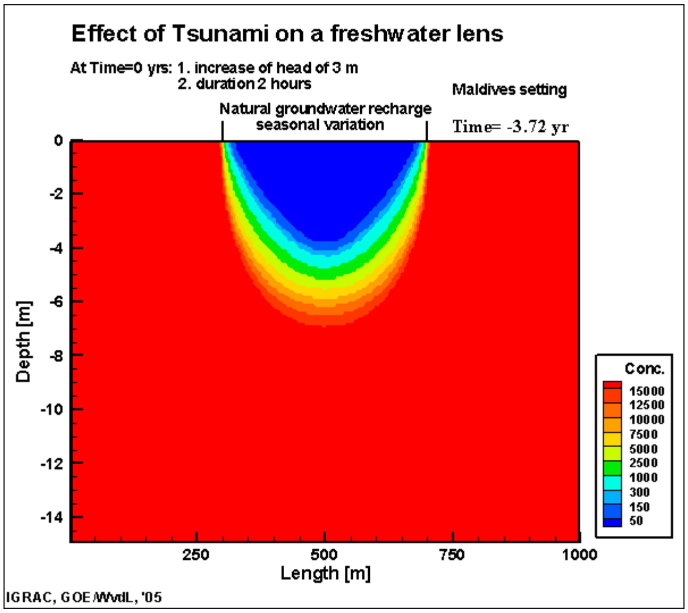


5. After the Tsunami
Freshwater mixed with brackish water



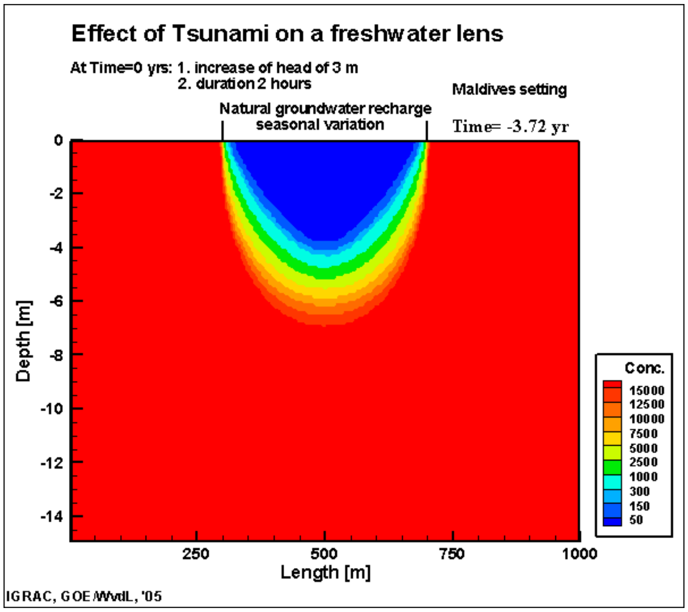
6. After the Tsunami
Recharge by rainfall replaces brackish water

Concept 2: Evolution of a freshwater lens after flooding



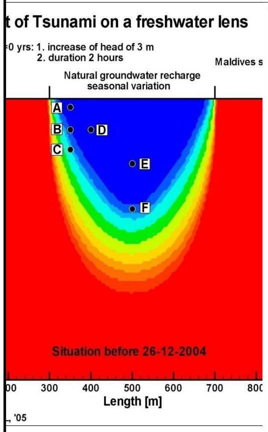
IGRAC, GOE/WvdL, '05

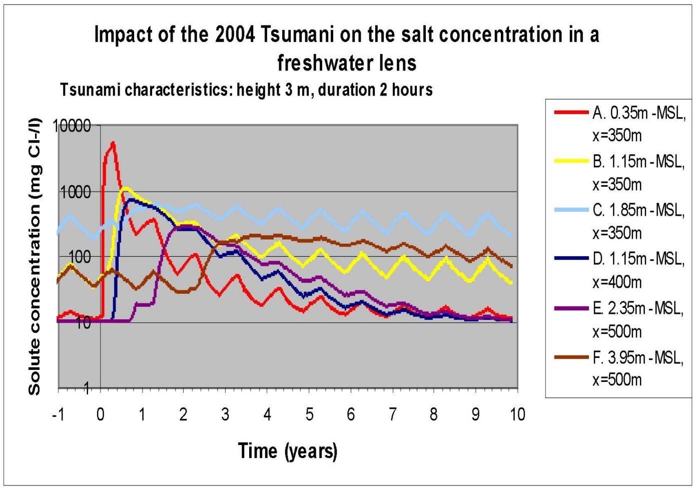
Concept 2: Evolution of a freshwater lens after flooding



IGRAC, GOE/WvdL, '05

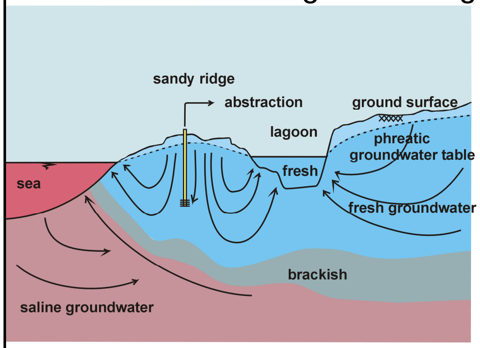
Concept 2: Evolution of a freshwater lens after flooding



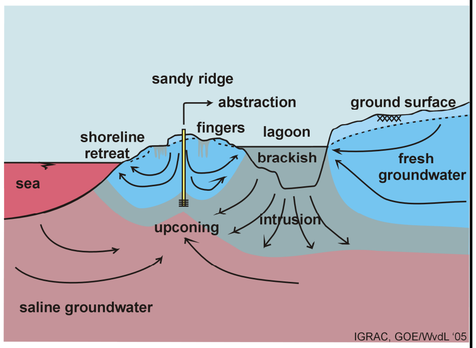


Concept 3: Freshwater lens in a coastal aquifer with a brackish lagoon

Case Sri Lanka: lagoon setting

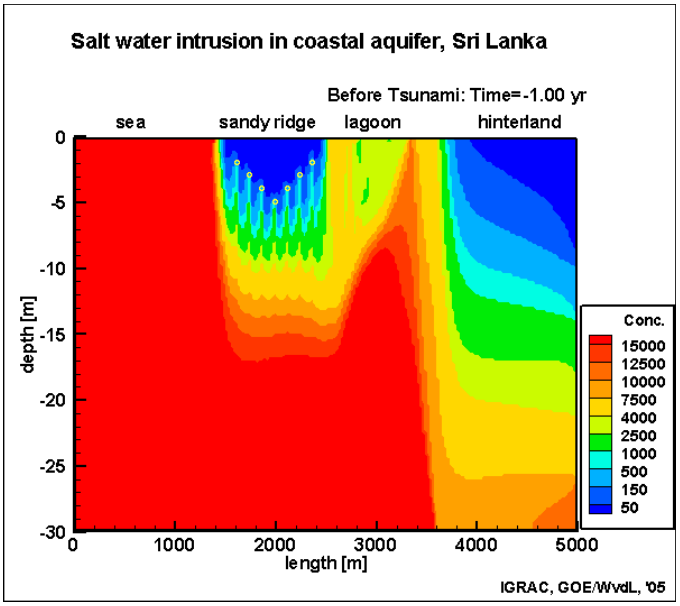


Before the Tsunami

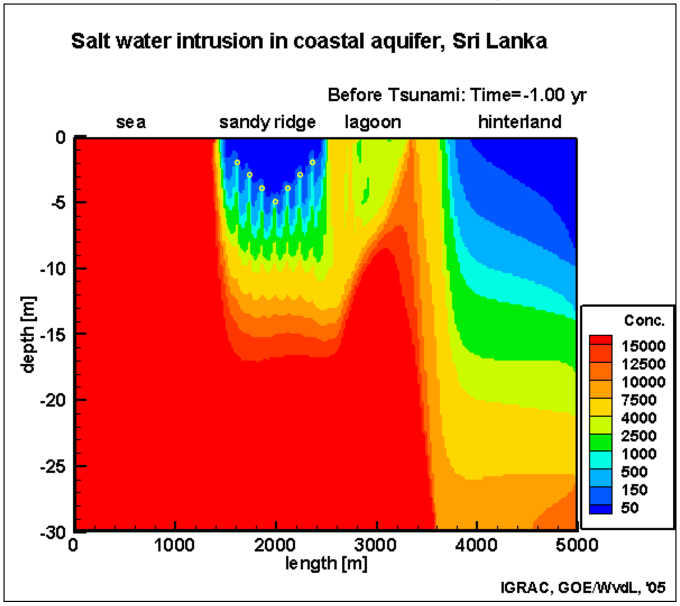


After the Tsunami

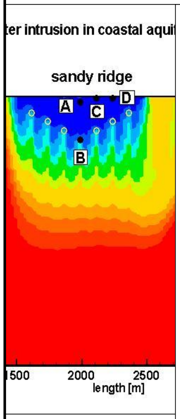
Concept 3: Freshwater lens in a coastal aquifer with a brackish lagoon

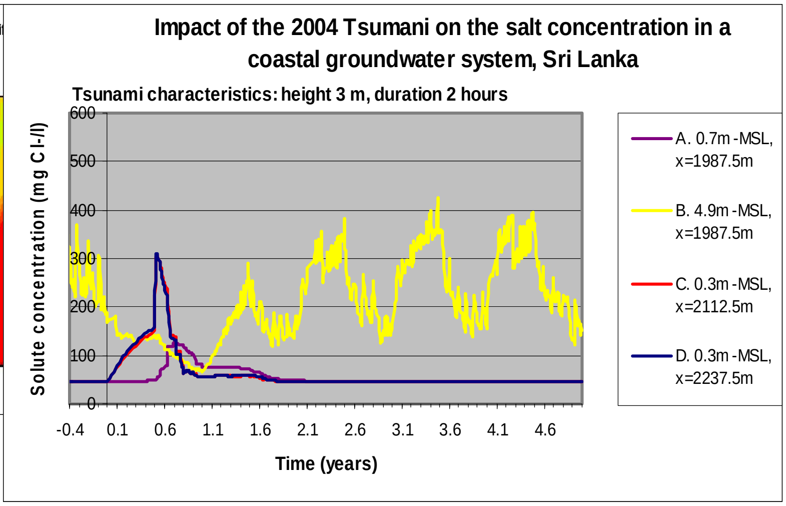


Concept 3: Freshwater lens in a coastal aquifer with a brackish lagoon



Concept 3: Freshwater lens in a coastal aquifer with a brackish lagoon




Impact of the 2004 Tsumani on the salt concentration in a coastal groundwater system, Sri Lanka

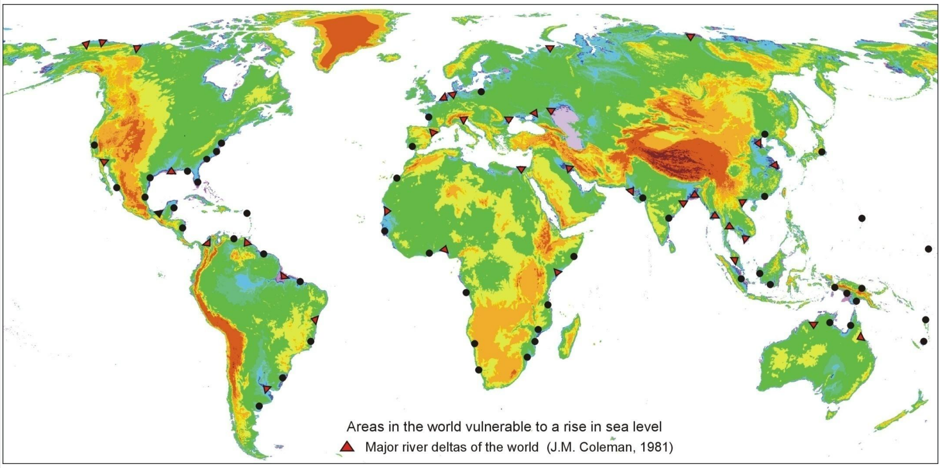
Tsunami characteristics: height 3 m, duration 2 hours

Effect sea level rise

Effects of sea level rise on groundwater resources in deltaic areas

1. Increase of salt water intrusion
2. Increase of upconing under groundwater extraction wells
3. Increase of piezometric head
4. Increase of seepage and salt load to the surface water system
5. Risk of instable Holocene aquitards
6. [Decrease of fresh groundwater reservoirs due to decrease in natural groundwater recharge]

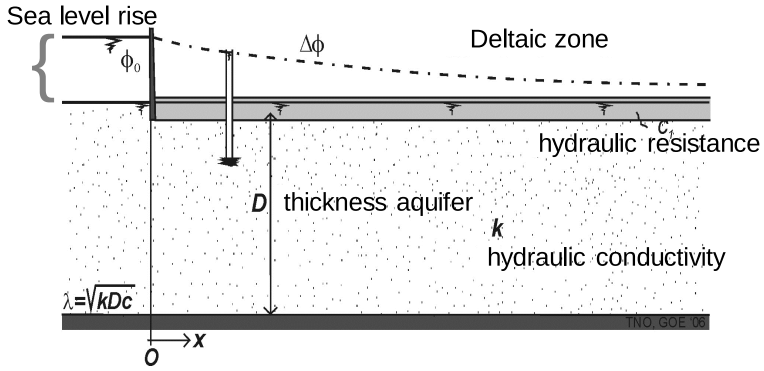
Effects of sea level rise on groundwater resources in deltaic areas


Areas in the world vulnerable to a rise in sea level

▲ Major river deltas of the world (J.M. Coleman, 1981)

Digital Elevation Model (DEM)

Effect of sea level rise:
Analytical approach for zone of influence in deltaic areas



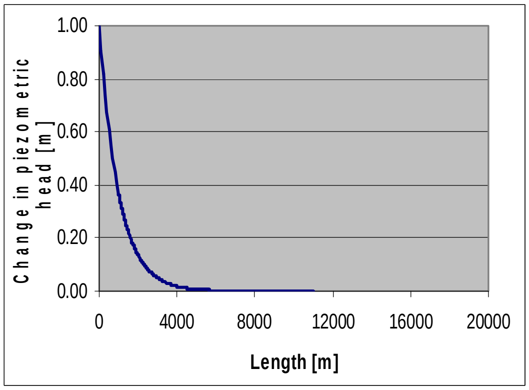
$$\Delta\phi(x)=\phi_0 e^{-x/\lambda}$$

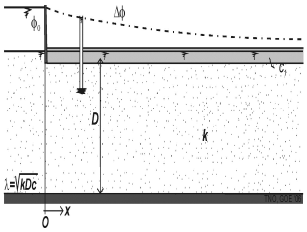
$$\lambda = \sqrt{kDc}$$

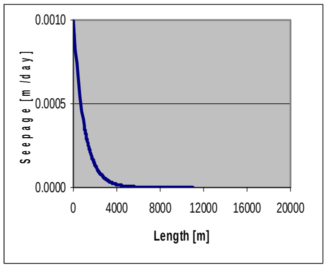
- Zone of influence is equal to sqrt(kDc)
- At $x=3\lambda$, only 5% of sea level rise is detactable

Effect of sea level rise:
Case 1 with Dutch subsoil parameters

kD = 1000 m^2/day
c = 1000 day
λ = 1000 m



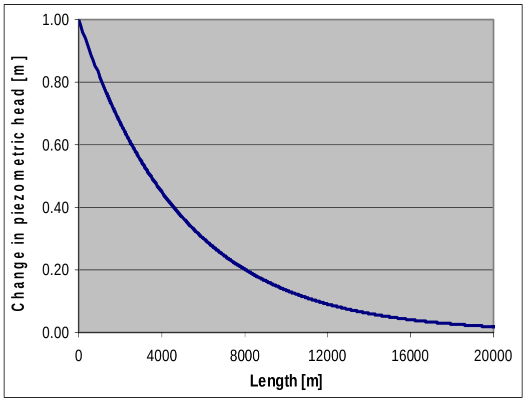


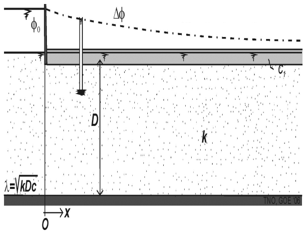


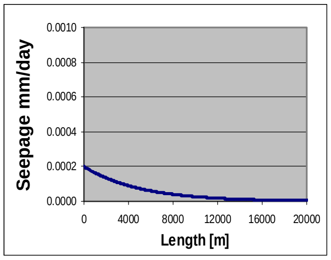
Effect of sea level rise:

Case 2 with Dutch subsoil parameters

kD = 5000 m2/day
c = 5000 day
λ = 5000 m

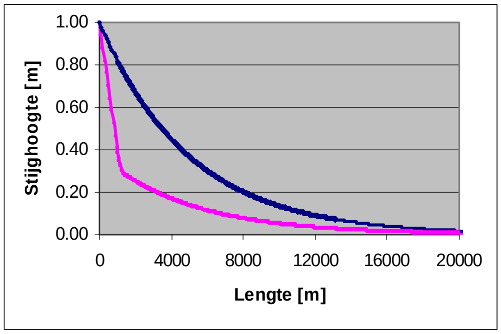


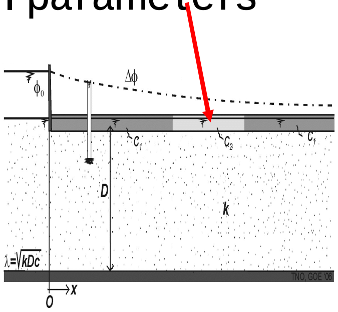


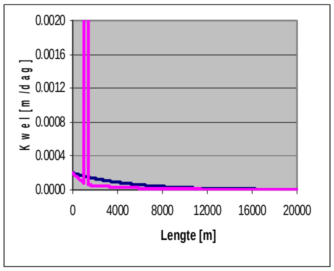


Case 3 with Dutch subsoil parameters

kD = 5000 m2/dag
c1 = 5000 dag, c2 = 50 dag

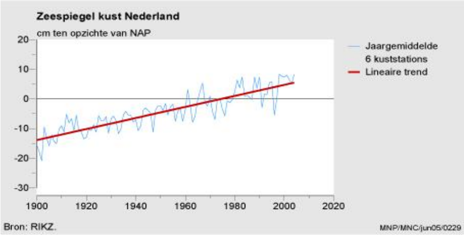


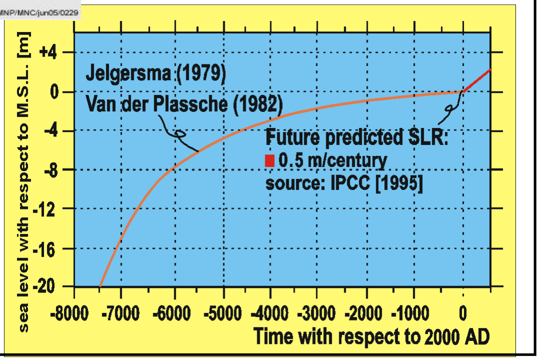




Climate change is HOT!

Past and future sea level rise in the Netherlands



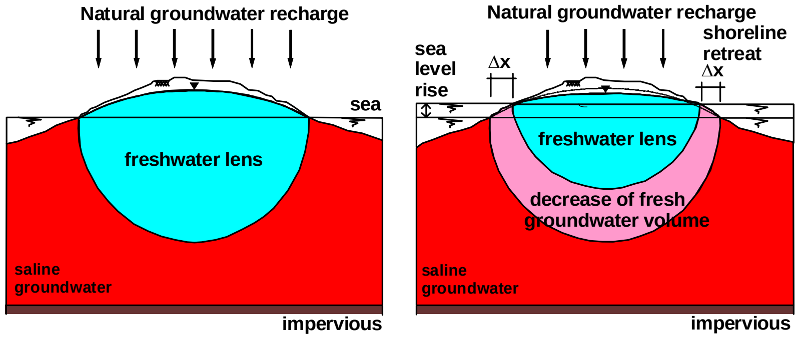


Implementing new KNMI06 climate scenarios

2100		G	G+	W	W+	C	C+
Worldwide temperature rise in 2050		**+1°C**	**+1°C**	**+2°C**	**+2°C**	**+3°C**	**+3°C**
Worldwide temperature rise in 2100		**+2°C**	**+2°C**	**+4°C**	**+4°C**	**+6°C**	**+6°C**
Change in airstream pattern Western Europa		**no**	**yes**	**no**	**yes**	**no**	**yes**
Winter	**Average temperature**	**+1,8°C**	**+2,3°C**	**+3,6°C**	**+4,6°C**	**+5,4°C**	**+6,9°C**
	Coldest winter day each year	**+2,1°C**	**+2,9°C**	**+4,2°C**	**+5,8°C**	**+6,3°C**	**+7,8°C**
	Average precipitation	7%	14%	14%	28%	21%	42%
Summer	**Average temperature**	**+1,7°C**	**+2,8°C**	**+3,4°C**	**+5,6°C**	**+5,1°C**	**+8,4°C**
	Hottest summer day each year	**+2,1°C**	**+3,8°C**	**+4,2°C**	**+7,6°C**	**+6,3°C**	**+11,4°C**
	Average precipitation	6%	-19%	12%	-38%	18%	-57%
Sea level rise	Absolute rise (cm)	35-60	35-60	40-85	40-85	45-110	45-110

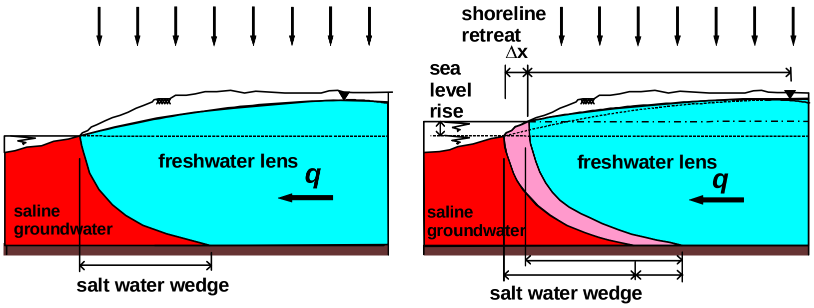
Effect of a relative sea level rise (1):

Deep aquifer



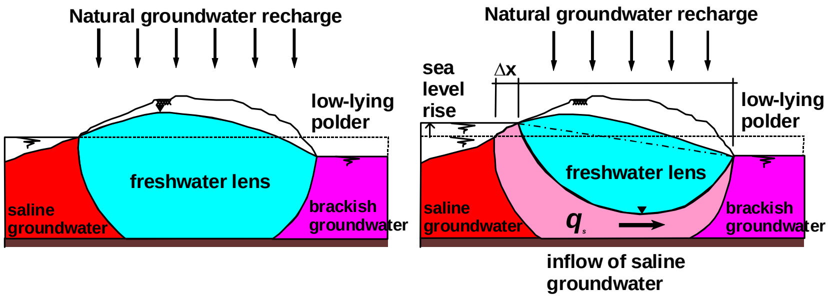
Effect of a relative sea level rise (2):

Shallow aquifer

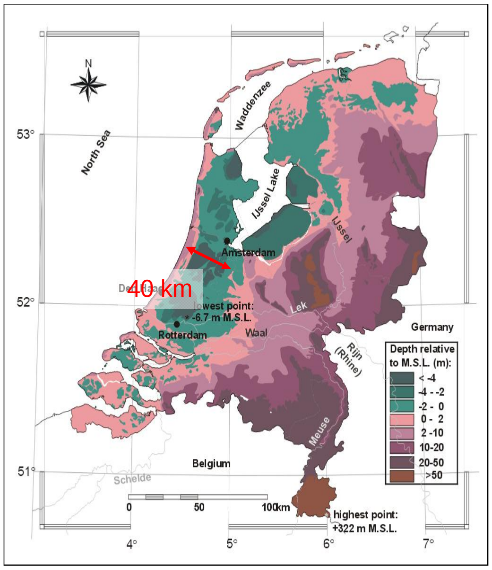


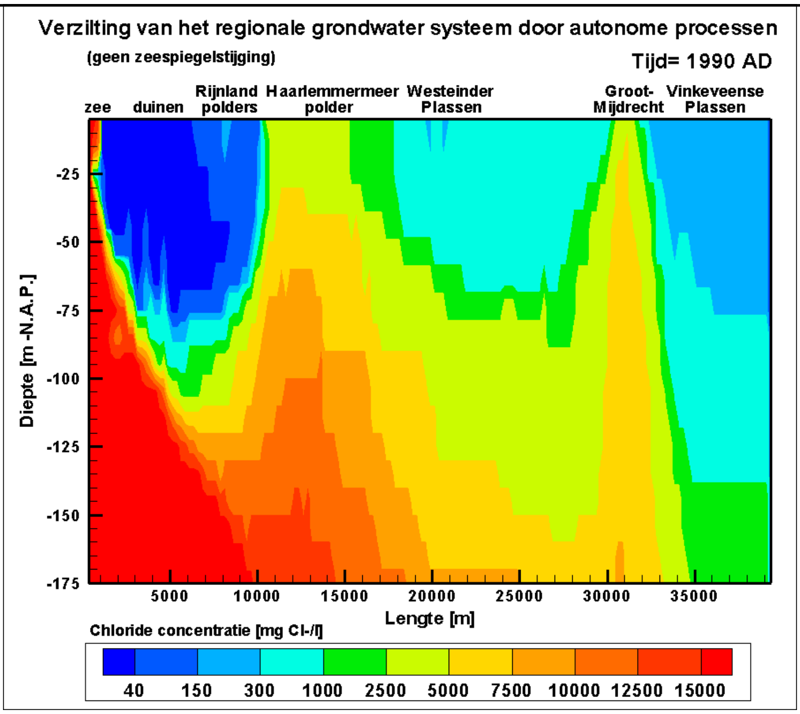
Effect of a relative sea level rise (3):

Shallow aquifer



2D Profile and effect sea level rise




Verzilting van het regionale grondwater systeem door autonome processen

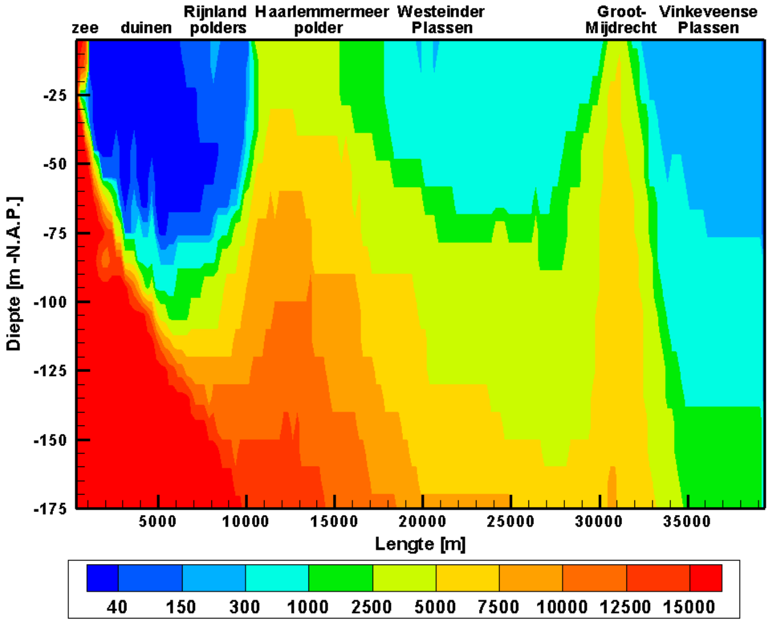
(geen zeespiegelstijging)

Tijd= 1990 AD

Verzilting van het regionale grondwater systeem door autonome processen

(geen zeespiegelstijging)

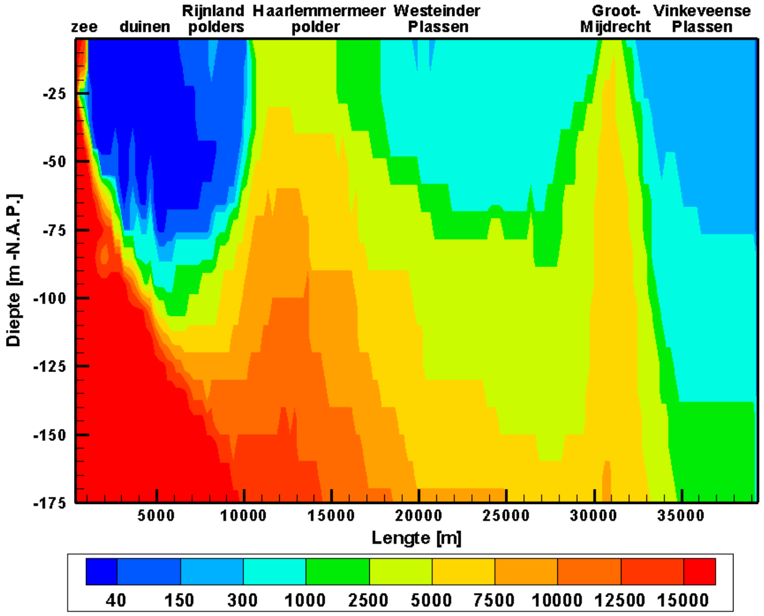
Tijd= 1990 AD



Verzilting van het regionale grondwater systeem door autonome processen

(zeespiegeldaling= -60cm per eeuw)

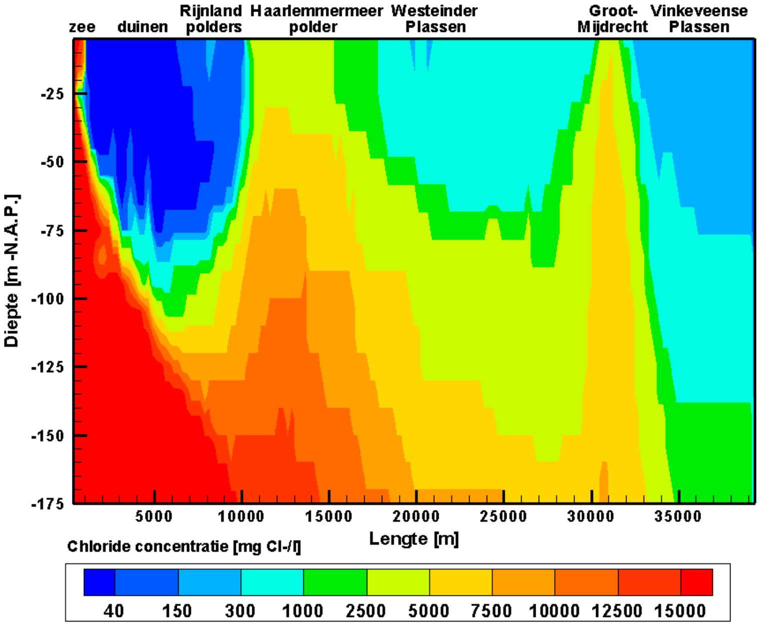
Tijd= 1990 AD



Verzilting van het regionale grondwater systeem door autonome processen

(zeespiegelstijging=60cm per eeuw)

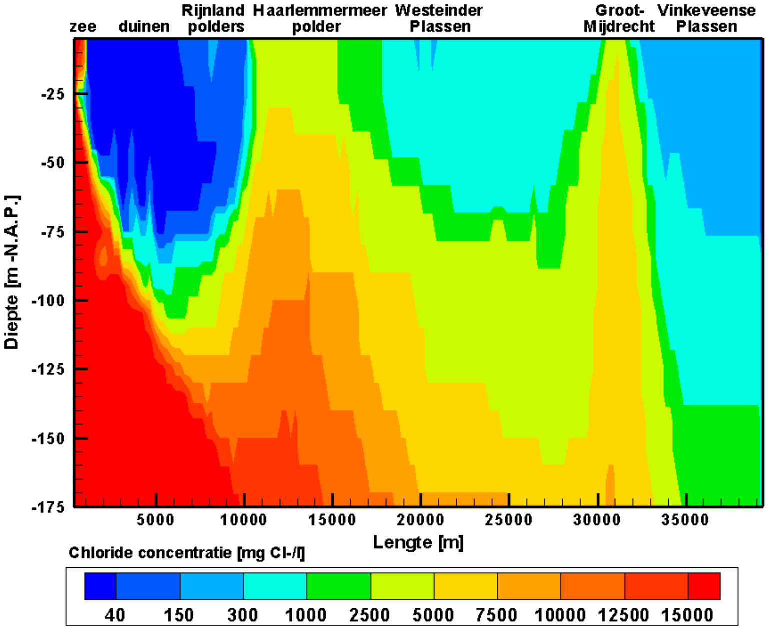
Tijd= 1990 AD



Verzilting van het regionale grondwater systeem door autonome processen

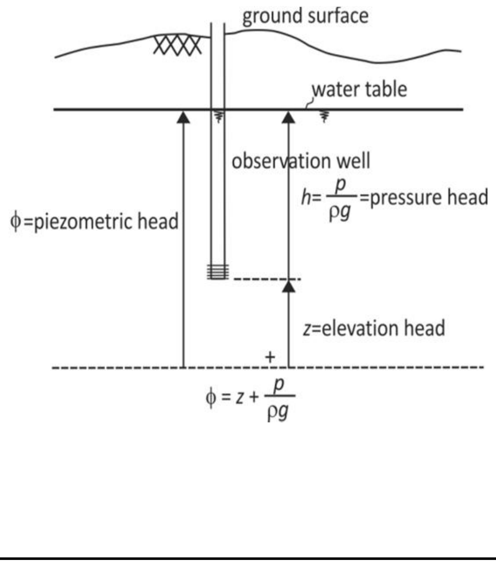
(zeespiegelstijging=150cm per eeuw)

Tijd= 1990 AD



Point water head
and
Freshwater head ϕ_f

Piezometric head ϕ



$$\phi = \frac{p}{\rho g} + z$$

$$p = \rho g\left(\phi - z\right)$$

Freshwater head ϕ_f

$$\phi_f = \frac{p}{\rho_f g} + z$$

1. Groundwater with different densities can be compared
2. Fictive parameter
3. Hydrologists like to use heads instead of pressures
4. Pressure sometimes better
5. Confusing (heads not perpendicular to streamlines)

Freshwater head ϕ_f

$$h_f = \frac{\rho}{\rho_f} h$$

$$\phi_f = h_f + z$$

$$\phi_f = \frac{\rho}{\rho_f} h + z$$

e.g.:
ρ_s=1025kg/m3
h=10m
ϕ_f=10.25m

Special case: hydrostatic pressure: q_z=0

$$q_z = -\frac{\kappa_z \rho_f g}{\mu}\left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

no vertical flow

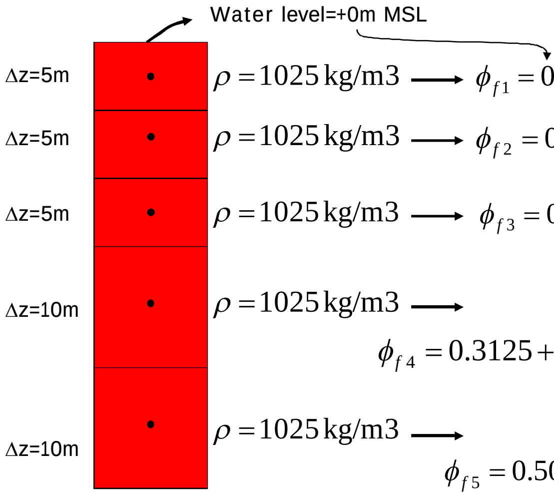
$$0 = \left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

$$\partial \phi_f = -\frac{\rho - \rho_f}{\rho_f}\partial z$$

$$\phi_{f2} = \phi_{f1} - \frac{\rho - \rho_f}{\rho_f}(z2 - z1)$$

$$\downarrow + \qquad \phi_{f2} = \phi_{f1} + \frac{\rho - \rho_f}{\rho_f}(\Delta z)$$

Hydrostatic boundary condition at the sea



$\rho = 1025\,\text{kg/m3} \longrightarrow \phi_{f1} = 0\,\text{m} + 0.025 * 2.5\text{m} = 0.0625\text{m}$

$\rho = 1025\,\text{kg/m3} \longrightarrow \phi_{f2} = 0.0625 + 0.025 * 5\text{m} = 0.1875\text{m}$

$\rho = 1025\,\text{kg/m3} \longrightarrow \phi_{f3} = 0.1875 + 0.025 * 5\text{m} = 0.3125\text{m}$

$\rho = 1025\,\text{kg/m3} \longrightarrow$

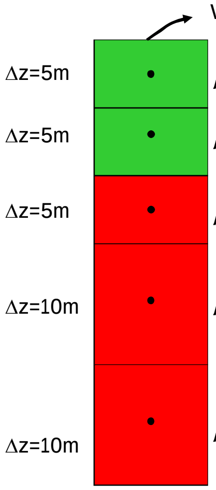
$\phi_{f4} = 0.3125 + 0.025 * (2.5\text{m} + 5\text{m}) = 0.50\text{m}$

$\rho = 1025\,\text{kg/m3} \longrightarrow$

$\phi_{f5} = 0.50 + 0.025 * (5\text{m} + 5\text{m}) = 0.75\text{m}$

$$\phi_{f2} = \phi_{f1} + \frac{\rho - \rho_f}{\rho_f}(\Delta z)$$

Hydrostatic boundary condition at the sea



$\rho = 1010\ \text{kg/m3} \longrightarrow \phi_{f1} = 0\ \text{m} + 0.010 * 2.5\text{m} = 0.025\text{m}$

$\rho = 1010\ \text{kg/m3} \longrightarrow \phi_{f2} = 0.025 + 0.010 * 5\text{m} = 0.075\text{m}$

$\rho = 1025\ \text{kg/m3} \longrightarrow$

$\phi_{f3} = 0.075 + 0.010 * 2.5\text{m} + 0.025 * 2.5\text{m} = 0.1625\text{m}$

$\rho = 1025\ \text{kg/m3} \longrightarrow$

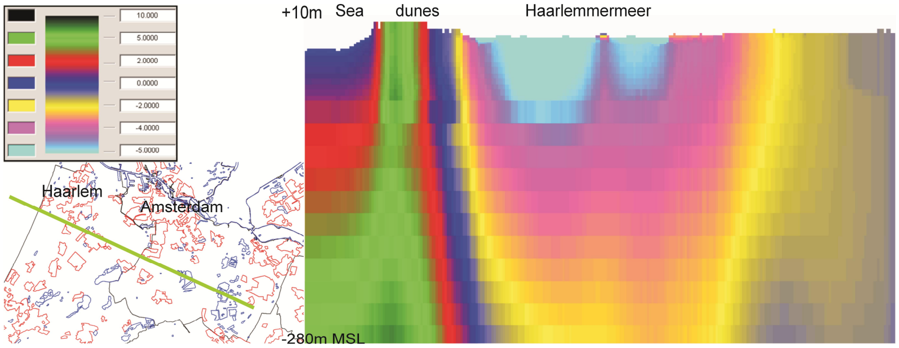
$\phi_{f4} = 0.1625 + 0.025 * (2.5\text{m} + 5\text{m}) = 0.35\text{m}$

$\rho = 1025\ \text{kg/m3} \longrightarrow$

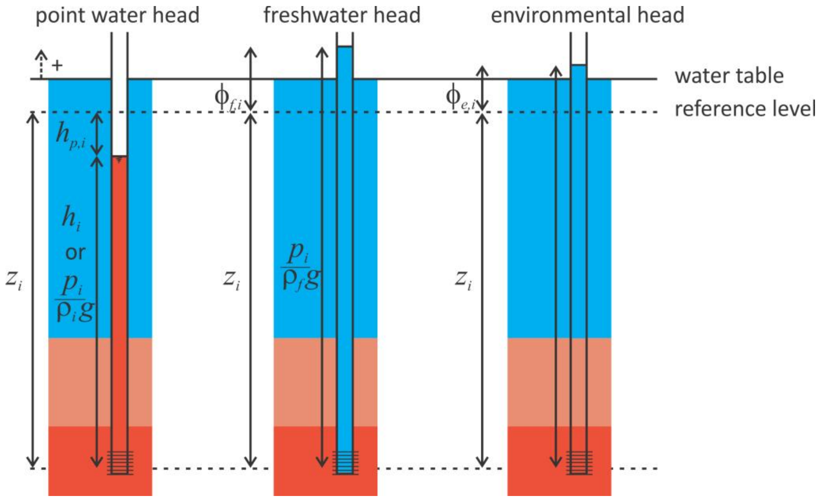
$\phi_{f5} = 0.35 + 0.025 * (5\text{m} + 5\text{m}) = 0.60\text{m}$

$$\phi_{f2} = \phi_{f1} + \frac{\rho - \rho_f}{\rho_f}(\Delta z)$$

Example 2D profile NHI model freshwater head ϕ_f



Which one is useful?



Post, Kooi and Simmons, 2007, Ground Water

Point water head

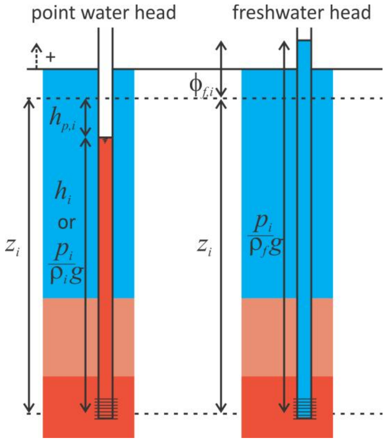
$$h_{p,i} = z_i + h_i \longleftrightarrow h_i = h_{p,i} - z_i$$

$$h_i = \frac{p_i}{\rho_i g} \longleftrightarrow p_i = h_i \rho_i g$$

Freshwater head

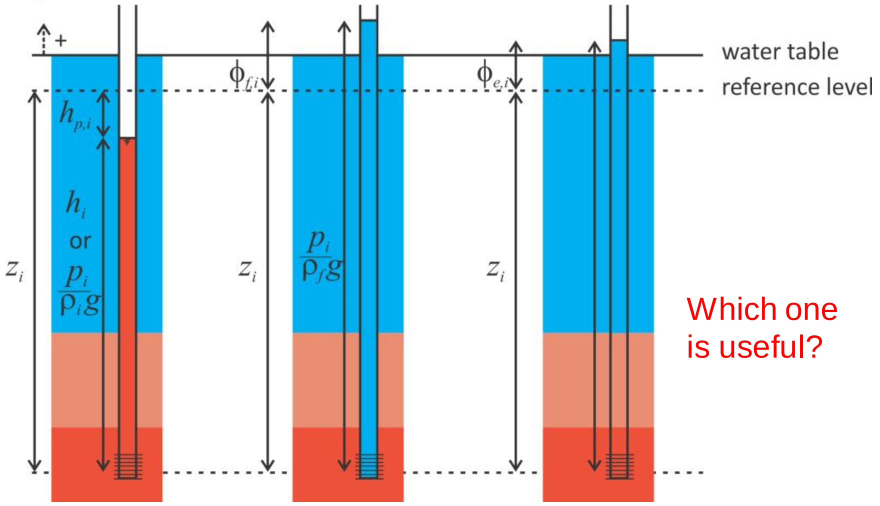
$$\phi_{f,i} = z_i + \frac{p_i}{\rho_f g} \longleftrightarrow \phi_{f,i} = z_i + \frac{h_i \rho_i}{\rho_f}$$

$$\phi_{f,i} = \frac{\rho_i}{\rho_f} h_{p,i} - \frac{\rho_i - \rho_f}{\rho_f} z_i$$



Post, Kooi and Simmons, 2007, Ground Water

$$h_{f,i} = \frac{\rho_i}{\rho_f} h_i - \frac{\rho_i - \rho_f}{\rho_f} z_i \qquad h_{f,i} = z_i + \frac{P_i}{\rho_f g}$$



Which one is useful?

Post, Kooi and Simmons, 2007, Ground Water

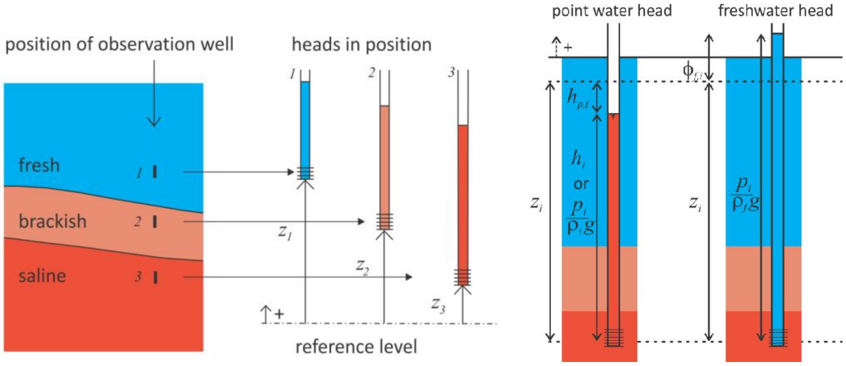
Point water head

Freshwater head

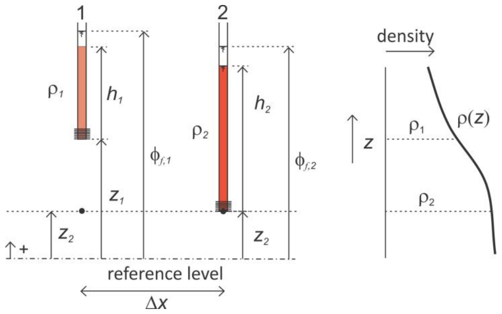
Example 1: $h_{p,i}$=-1 *m MSL*, ρ_i =1025 kg/m^{-3}, z_i=-11*m MSL*: $\phi_{f,i}$=-0.75*m MSL*.

Example 2: $h_{p,i}$=0 *m MSL*, ρ_i =1025 kg/m^{-3}, z_i=-10*m MSL*: $\phi_{f,i}$=0.25*m MSL*.

Example 3: $h_{p,i}$=0 *m MSL*, ρ_i =1025 kg/m^{-3}, z_i=-100*m MSL*: $\phi_{f,i}$=2.50*m MSL*.



Freshwater head ϕ_f: horizontal flow?

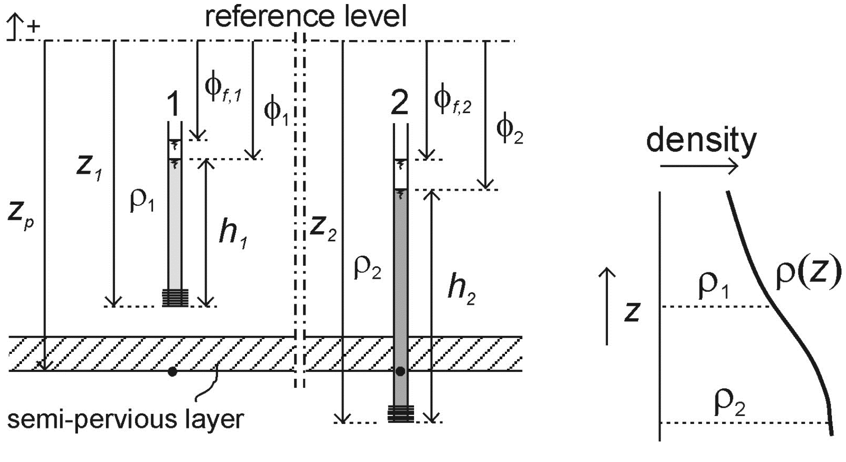


$$p_1^{at\ z=z_2} = \rho_1 g h_1 + \int_{z_2}^{z_1} \rho(z) g dz \qquad \phi_{f,1}^{at\ z=z_2} = z_2 + \frac{\rho_1}{\rho_f} h_1 + \frac{1}{\rho_f g} \int_{z_2}^{z_1} \rho(z) g dz$$

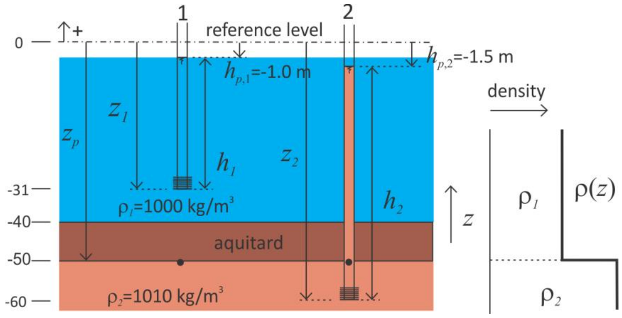
$$p_2^{at\ z=z_2} = \rho_2 g h_2 \qquad \phi_{f,2}^{at\ z=z_2} = z_2 + \frac{\rho_2}{\rho_f} h_2$$

$$q^{at\ z=z_2} \cong -k_x \frac{\phi_{f,2}^{at\ z=z_2} - \phi_{f,1}^{at\ z=z_2}}{\Delta x}$$

Freshwater head ϕ_f : vertical flow?

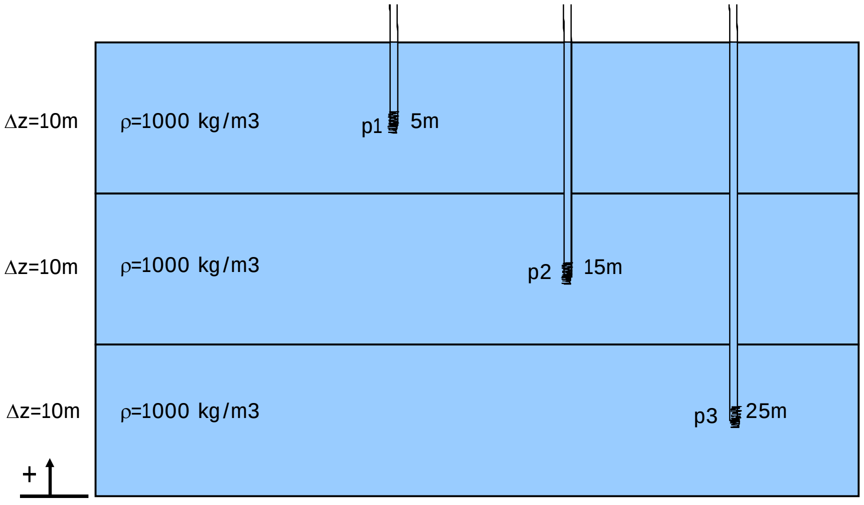


Freshwater head ϕ_f

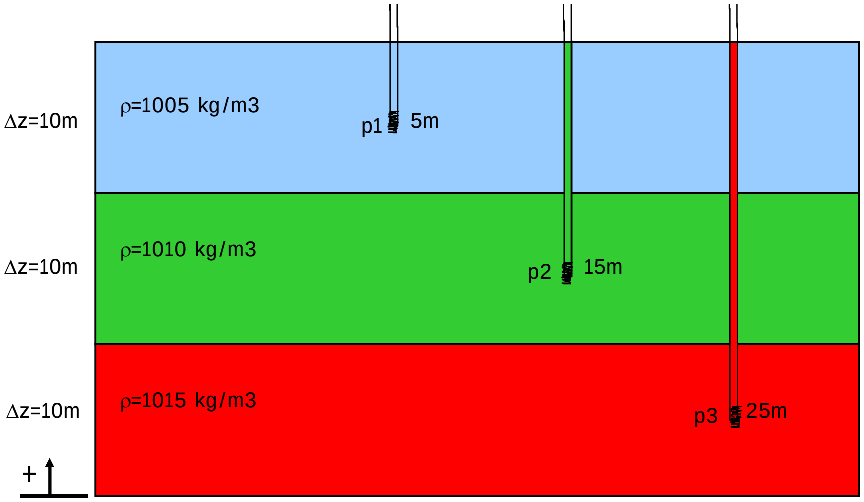


$$\phi_{f,1}^{z=-50} = -50 + \frac{1000}{1000}30 + \frac{1}{1000g}\int_{-50}^{-31} 1000 g dz = -50 + 30 + 19 = -1.0$$

$$\phi_{f,2}^{z=-50} = -50 + \frac{1010}{1000}58.5 - \frac{1}{1000g}\int_{-60}^{-50} 1010 g dz = -50 + 59.085 - 1.01(-50+60) = -1.015$$

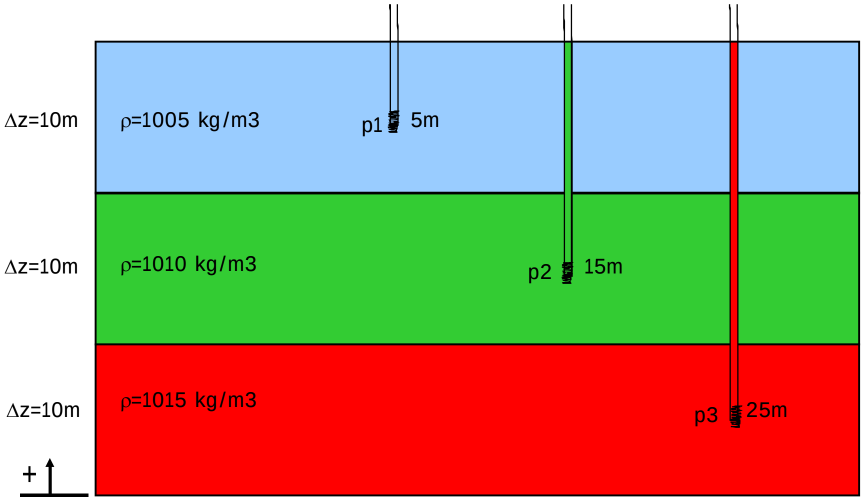


No flow



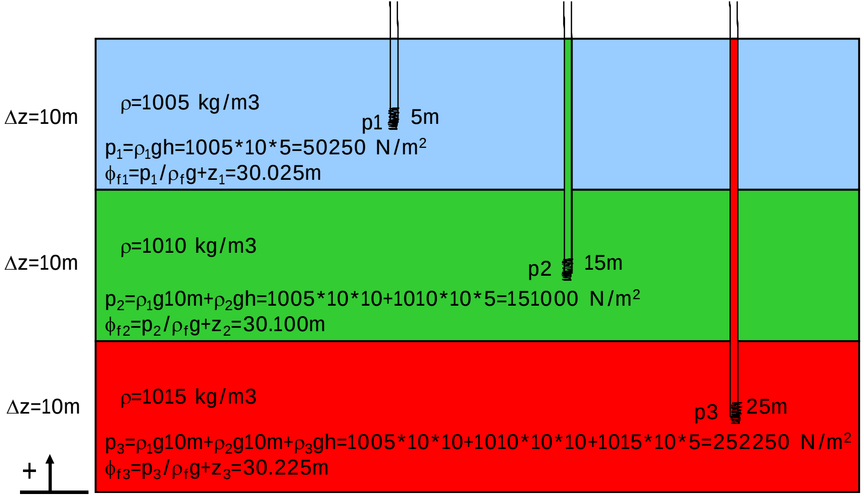
Flow or no flow? (if p≠hydrostatic than flow)

Calculate to freshwater head!



1. Determine hydrostatic pressure (and freshwater head ϕ_f)
2. Determine pressure p <u>in</u> well! (and freshwater head ϕ_f)

1. Determine hydrostatic pressure and frwhead



ρ=1005 kg/m3

$p_1=\rho_1 gh=1005*10*5=50250\ N/m^2$

$\phi_{f1}=p_1/\rho_f g+z_1=30.025m$

ρ=1010 kg/m3

$p_2=\rho_1 g10m+\rho_2 gh=1005*10*10+1010*10*5=151000\ N/m^2$

$\phi_{f2}=p_2/\rho_f g+z_2=30.100m$

ρ=1015 kg/m3

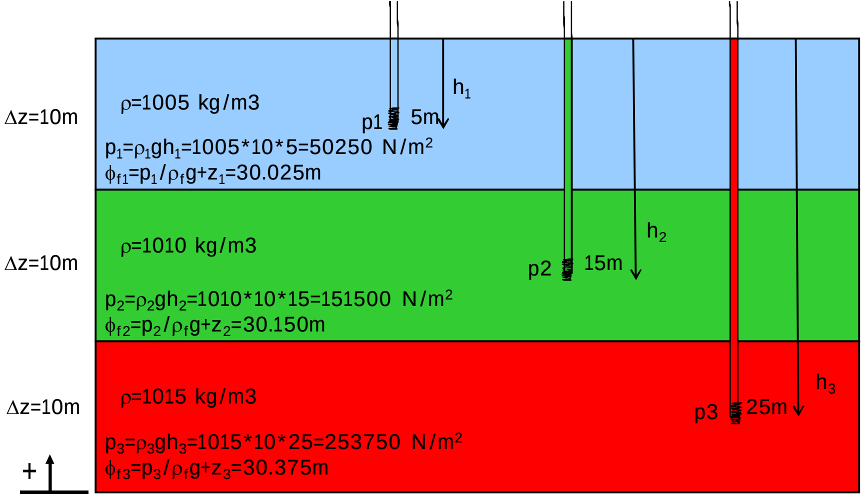
$p_3=\rho_1 g10m+\rho_2 g10m+\rho_3 gh=1005*10*10+1010*10*10+1015*10*5=252250\ N/m^2$

$\phi_{f3}=p_3/\rho_f g+z_3=30.225m$

1. Determine hydrostatic pressure (and freshwater head ϕ_f)
2. Determine pressure p <u>in</u> well! (and freshwater head ϕ_f)

---

2. Determine pressure p <u>in</u> well and frwhead



ρ=1005 kg/m3

$p_1=\rho_1 gh_1=1005*10*5=50250\ N/m^2$

$\phi_{f1}=p_1/\rho_f g+z_1=30.025m$

ρ=1010 kg/m3

$p_2=\rho_2 gh_2=1010*10*15=151500\ N/m^2$

$\phi_{f2}=p_2/\rho_f g+z_2=30.150m$

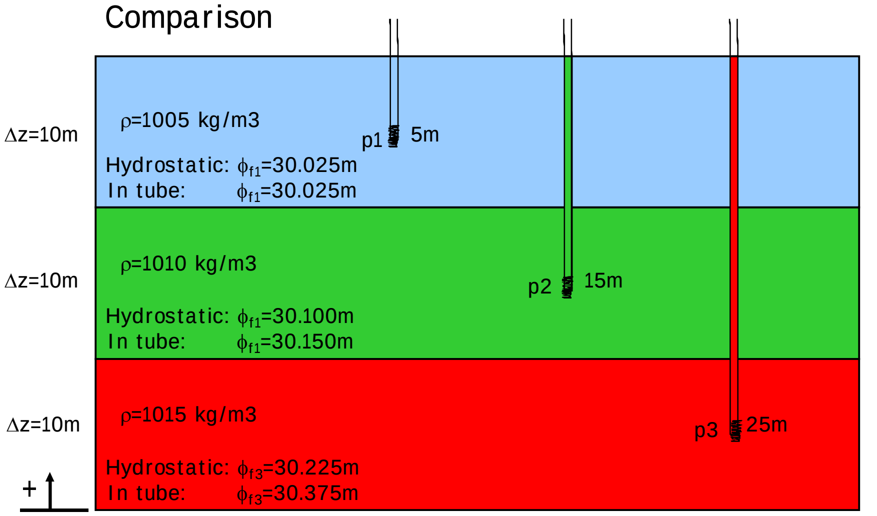
ρ=1015 kg/m3

$p_3=\rho_3 gh_3=1015*10*25=253750\ N/m^2$

$\phi_{f3}=p_3/\rho_f g+z_3=30.375m$

1. Determine hydrostatic pressure (and freshwater head ϕ_f)
2. Determine pressure p <u>in</u> well! (and freshwater head ϕ_f)

Comparison



Δz=10m

ρ=1005 kg/m3

p1 5m

Hydrostatic: ϕ_{f1}=30.025m
In tube: ϕ_{f1}=30.025m

Δz=10m

ρ=1010 kg/m3

p2 15m

Hydrostatic: ϕ_{f1}=30.100m
In tube: ϕ_{f1}=30.150m

Δz=10m

ρ=1015 kg/m3

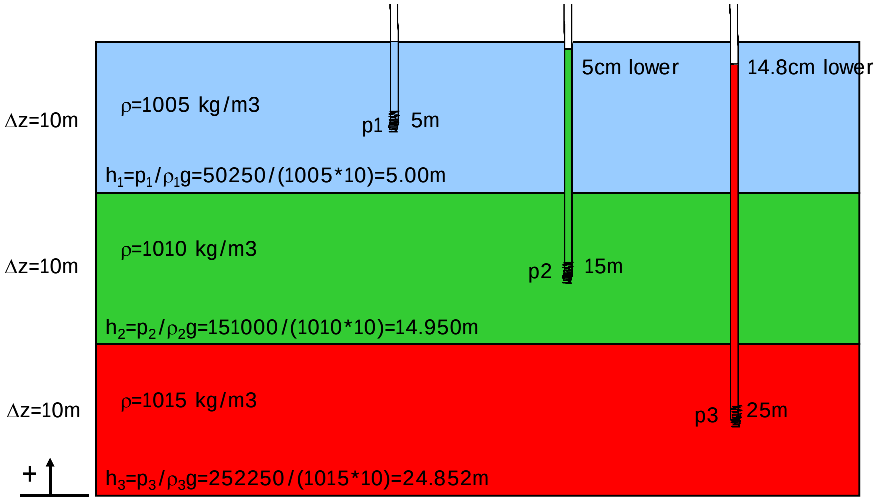
p3 25m

Hydrostatic: ϕ_{f3}=30.225m
In tube: ϕ_{f3}=30.375m

+

Conclusion: freshwater head not equal, so vertical upward flow!

What would be the water level in the tube if hydrostatic?



5cm lower

14.8cm lower

Δz=10m

ρ=1005 kg/m3

p1 5m

$h_1=p_1/\rho_1 g$=50250/(1005*10)=5.00m

Δz=10m

ρ=1010 kg/m3

p2 15m

$h_2=p_2/\rho_2 g$=151000/(1010*10)=14.950m

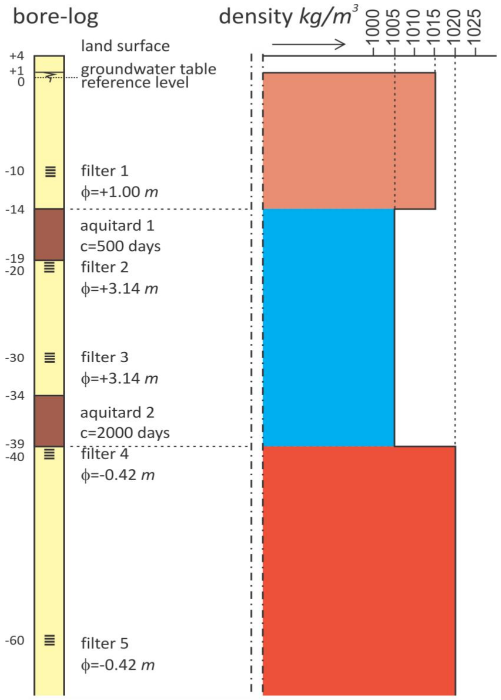
Δz=10m

ρ=1015 kg/m3

p3 25m

+

$h_3=p_3/\rho_3 g$=252250/(1015*10)=24.852m

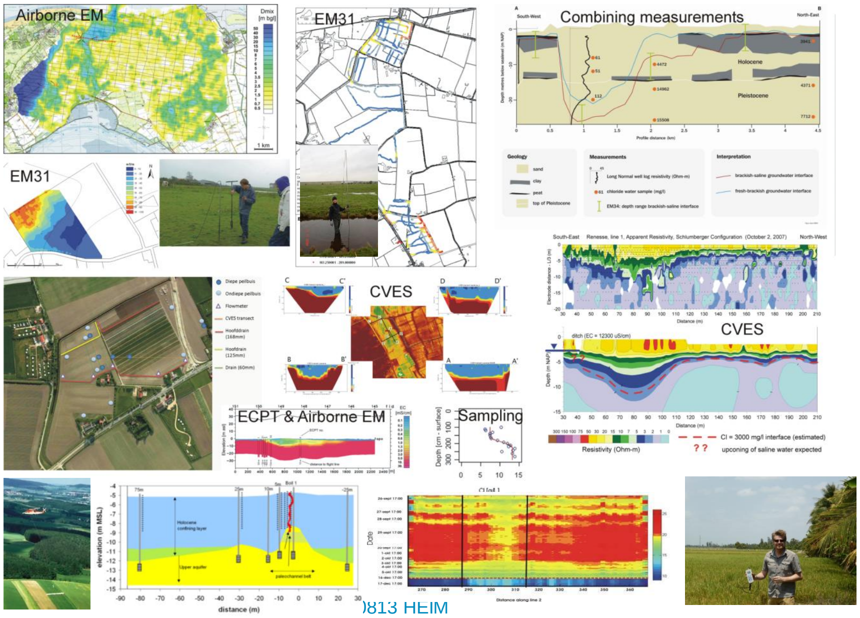


Take home message

1. In coastal area (with fresh-brackish-saline groundwater), always measure head and Electrical Conductivity (EC)
2. Convert EC to density
3. Determine freshwater head with lecture notes and ppt
4. Determine flow

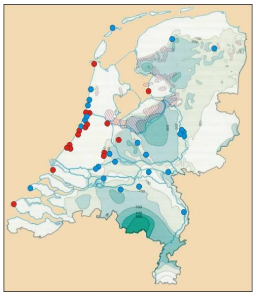
Monitoring

Different (fresh-salt) monitoring techniques



Monitoring salt in groundwater

- Why monitoring?
  - Mapping salt concentrations in the groundwater
  - Detection of trends (upconing near pumping stations)
  - System and process knowledge
  - Input for a groundwater model



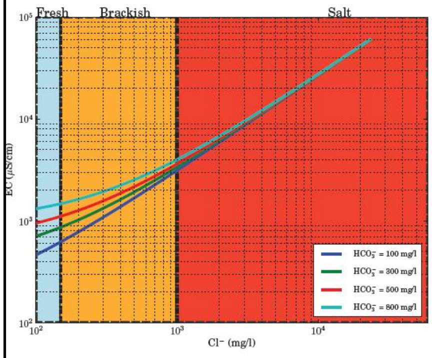
● Pumping stations with salinisation

● Pumping stations closed due to salinisation

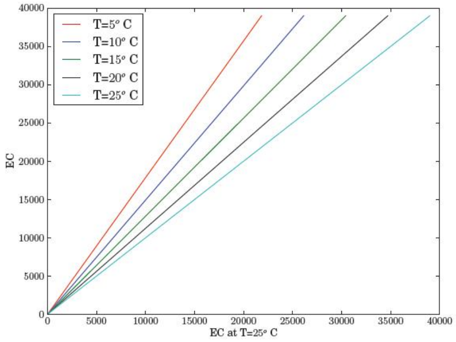
- Methods:
  1. Direct: water sample available
  2. Indirect: conductance of the subsoil

Source: V. Post, 2007

EC and Chloride



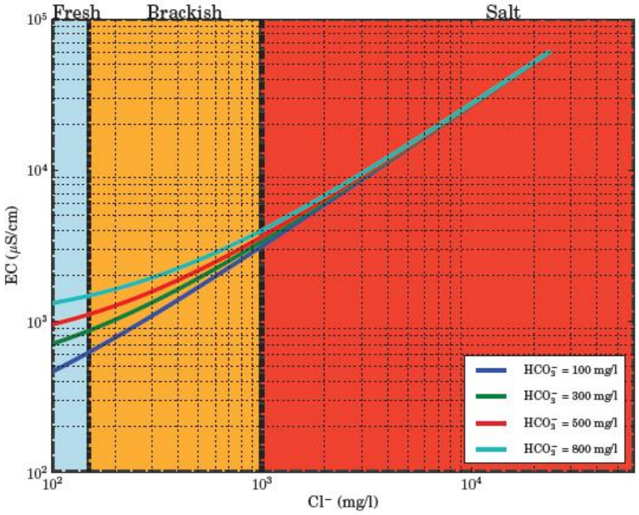
EC-Cl at different HCO_3^- concentrations.



(b) EC and temperature standardized EC.

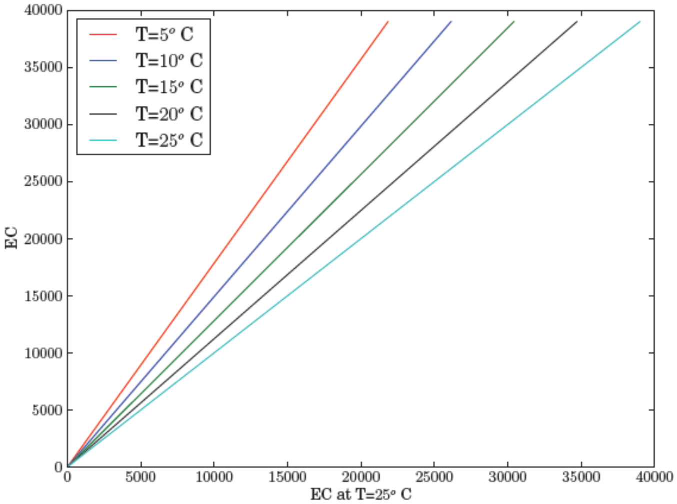
P. Pauw, 2009

EC and Chloride

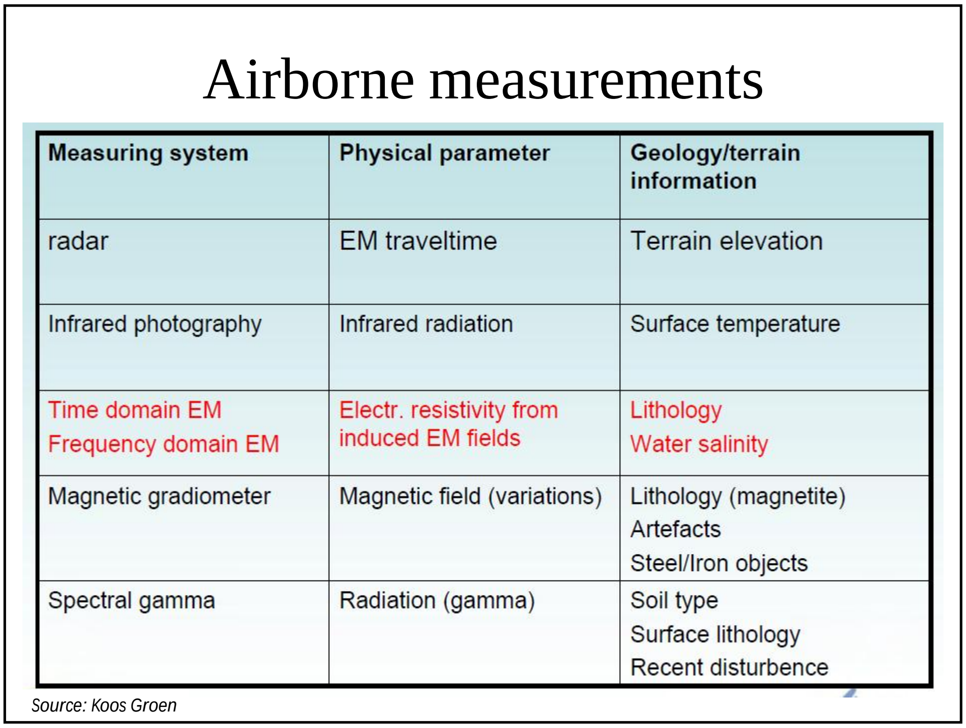


201206 EC-Cl at different HCO_3^- concentrations.

EC and Chloride



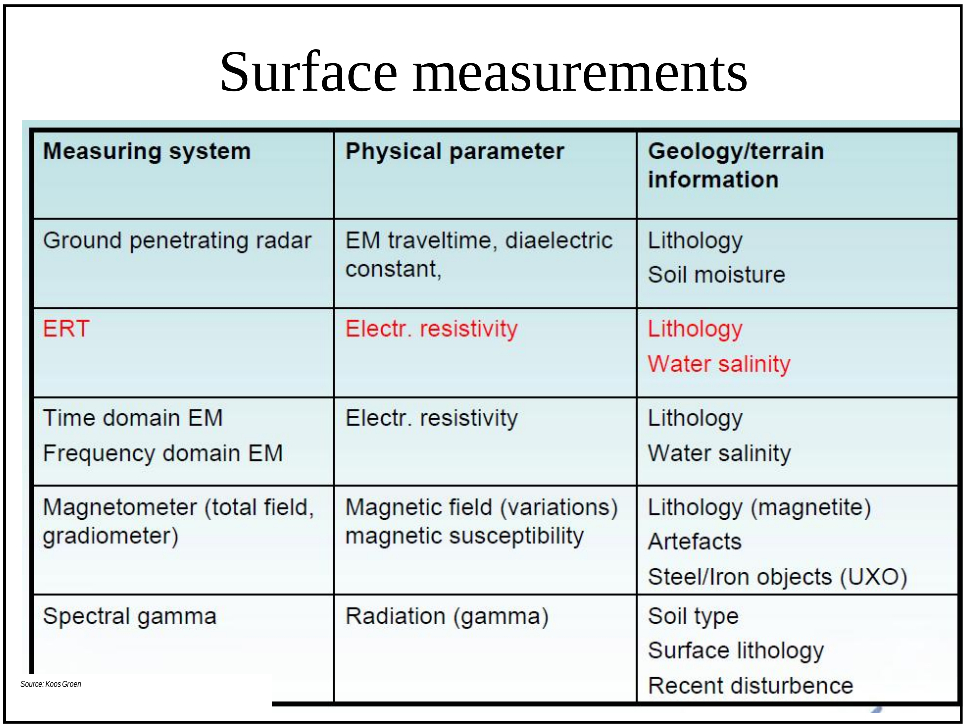
2 (b) EC and temperature standardized EC.



Airborne measurements

Measuring system	**Physical parameter**	**Geology/terrain information**
radar	EM traveltime	Terrain elevation
Infrared photography	Infrared radiation	Surface temperature
Time domain EM Frequency domain EM	Electr. resistivity from induced EM fields	Lithology Water salinity
Magnetic gradiometer	Magnetic field (variations)	Lithology (magnetite) Artefacts Steel/Iron objects
Spectral gamma	Radiation (gamma)	Soil type Surface lithology Recent disturbence

Source: Koos Groen



Surface measurements

Measuring system	**Physical parameter**	**Geology/terrain information**
Ground penetrating radar	EM traveltime, diaelectric constant,	Lithology Soil moisture
ERT	Electr. resistivity	Lithology Water salinity
Time domain EM Frequency domain EM	Electr. resistivity	Lithology Water salinity
Magnetometer (total field, gradiometer)	Magnetic field (variations) magnetic susceptibility	Lithology (magnetite) Artefacts Steel/Iron objects (UXO)
Spectral gamma	Radiation (gamma)	Soil type Surface lithology Recent disturbence

Source: Koos Groen

Cone Penetration Tests

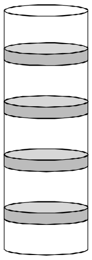
Measuring system	Physical parameter	Geology/terrain information
mechanical CPT	Cone resistance Friction resistance	Lithology Geotechnical parameters
Electrical conductivity	Electrical formation conductivity	Water salinity
Contnuous water pressure	Water pressure	Lithology Piezometric head
Water pressure dissipation in clay layers	Water pressure in time	Permeability clays
BAT sampling in CPT casing		Water chemistry
ROST, MIP		Contamination of hydrocarbons (high concentration)
Camera sonde	Visual view	Lithology, contamination, gas

Source: Koos Groen

Monitoring salt in groundwater: Direct methods

Method	Advantage	Disadvantage
1. Observation well	•High accuracy •Detection trends	•Costly •Point measurement
2. Well screens in observation well	•High accuracy •Detection trends •High vertical resolution	•Costly
3. Sediment sample (extraction milliliters of water)	•High accuracy •High vertical resolution	•Very costly and time consuming

Direct methods 1 and 2



Source: V. Post, 2007

Monitoring salt in groundwater: Indirect methods

Indirect methods measure the **conductance** of:

1. **The groundwater**
   - High conductance: saline groundwater
   - Low conductance: fresh groundwater

AND

2. **The soil**
   - High conductance: clay, sand
   - Low conductance: coarse sand, gravel

Hence information about the lithology (sand, clay etc) is needed!

Source: V. Post, 2007

Monitoring salt in groundwater: Indirect methods

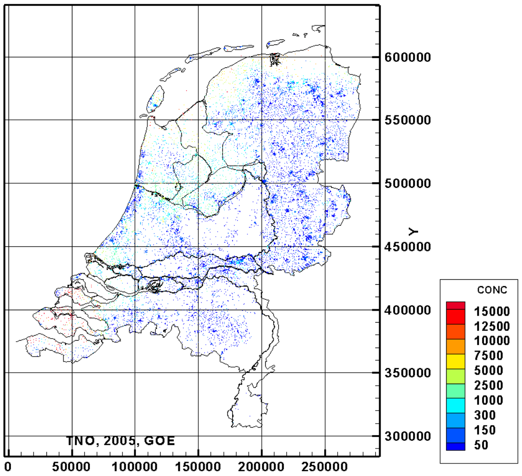
Method	**Advantages**	**Disadvantages**
1. Electrical conductance measurements	•High resolution (3D) •Depth ~200 m	•Time consuming
2. Electromagnetic measurements	•Fast	•Limited vertical resolution •Sensitive for underground conductors (pipes)
3. Satellites	•Suitable for large areas	•Small vertical resolution •Low accuracy

Source: V. Post, 2007

Method used at Deltares

Combination of:
- Direct measurements
- Electrical conductance measurements
  - Surface (VES)
  - Borehole

Number of measurements bottom Holocene top layer : direct methods and Vertical Electric Soundings (VES)



Source: Oude Essink et al (2005)

Electrical conductance measurements

1. Measuring:
   - **Inside a borehole**
   - From surface level
   - From the air

Source: TNO

Source: V. Post, 2007

Electrical conductance measurements

1. Measuring:
   - Inside a borehole
   - **From surface level (depth ~ 200 m)**
   - From the air

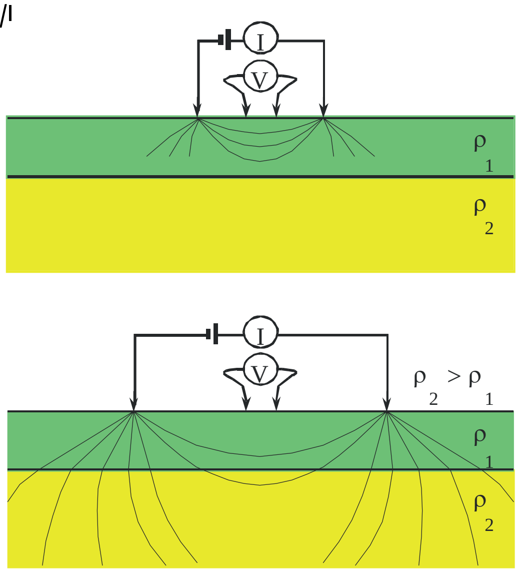
Source: Vitens

Source: V. Post, 2007

Principle geo-elektrical measurement

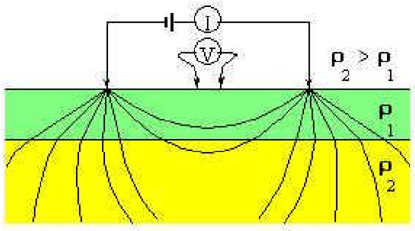
I: currentelektrode, V: potentialelektrodes, Ra: appearant elektrical resistiuvity

Ra = constant * V/I

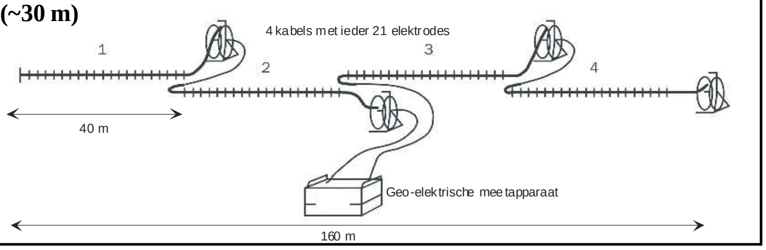


Types geo-electrical measurements

- I Vertical Electrical Sounding (VES)
- **4 elektrodes at surface**
- **1D elektrical resistivity profile**
- **Labor intense**
- **Accurate, great depths**
- **Deep hydrogeology**



- II Continue Vertical Elektrical Sounding (CVES)
- **>80 elektrodes at surface**
- **2D elektrical resistivity subsurface**
- **Limited depth (~30 m)**

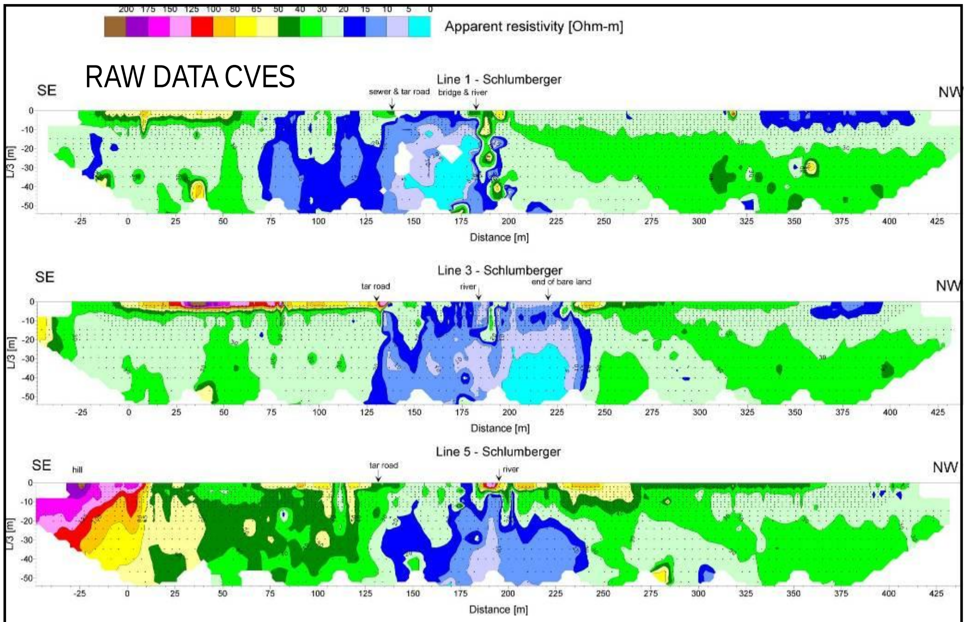


20120622 SW

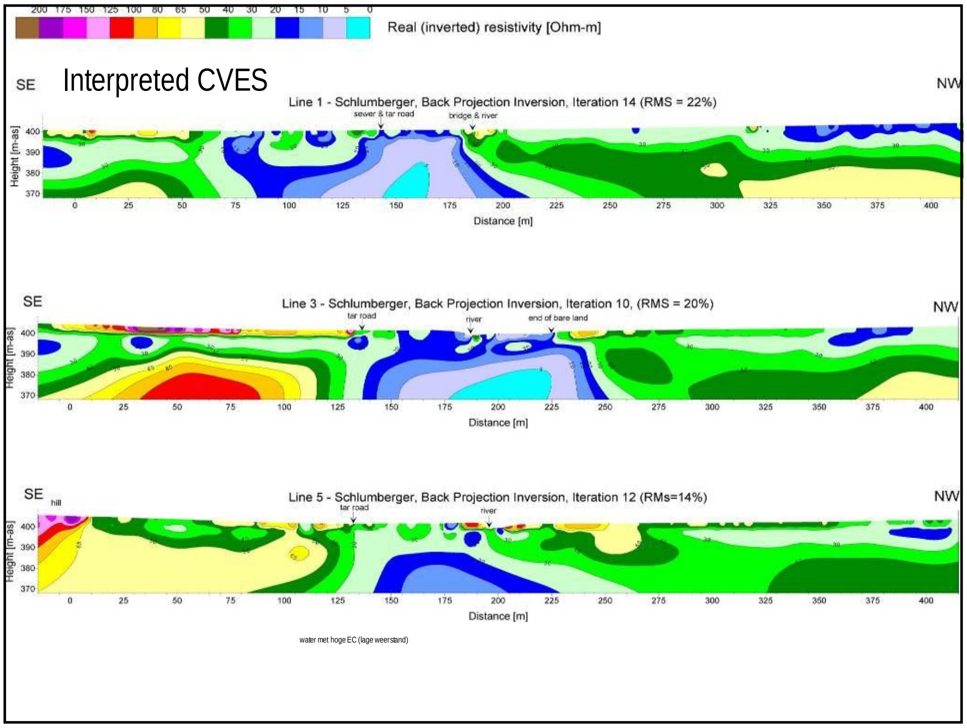
VES measurement end 1950s/begin 1960s

CVES
measurements 2010s

RAW DATA CVES



water met hoge EC (lage weerstand)



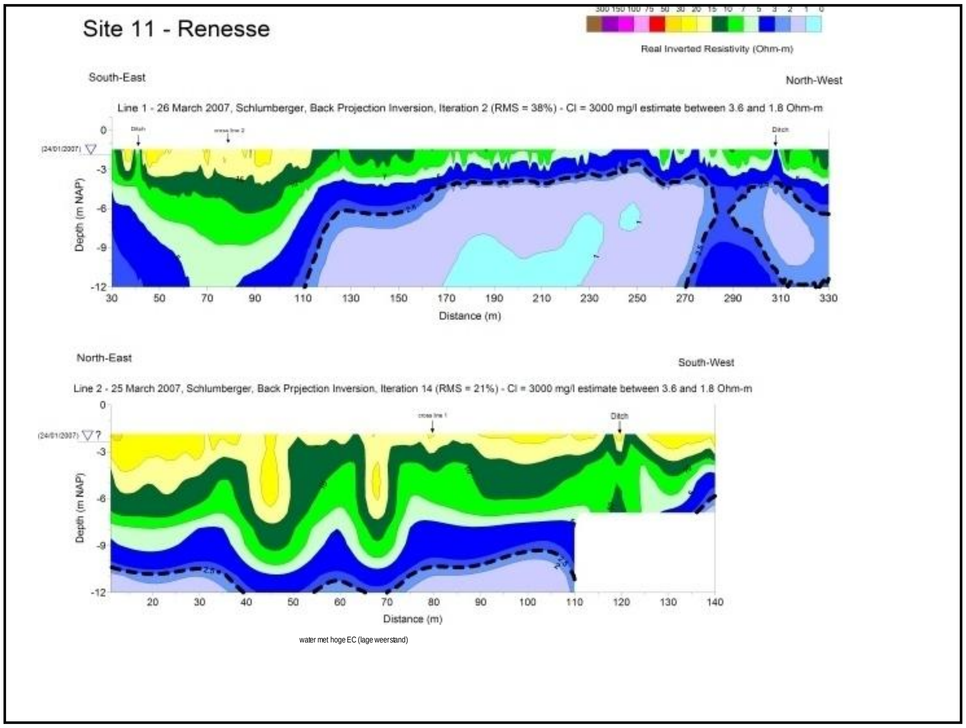
Interpreted CVES

Line 1 - Schlumberger, Back Projection Inversion, Iteration 14 (RMS = 22%)

Line 3 - Schlumberger, Back Projection Inversion, Iteration 10, (RMS = 20%)

Line 5 - Schlumberger, Back Projection Inversion, Iteration 12 (RMs=14%)

water met hoge EC (lage weerstand)



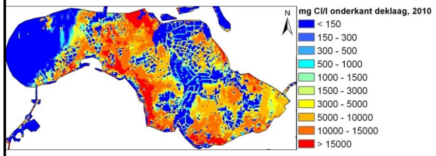
Site 11 - Renesse

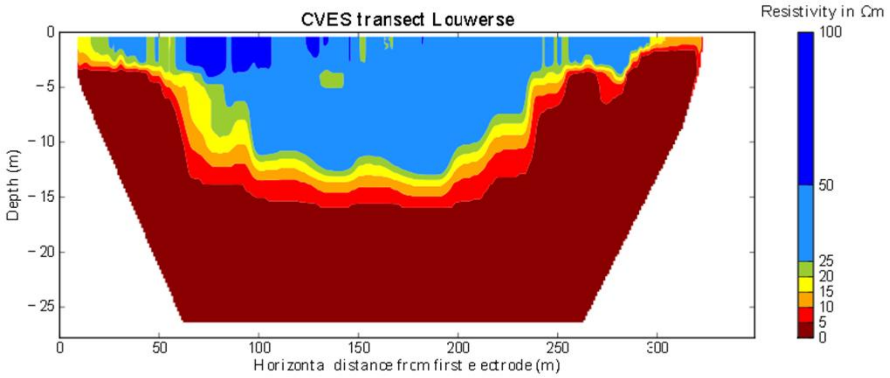
Line 1 - 26 March 2007, Schlumberger, Back Projection Inversion, Iteration 2 (RMS = 38%) - Cl = 3000 mg/l estimate between 3.6 and 1.8 Ohm-m

Line 2 - 25 March 2007, Schlumberger, Back Prpjection Inversion, Iteration 14 (RMS = 21%) - Cl = 3000 mg/l estimate between 3.6 and 1.8 Ohm-m

water met hoge EC (lage weerstand)

Possible measures for sandy creeks





Monitoring salt in groundwater: Indirect methods

- Electrical conductance measurements

$\boxed{\rho_s = F^* \rho_w}$

ρ_s = resistance subsoil & groundwater
ρ_w = resistance groundwater
F = formation factor

Lithology	**F**
Gravel with sand	7
Coarse sand	5
Sand with silt	2 - 3
Clay	*1-3**
peat	*1**

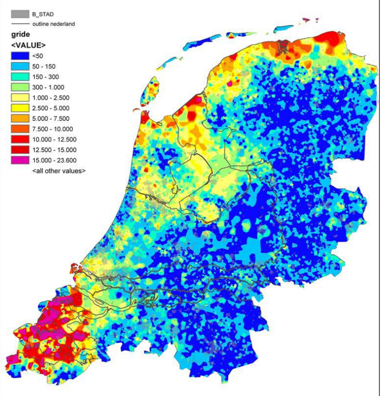
} → *F varies with the resistance of the groundwater*

If the lithology is known AND the measurement is in an aquifer
→ ρ_w can be calculated

VES measurements are used in combination with borehole logging

Source: Oude Essink, 2005

Result: chloride concentration bottom Holocene toplayer



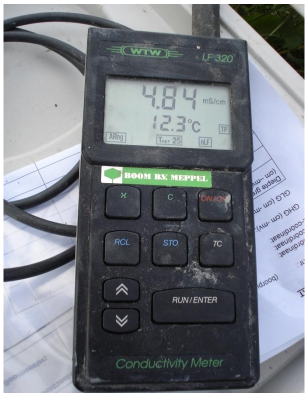
Source: Oude Essink, 2005

- Software Geological Survey of the Netherlands (TNO) is used to determine the salt concentration of the groundwater in the measurements

- Inter- and extrapolation is used to make a continuous field

- 2D Result is an combination of:
  1. Direct measurements (3500)
  2. Electrical conductance in boreholes (2000)
  3. Vertical Electric Sounding (VES) measurements (10.000)

T-EC probe



CLIWAT CLIMATE & WATER

The Interreg IVB North Sea Region Programme

WETTERSKIP FRYSLÂN

provinsje fryslân
provincie fryslân

T EC fieldwork

Altitude measurements

CLIWAT
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The Interreg IVB
North Sea Region
Programme

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FRYSLÂN

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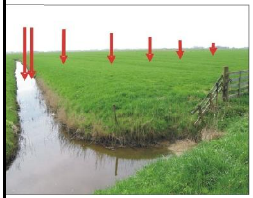
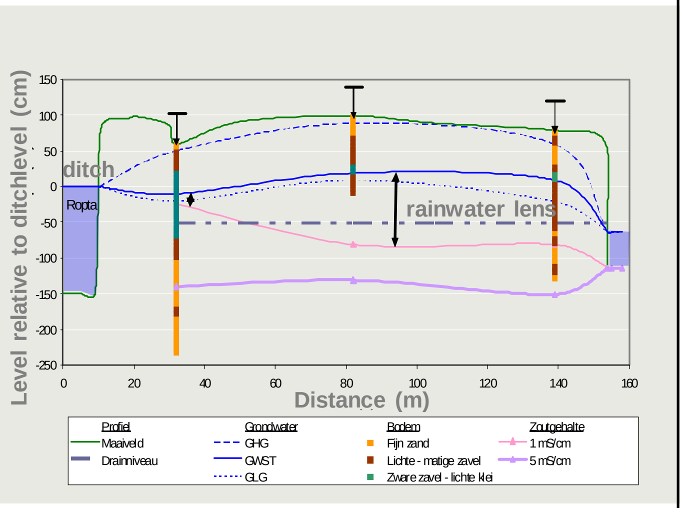
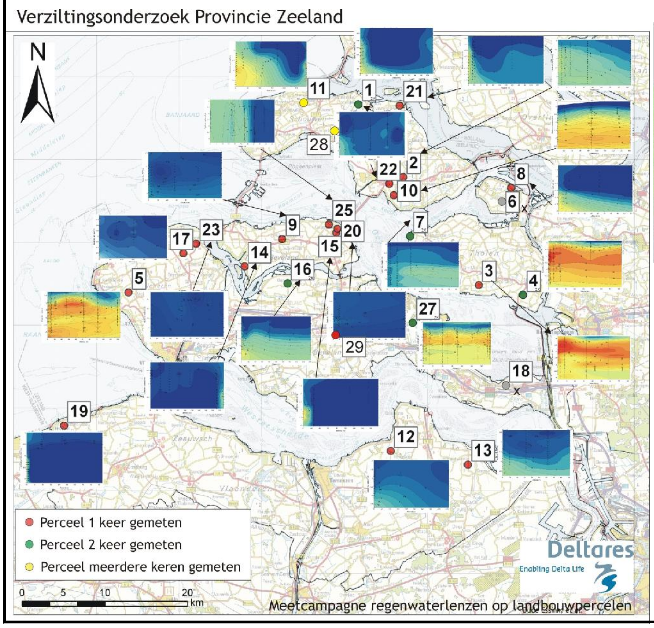
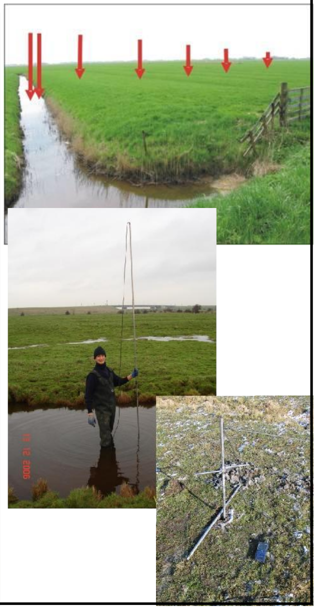
Use field measurements to understand the process





TEC-probe Monitoring campaign 2005-2009

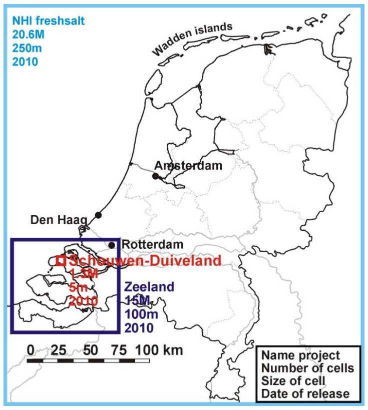


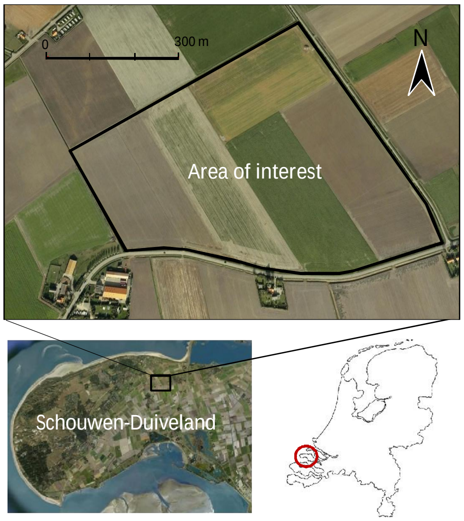


CliWat www.cliwat.eu

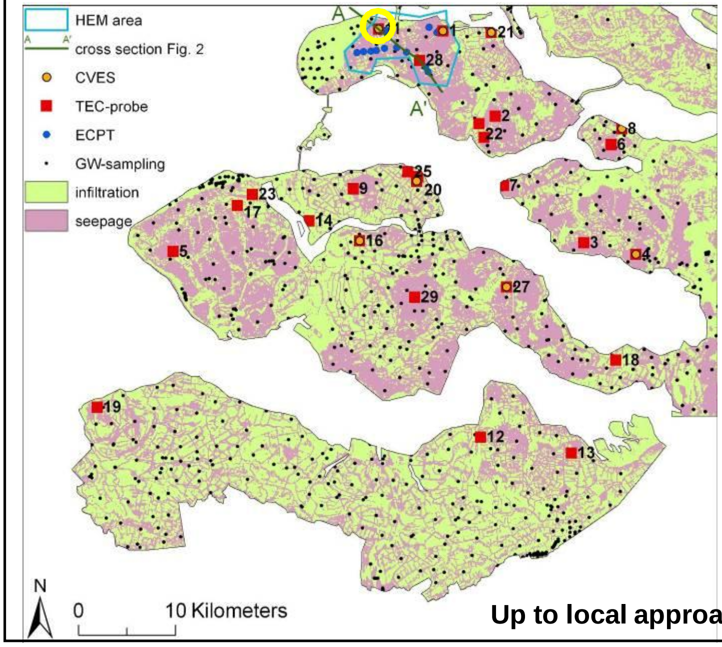
- Transnational project in the North Sea Region
- Main objectives:
  - to evaluate the physical and chemical impacts of climate change on groundwater and surface water systems
  - to provide data for adaptive and sustainable water management and infrastructure.
- Different innovative monitoring techniques (Helicopter EM, CVES, CPT, TEC-probe) are used to map the salinization status of the coastal groundwater system.

Description local area





Monitoring network in our Pilot Area Zeeland



CLIWAT CLIMATE & WATER

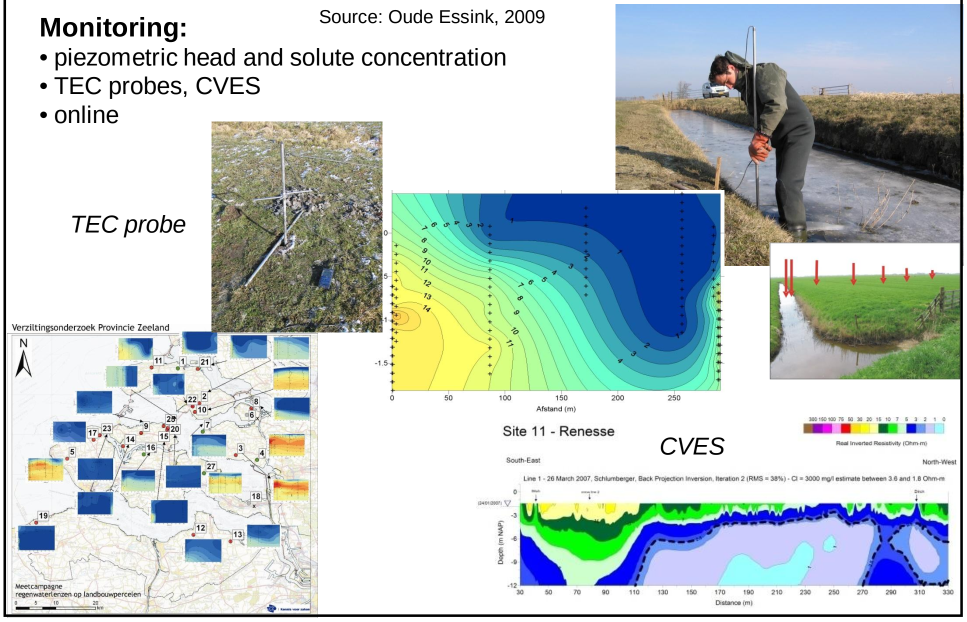
BGR Bundesanstalt für Geowissenschaften und Rohstoffe GEOZENTRUM HANNOVER

Up to local approach

Example: Assessing effect of climate change on salt water intrusion

Source: Oude Essink, 2009

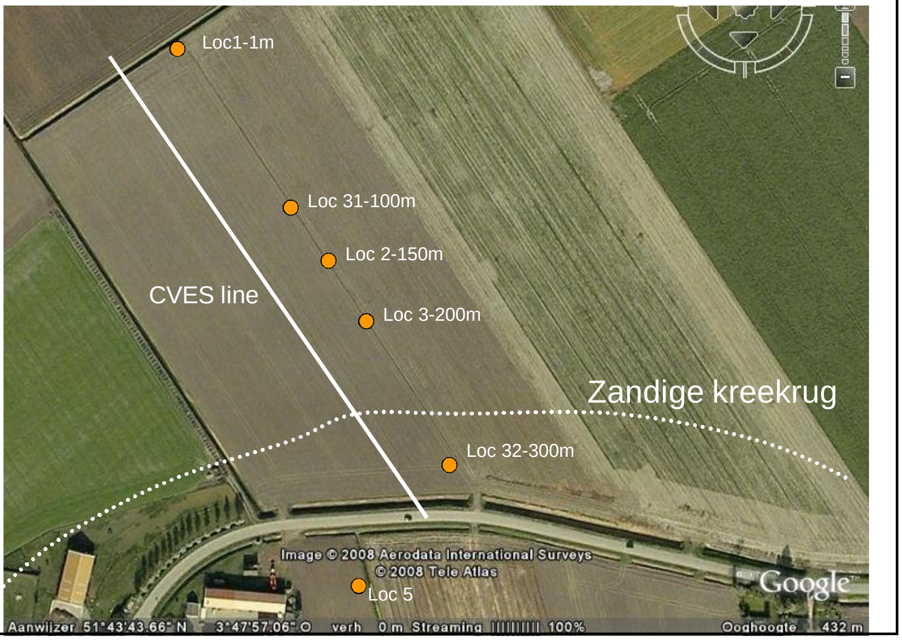
Monitoring:
- piezometric head and solute concentration
- TEC probes, CVES
- online

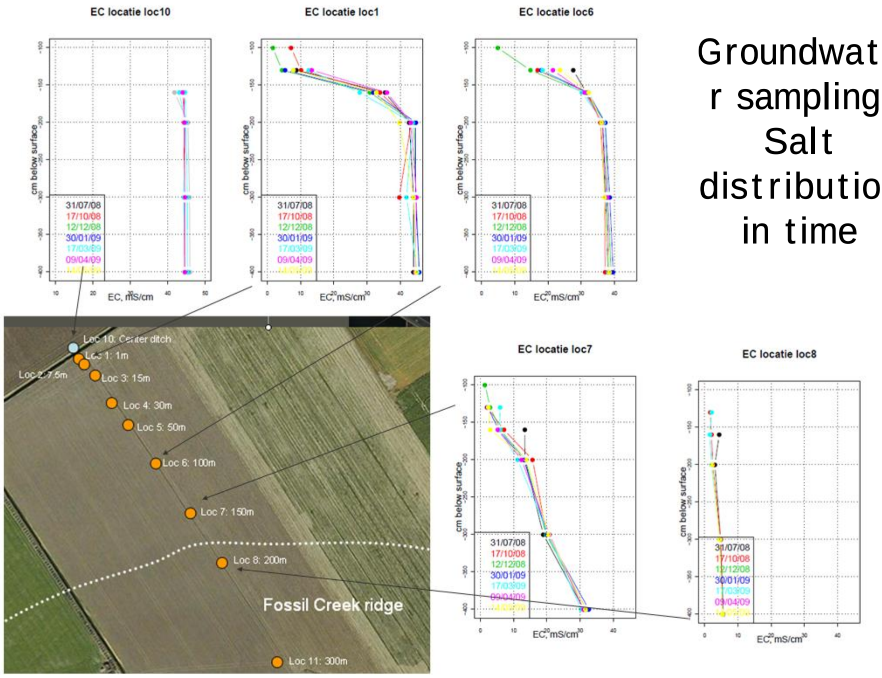


TEC probe

CVES

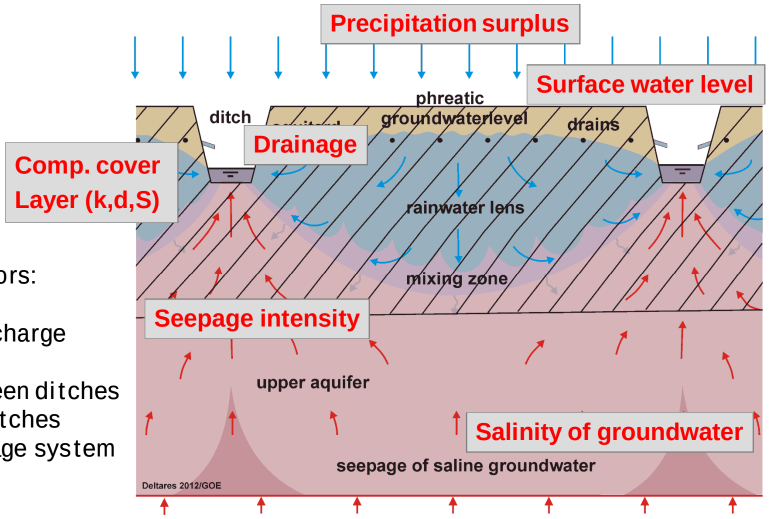
Site 11: from infiltration to seepage





Groundwater sampling: Salt distribution in time

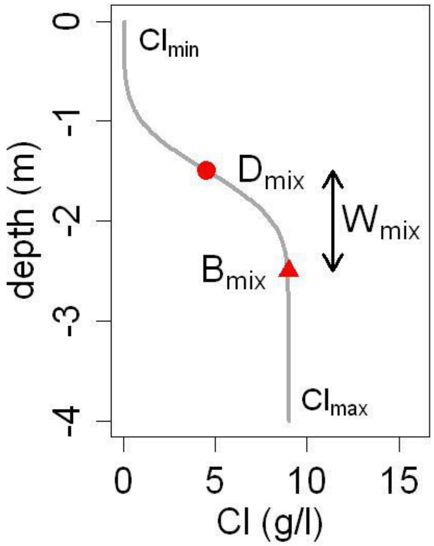
Factors controlling fresh-salt interface

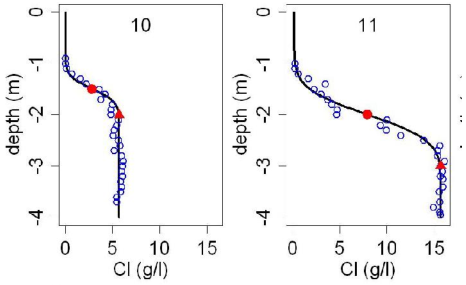


Important factors:

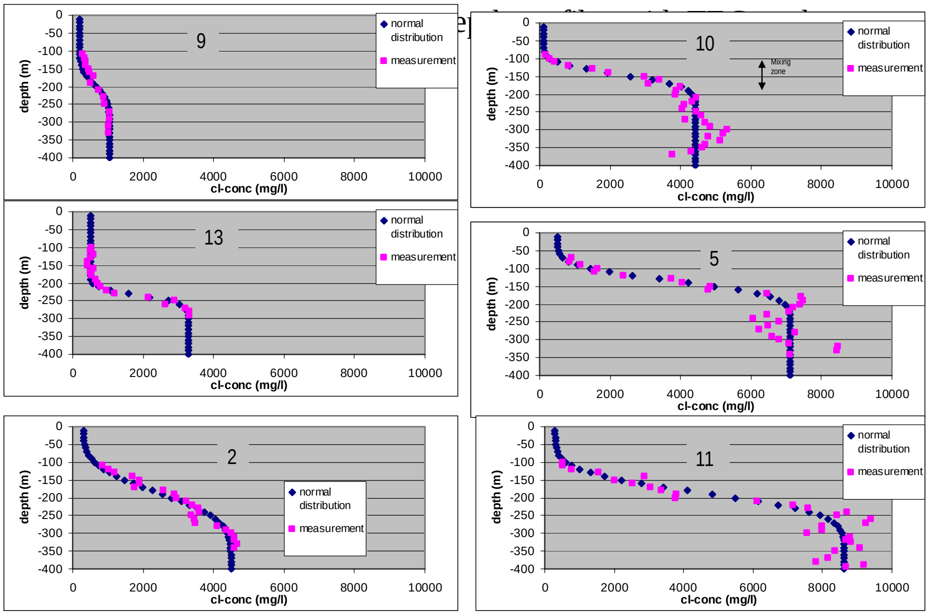
-natural grw recharge
-geology
-distance between ditches
-water levele ditches
-capacity drainage system

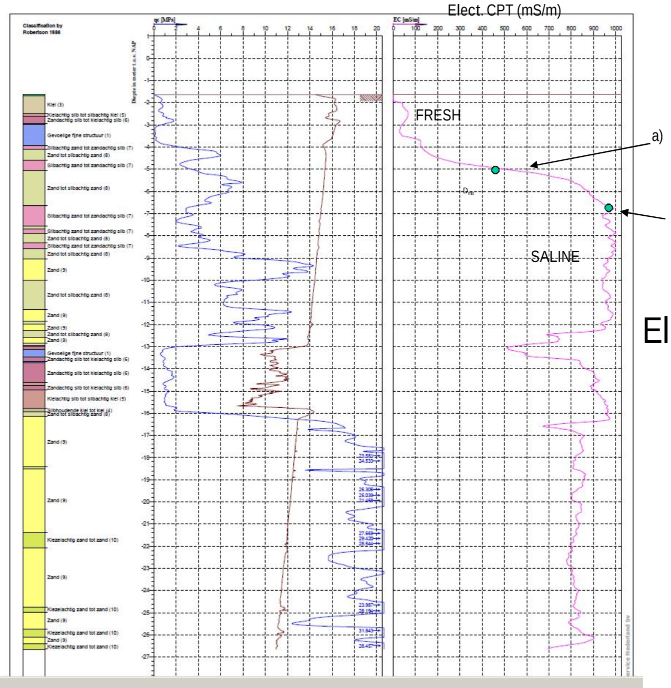
Lens characteristics





Louw, P.G.B., de, Eeman, S., Siemon, B., Voortman, B.R., Gunnink, J., Baaren, E.S., van and G.H.P. Oude Essink, Shallow rainwater lenses in deltaic areas with saline seepage, *Hydrol. Earth Syst. Sci. Discuss.*, 8, 7657-7707, 2011.



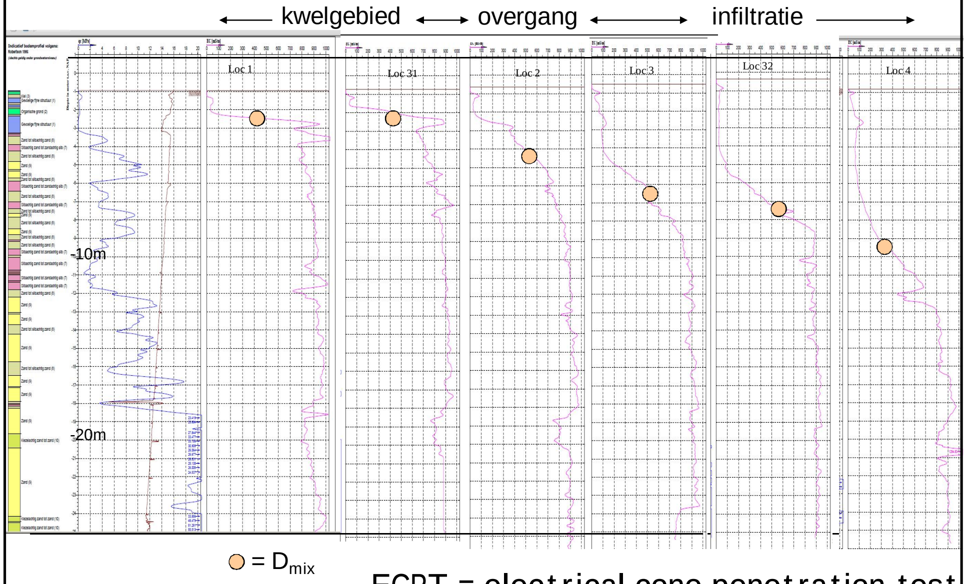


a) Depth of transition, D_{mix}, zone between 2 types of groundwater (fresh-saline)

b) Start of transition, S_{mix},

Electrical CPT

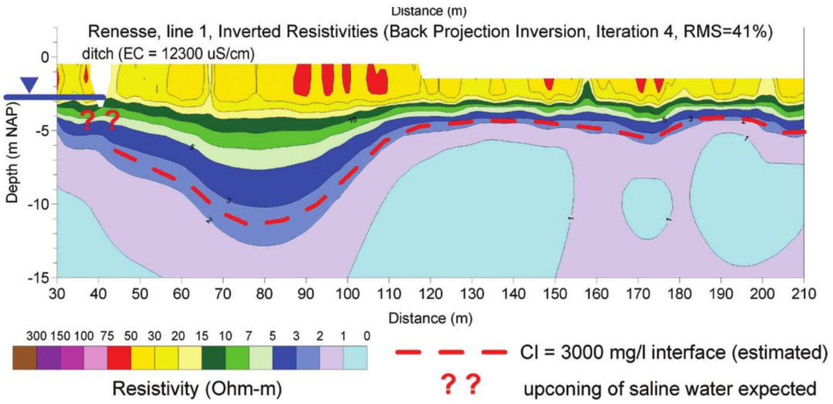
Results from ECPT's (soundings)



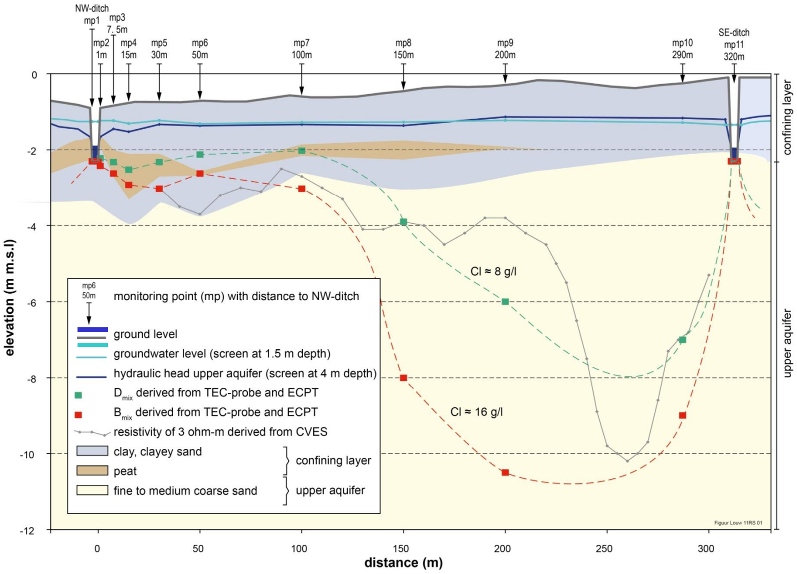
ECPT = electrical cone penetration test

CVES

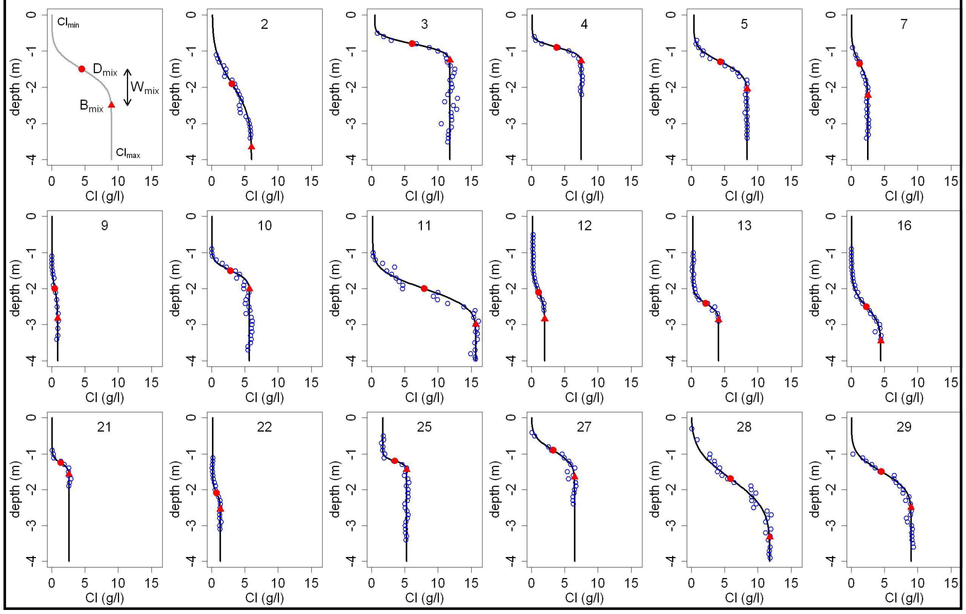
CVES: continuous vertical eletrical sounding



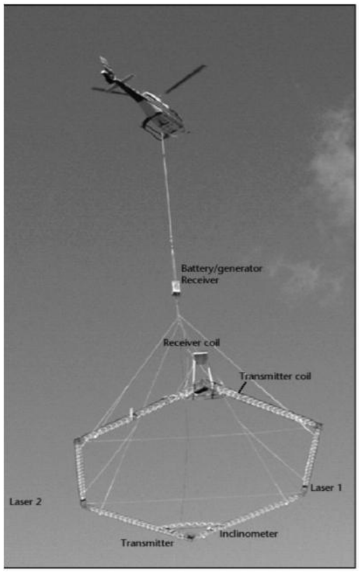
Seepage / infiltration determines thickness rainwaterlens



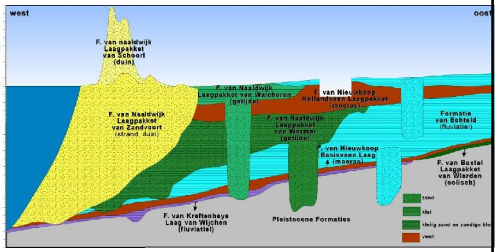
TEC-probe results



Electrical conductance measurements



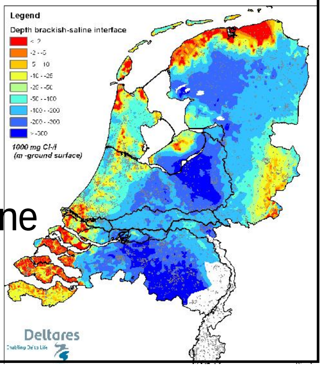
From bulk to groundwater resistivity



EC lithology

EC^{bulk}

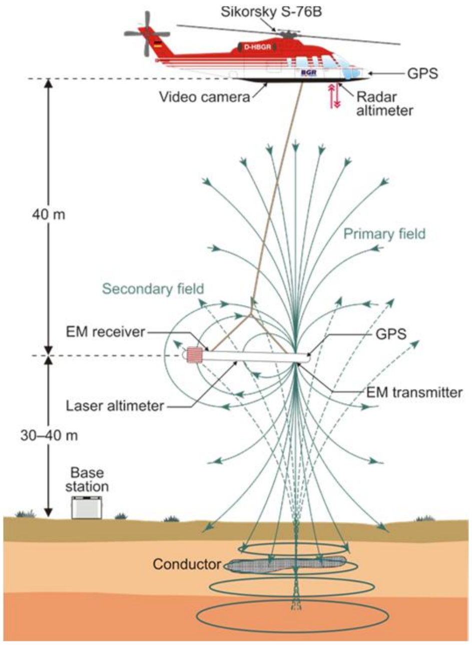
EC groundwater
→ fresh-brackish-saline



EC = Electrical Conductivity = conductivity

BGR helicopter-borne geophysical system

Airborne geophysical survey system	
Helicopter:	Sikorsky S-76B
Helicopter equipment:	GPS-Navigation GPS-Tracking Radar and barometric altimeters Video camera
Standard equipment:	Electromagnetic system Magnetometer Laser altimeter Gamma-ray spectrometer
Optional equipment:	Laser scanner Pulse radar *Stepped frequency* - Radar Gravimeter Differential GPS Photogrammetric camera Infrared camera
Base station equipment:	Magnetic total field sensor Air pressure sensor Differential GPS
Survey speed:	130 – 160 km/h
Sampling distance:	~ 4 and 40 m
Line separation	50 – 2000 m

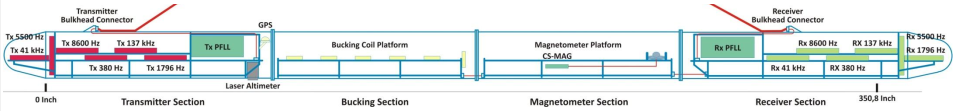


Meeting in Utrecht Feb. 25th 2014

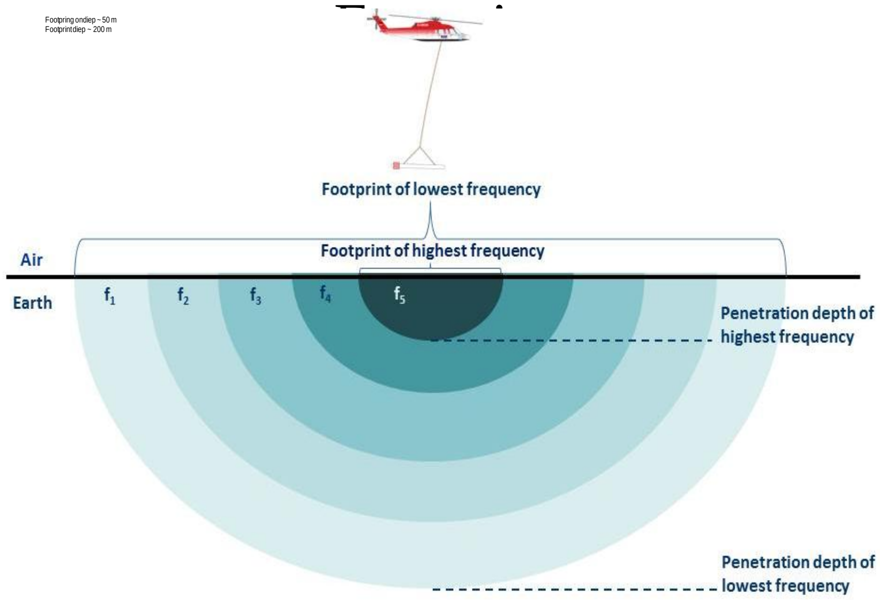
BGR helicopter-borne geophysical system

Recent six-frequency HEM system		
Type:	RESOLVE – Digital system Modified BKS36a DSP and BKS60 DSP systems	
Length:	~ 10 m	
Weight:	~ 400 kg incl. cable (80 kg)	
Manufacturer:	Fugro Airborne Systems, Canada	
Frequency [Hz]	Coil separation[m]	Geometry
387	7.94	horizontal coplanar
1820	7.93	horizontal coplanar
5500	9.06	vertical coaxial
8225	7.93	horizontal coplanar
41550	7.91	horizontal coplanar
133200	7.92	horizontal coplanar

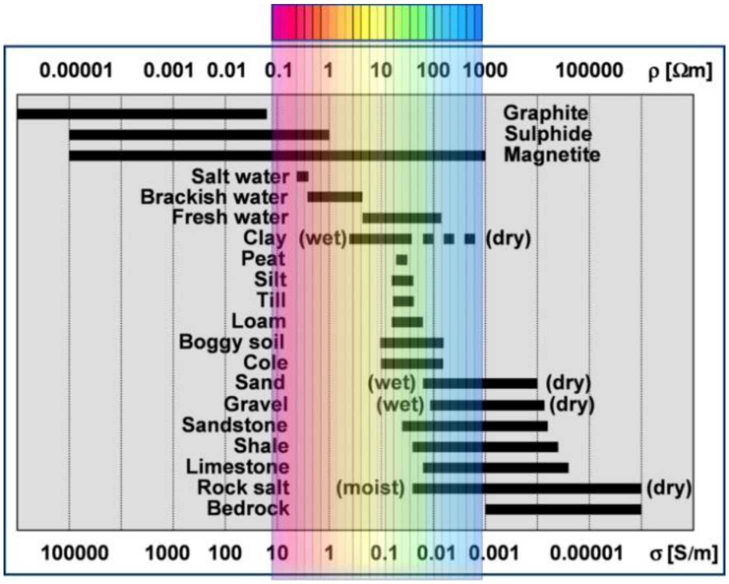

Ondiep voor hoge frequenties en/of hoge geleidbaarheid

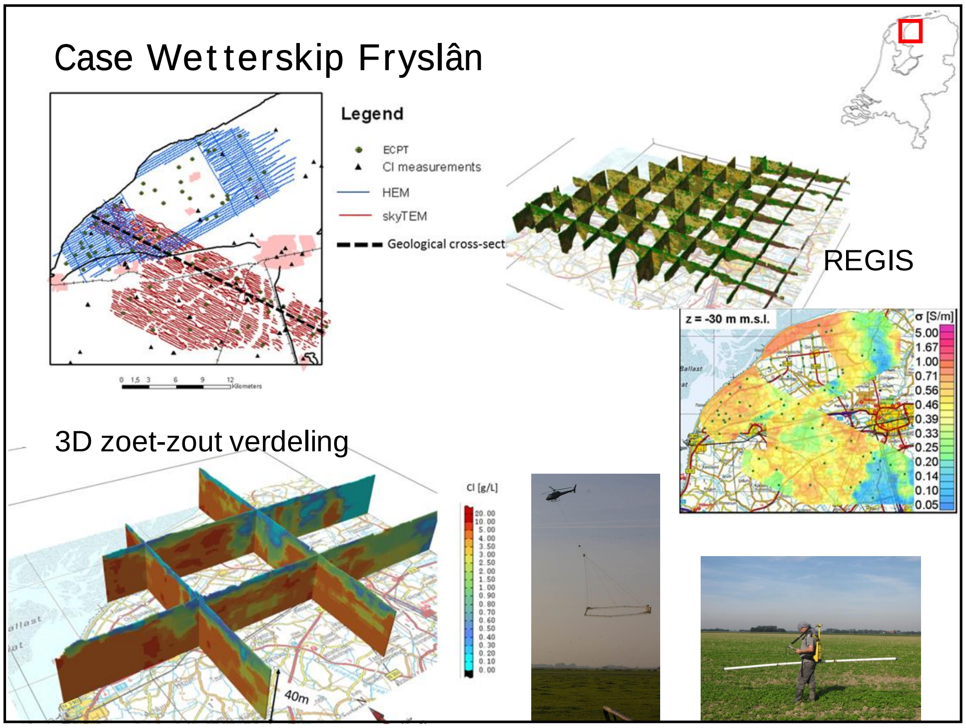


Footpring ondiep ~ 50 m
Footprint diep ~ 200 m



Typical resistivities / conductivities

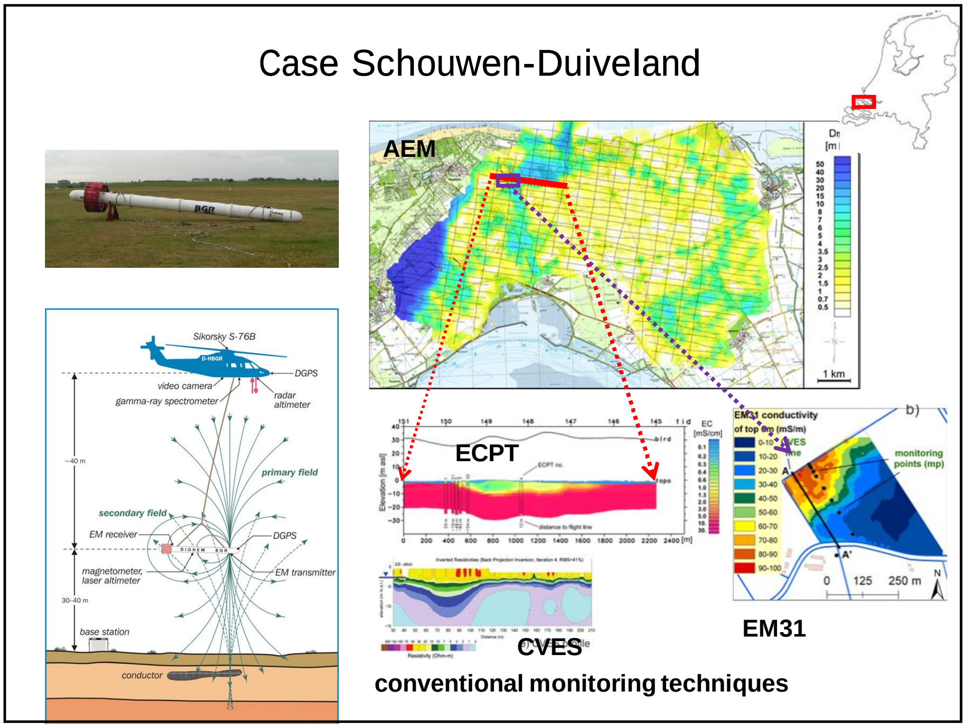




Case Wetterskip Fryslân

REGIS

3D zoet-zout verdeling



Case Schouwen-Duiveland

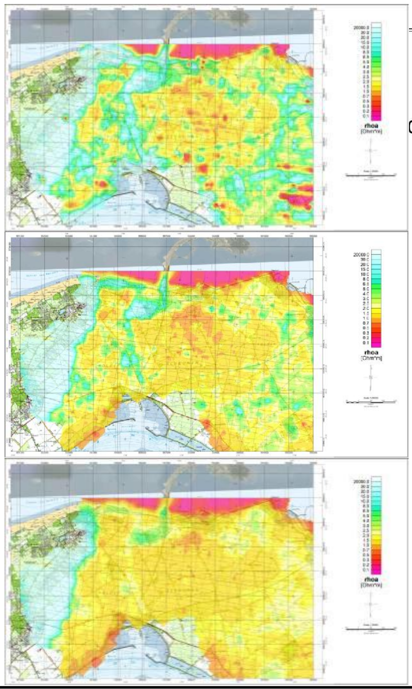
AEM

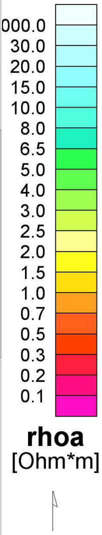
ECPT

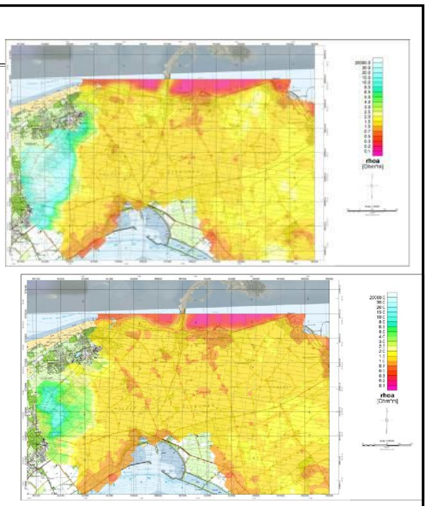
CVES

EM31

conventional monitoring techniques

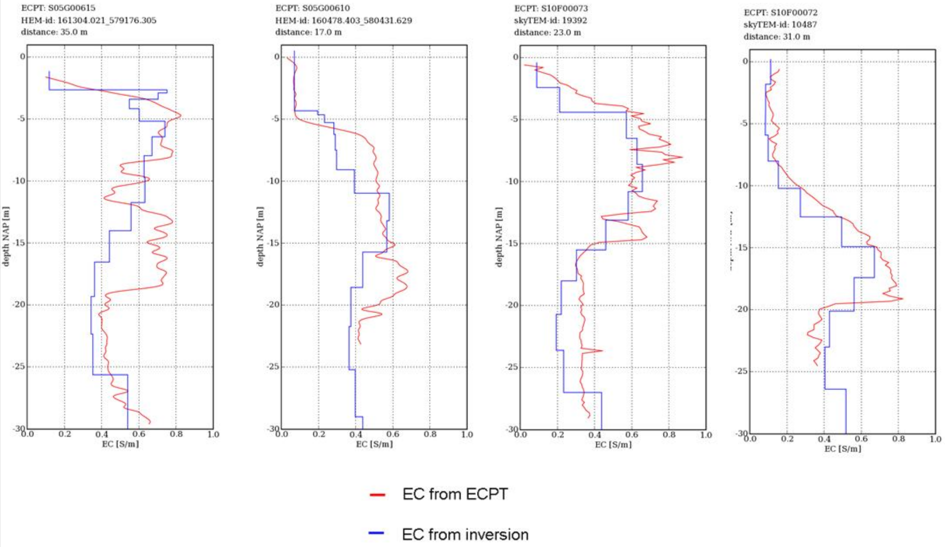






HEM results with depth

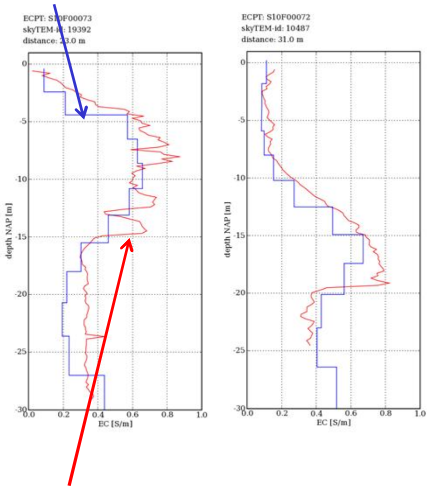
Compare Airborne EM with ECPT Case Wetterskip Fryslân



3D characterising fresh-saline groundwater

How much samples in 1 week on 900km^2?

AEM: 80000 data points

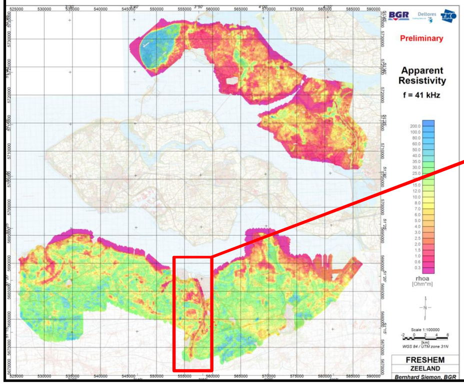


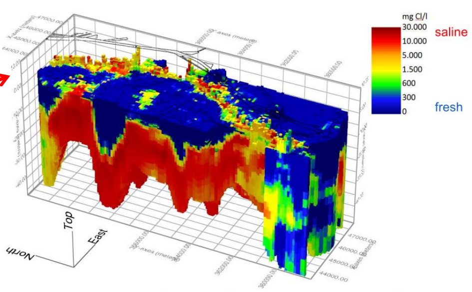
In-situ: >100 data points

3D Characterisation of the subsoil

Airborne EM surveys:
much cheaper, faster, 3D,
and as equal accurate as
conventional geophysical methods

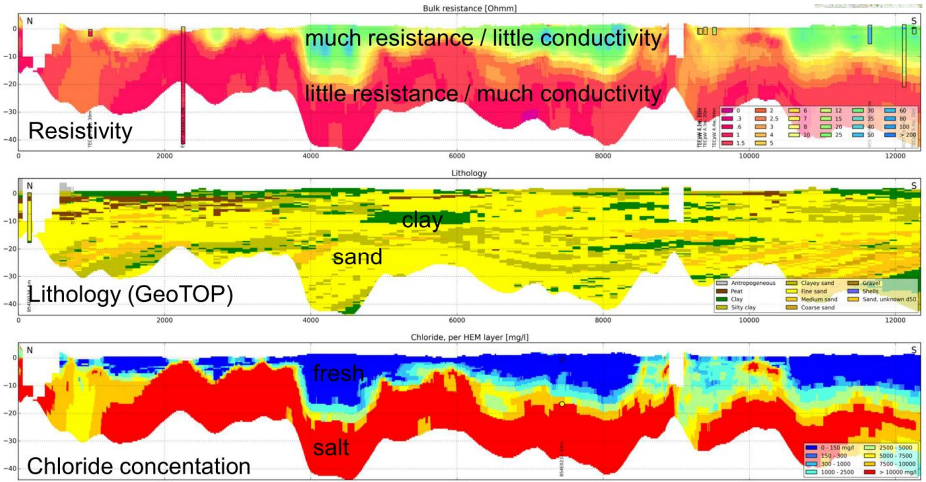
TNO innovation for life BGR Deltares Enabling Delta Life





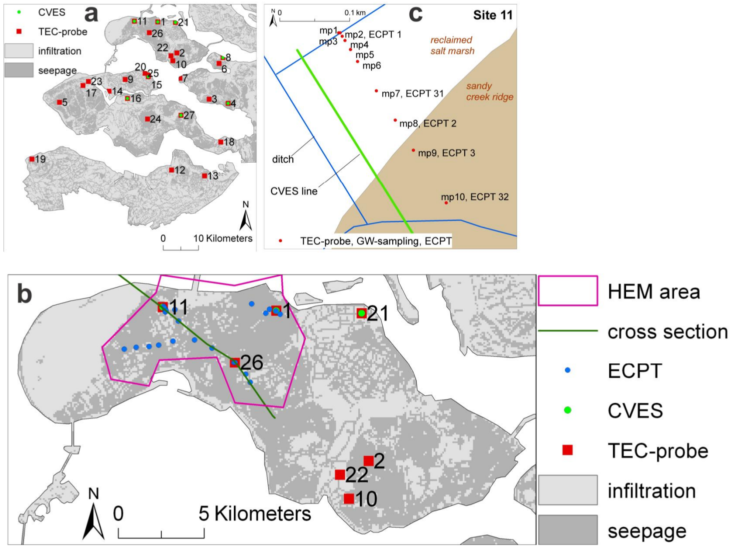
FRESHEM pilot Canal zone, visualization in iMOD

Example NL, Zeeland, project FRESHEM



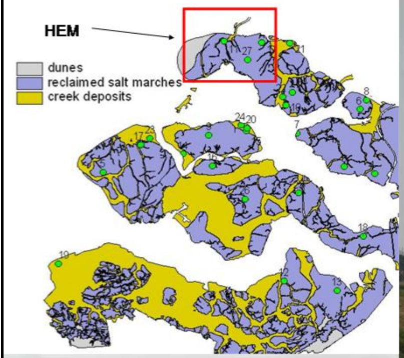
20160524 Ara Sul

Combining monitoring techniques



10 juni 2013

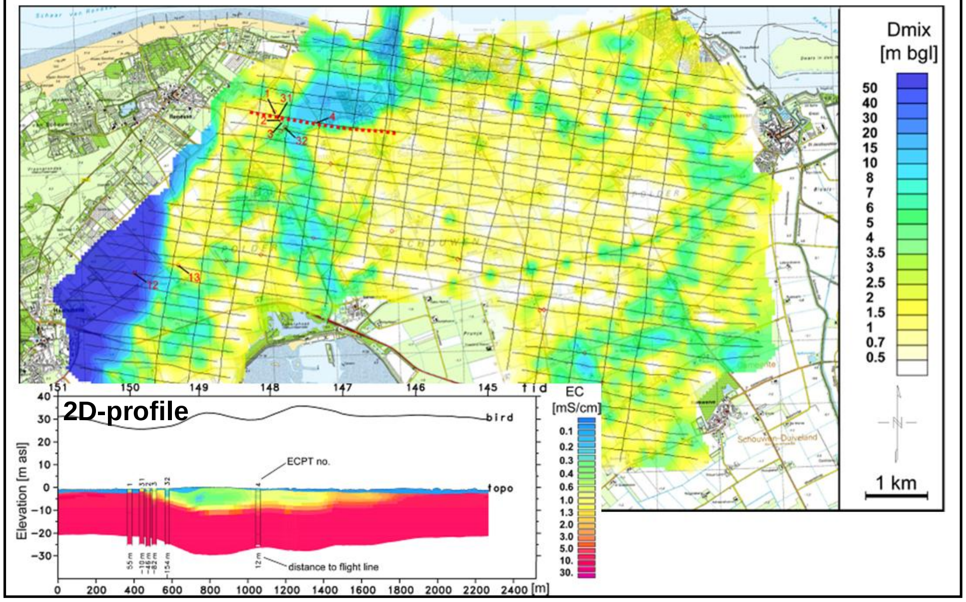
Helicopter-EM data for mapping fresh-saline groundwater



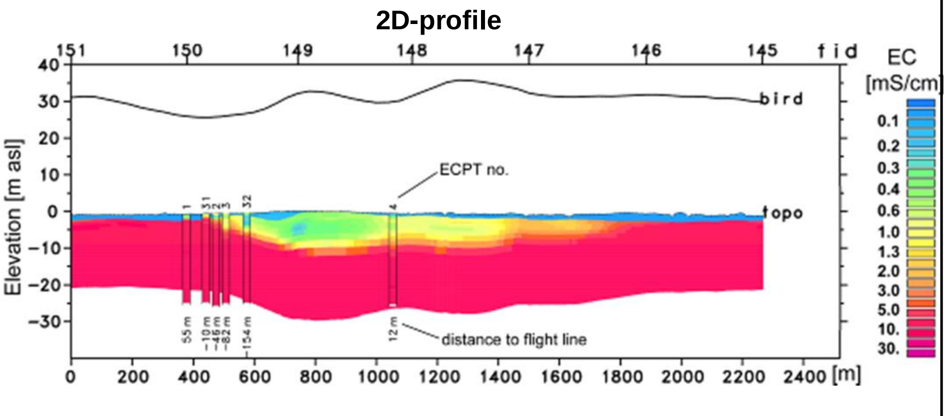
Interreg IV-B

CLIWAT
CLIMATE & WATER

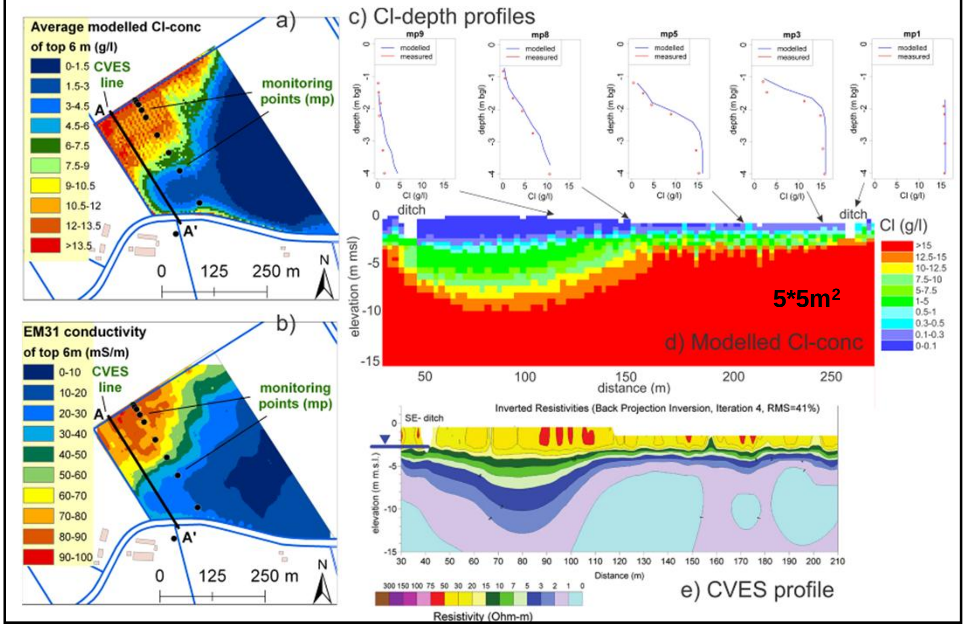
Thickness rainwater lens (D_{mix}) by HEM



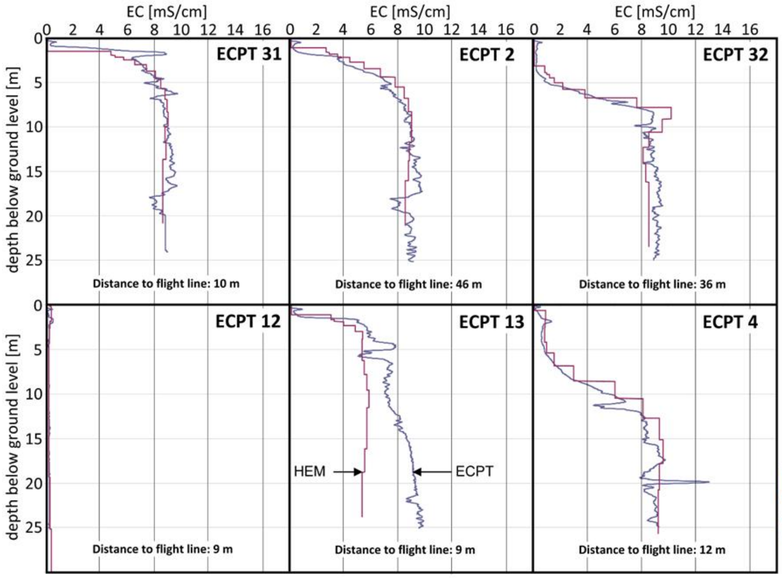
Thickness rainwater lens (D_{mix}) by HEM



Comparison monitoring data with model results

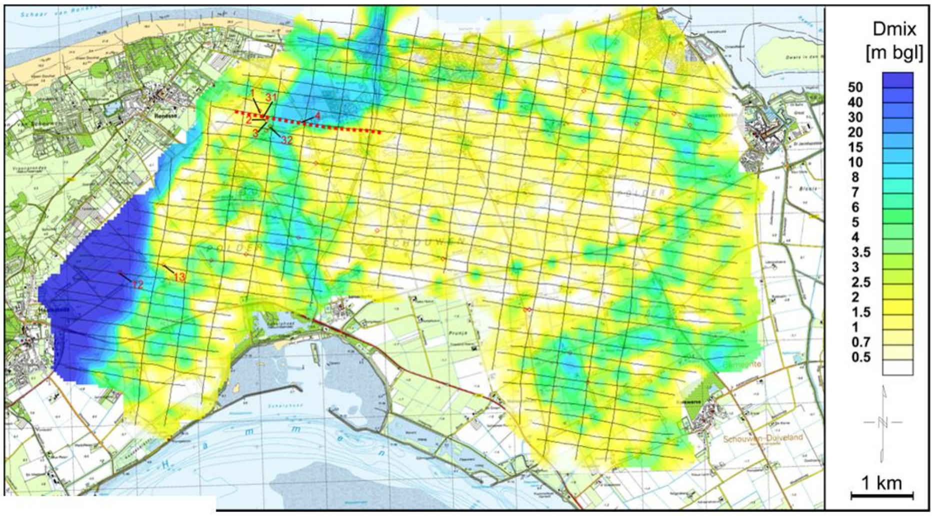


Comparison HEM – ECPT



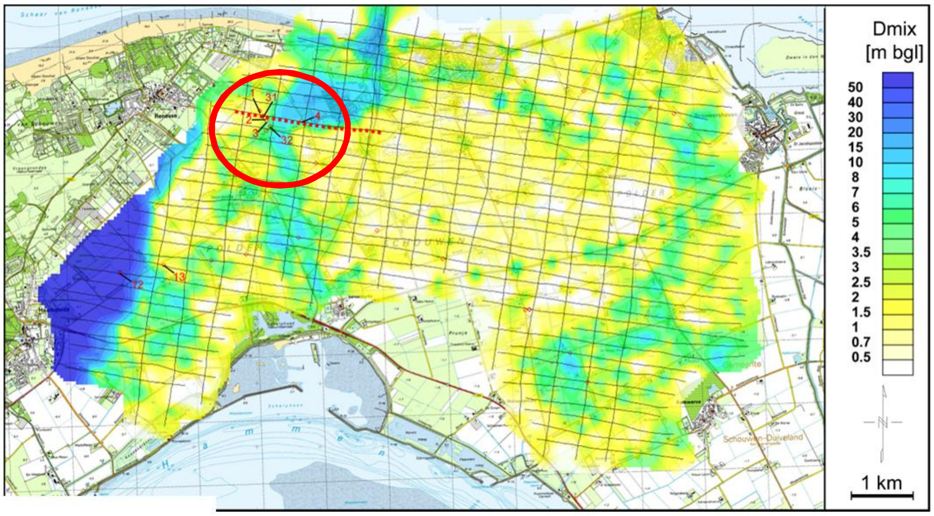
Bundesanstalt für Geowissenschaften und Rohstoffe
TRUM HANNOVER

Rainwater lens thickness (D_{mix}= average position mixing zone) mapped with HEM



BGR Bundesanstalt für Geowissenschaften und Rohstoffe
GEOZENTRUM HANNOVER

Rainwater lens thickness (D_{mix}= average position mixing zone) mapped with HEM



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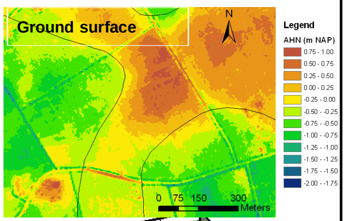
GEOZENTRUM HANNOVER

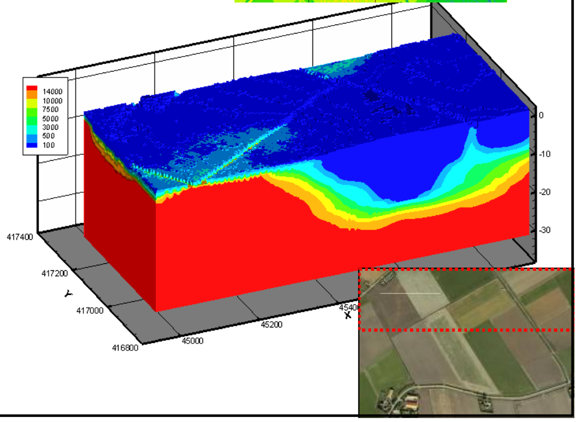
Local 3D model of the agricultural plot



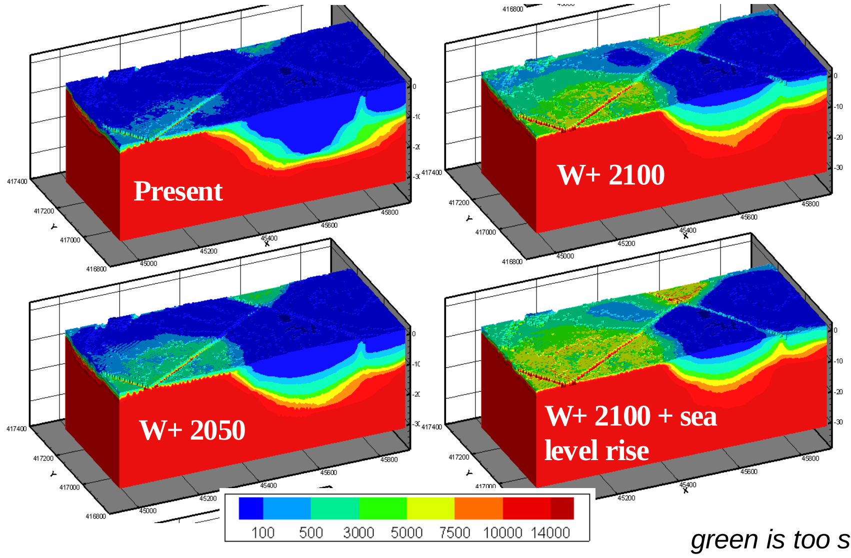
Modelling:
- variable-density
- 3D, non-steady
- groundwater flow & coupled solute transport
- model cell size: 5*5m^2

Code:
MOCDENS3D

Assessing effects:
- autonomous salinisation
- sea level rise
- changing recharge pattern
- (adaption measures)



Local approach: simulated Cl-conc. with different CC-scenarios

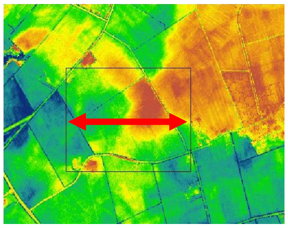


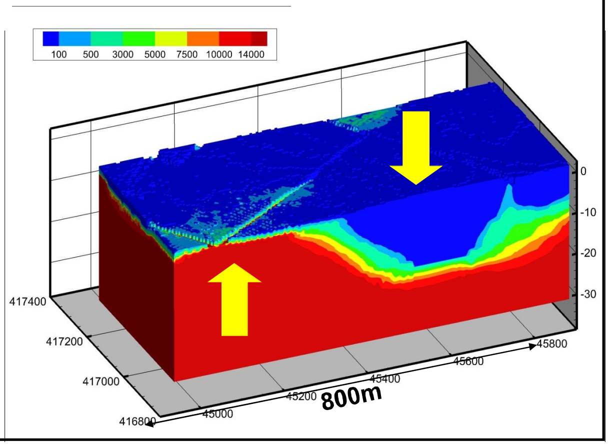
green is too salty to grow fresh crops

Use variable-density groundwater flow modelling

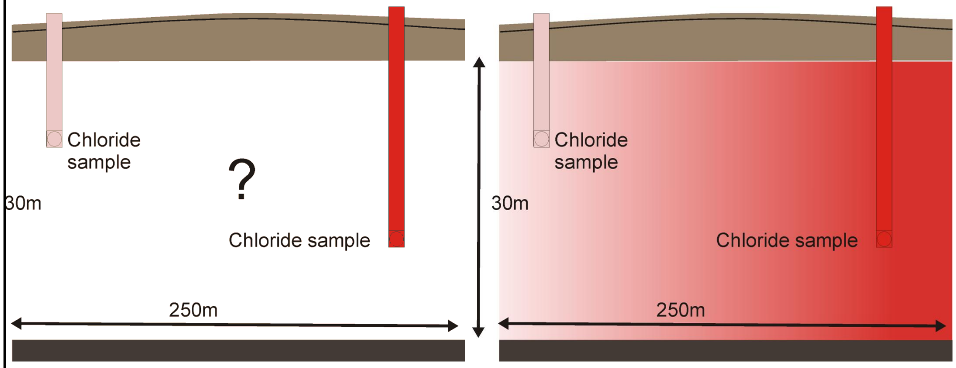
Why a model?

- variation in ground surface directly affects fresh-saline disribution

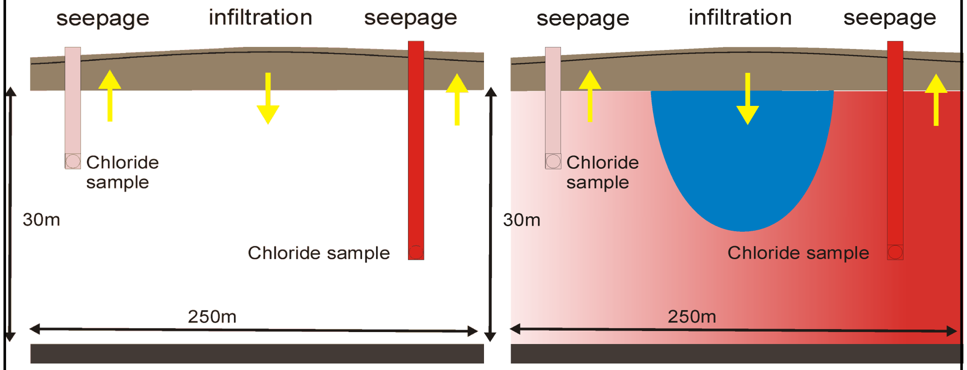




Interpolation chloride



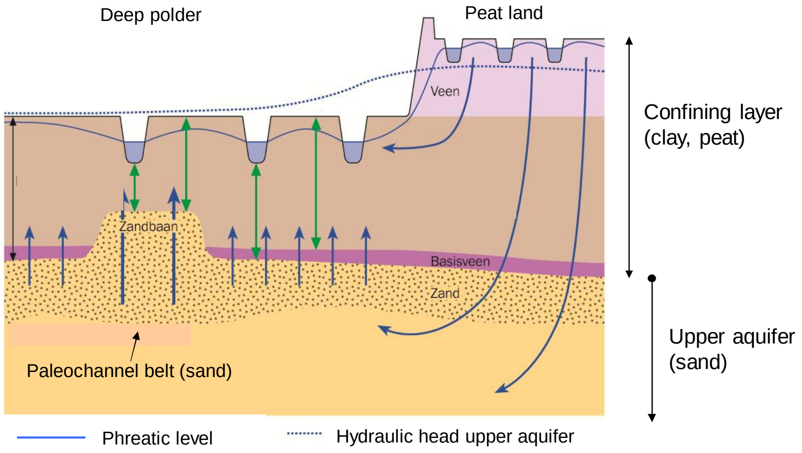
Using flow model for better interpolate chloride



Salty boils

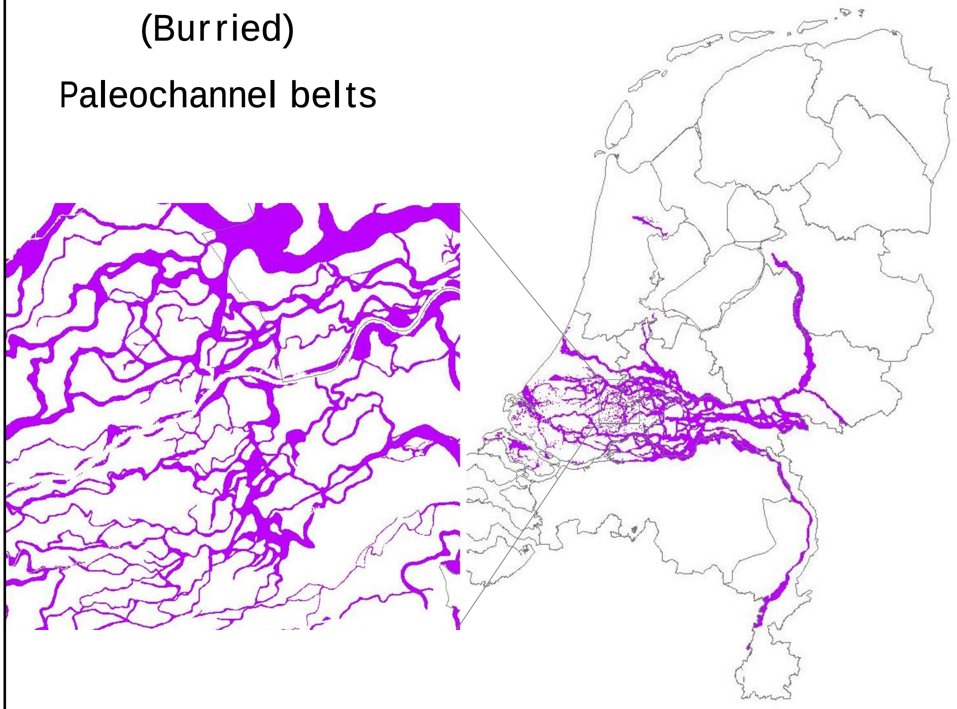
Louw, P.G.B., de, Oude Essink, G.H.P., Stuyfzand, P.J., Zee, van der, S.E.A.T.M., 2010, Upward groundwater flow in boils as the dominant mechanism of salinization in deep polders, The Netherlands, J. Hydrol. 394, 494-506.

Upward groundwater seepage in a deep polder and paleochannel belts as preferential flow paths

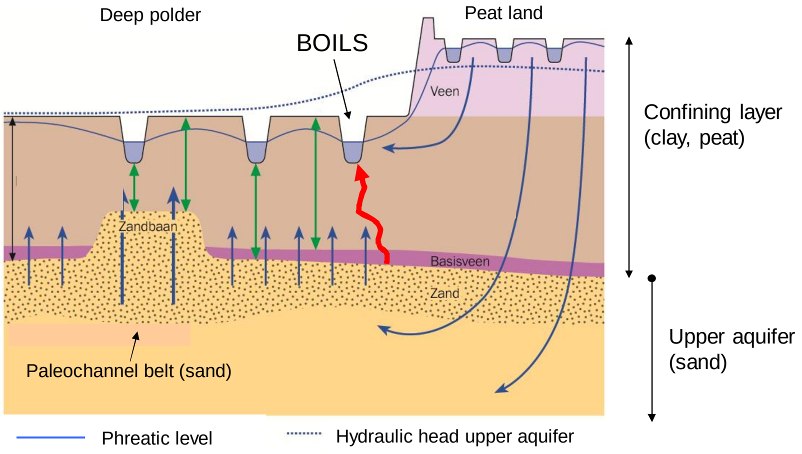


(Burried)

Paleochannel belts

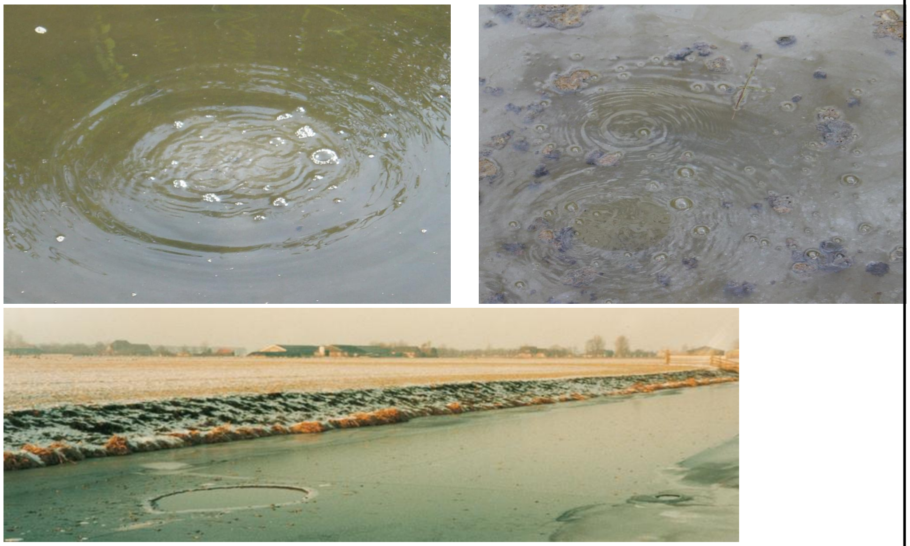


Preferential seepage via boils

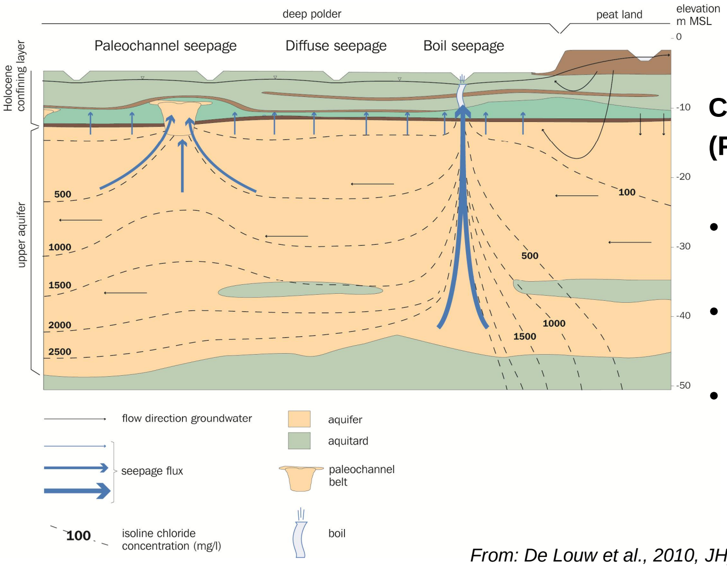


Preferential saline seepage via boils

Preferential saline seepage via boils



Three types of upward groundwater seepage

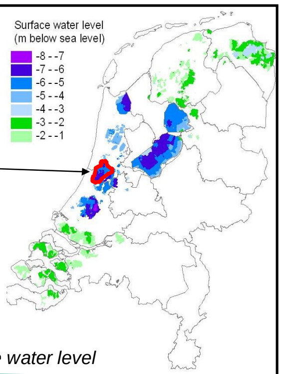


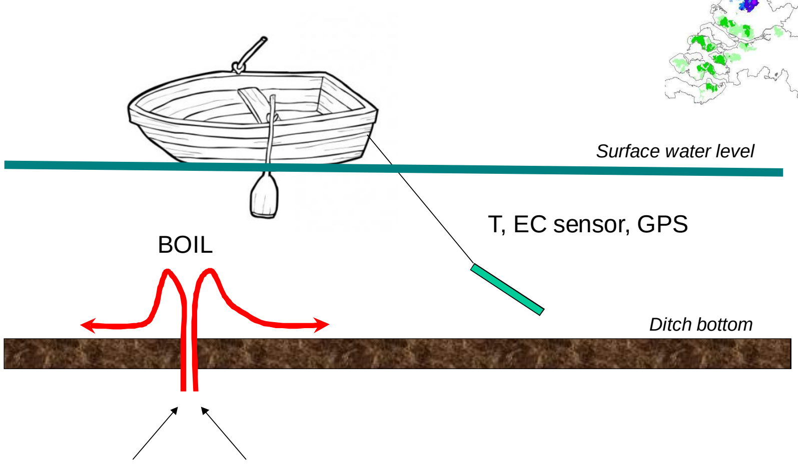
Cl-conc seepage:
(Polder Noordplas)

- Diffuse :
  100 mg/l
- Paleochannel :
  600 mg/l
- Boils :
  1100 mg/l

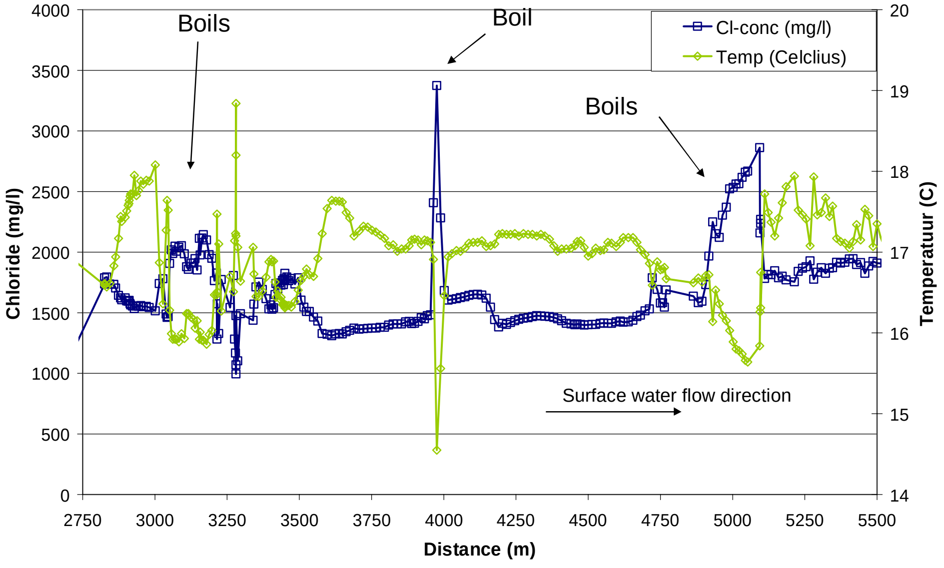
From: De Louw et al., 2010, JHydr.

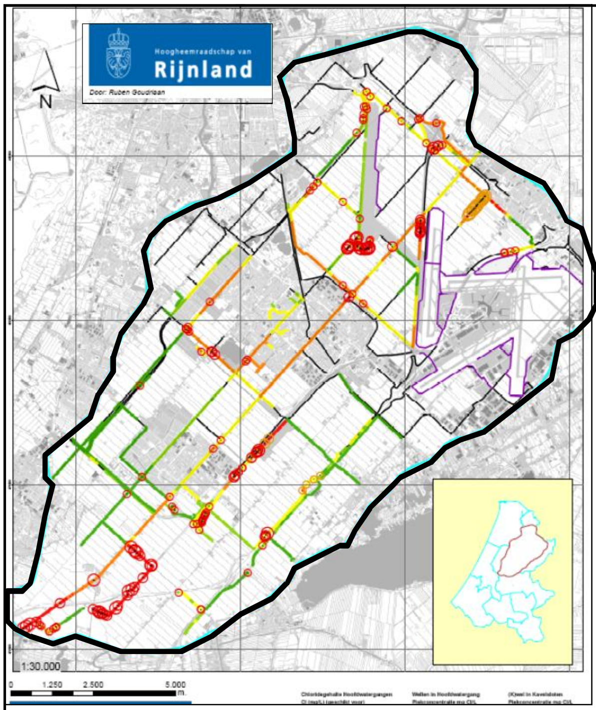
Continuous T and EC monitoring of surface water while sailing





T and EC measurements in surface water (canal)





Mapped boils and Cl-conc. surface water

Boils

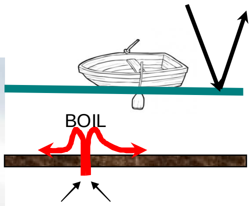
- ○ Cl = 500 -2000 mg/l
- ○ Cl > 2000 mg/l

Cl-conc surface water

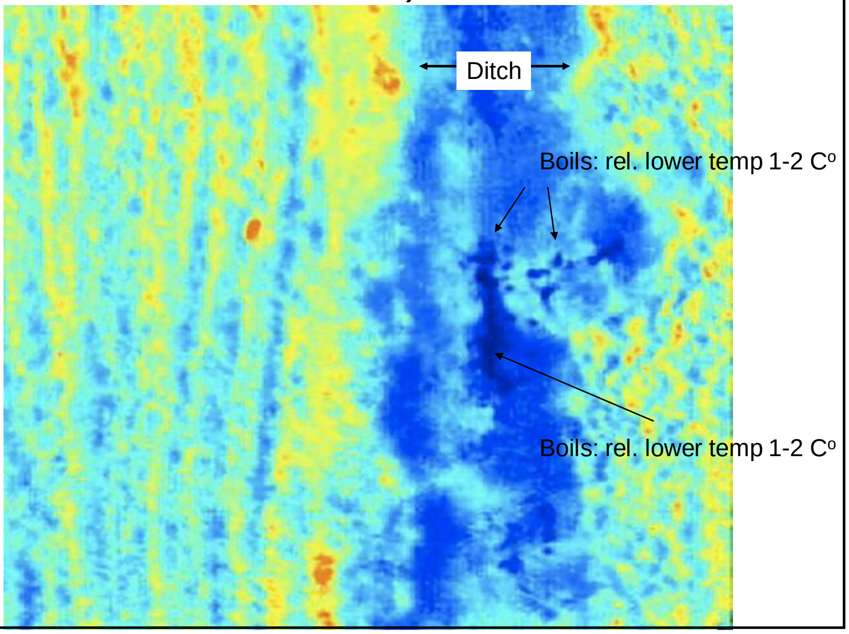
- 🟩 0-300 mg/l
- 🟨 300-600 mg/l
- 🟧 600-1000 mg/l
- 🟥 > 1000 mg/l

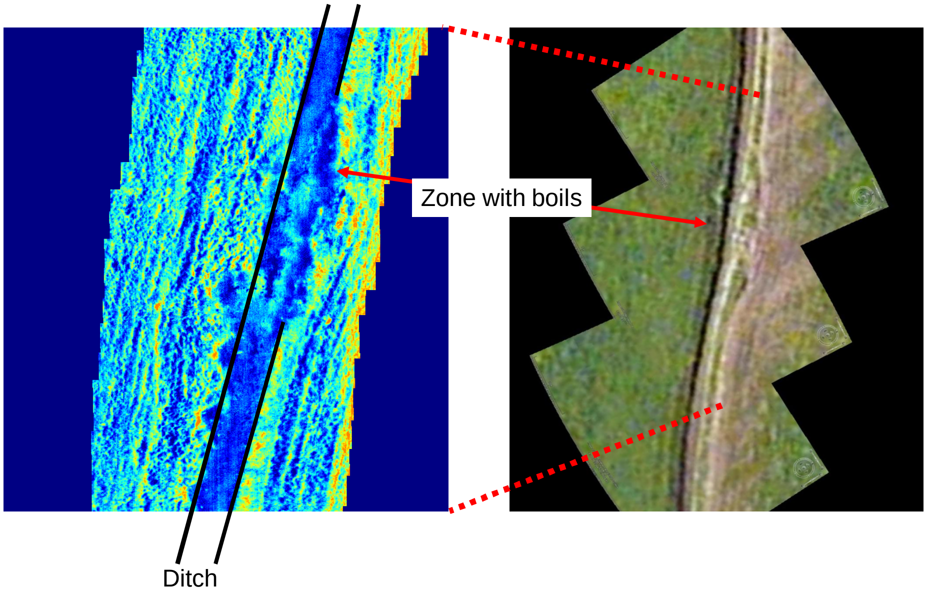
LARS technology (TNO Industry): Thermal Infra-red

- Altitude: 0-150 m
- Temp-detection using Thermal Infra Red sensors (only surface !)



Thermal infra-red results (blue is cold, red is warm)

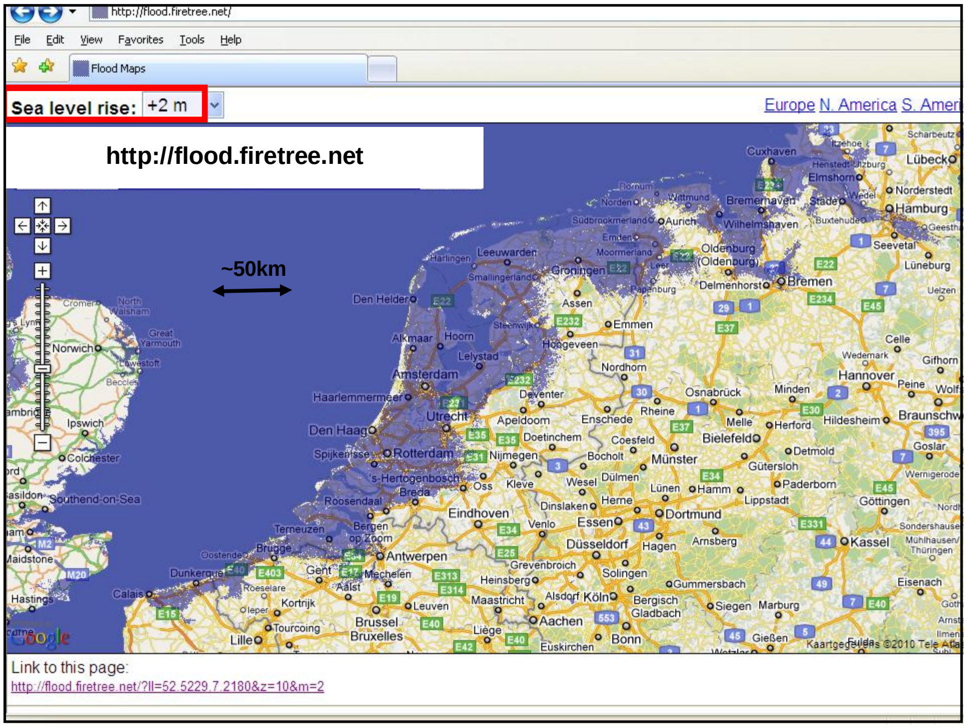




To get an idea about the possible future effects of sea level rise and climate change in your delta ...

evaluate of the past water management in the Dutch delta

Salt water intrusion in the Netherlands



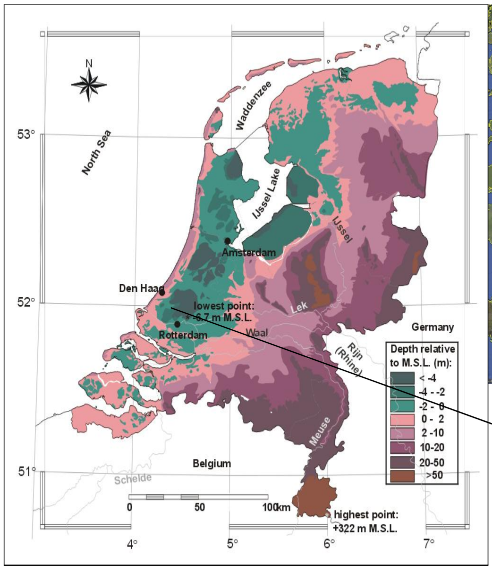
Sea level rise: +2 m

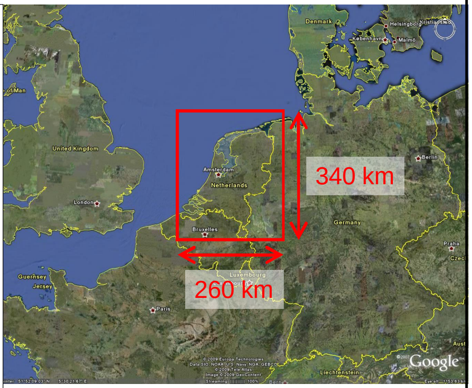
http://flood.firetree.net

~50km

Link to this page:
http://flood.firetree.net/?ll=52.5229,7.2180&z=10&m=2

The ‘low-lying’ lands: Netherlands





The city of Delft

Case study: The Netherlands

The Dutch coastal zone is already theathened by sea level rise and land subsidence for many centuries

Intensive water management system

Coping with salt water intrusion problems since 1950’s

The 'low-lying' lands: Netherlands

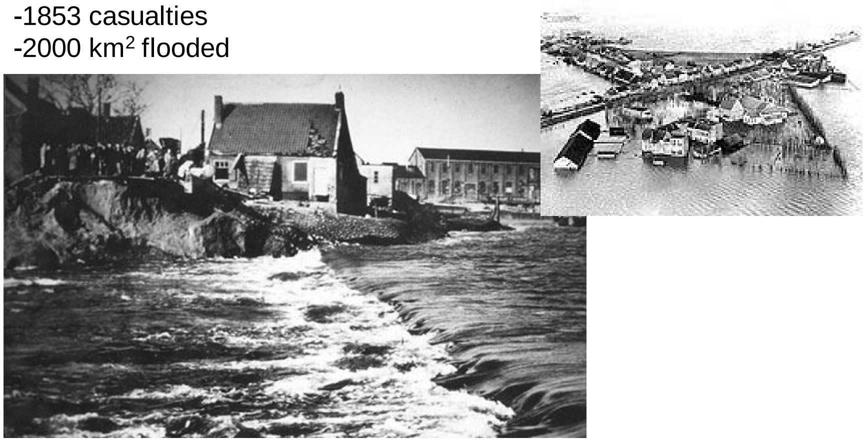
The facts:

- a deltaic area with 3 rivers: Meuse, Scheldt & Rhine
- 25% of land surface is lying below mean sea level
- 65 % would be flooded regularly if there were no dunes and dikes
- 8 million people would be endangered

The Great Flooding in february 1953

Combination of high tide and heavy storm:

-1853 casualties
-2000 km^2 flooded



Infrastructure to protect our low-lying land from flooding

River flooding in 1995

Combination of heavy rains upstream the catchment
& short retention time

Dike collapse 2003

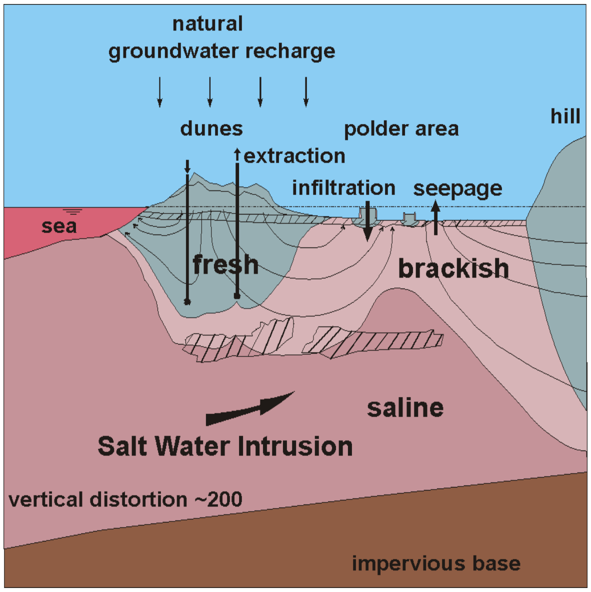
Combination of peat dike instability and very dry summer

Estimated water management costs ‘to keep our feet dry’

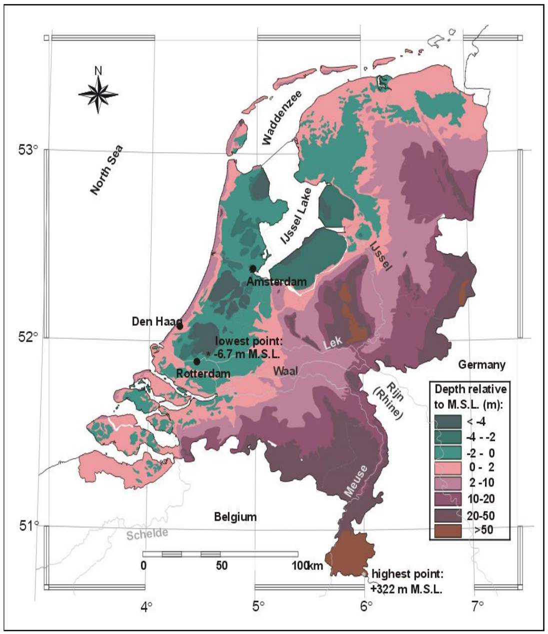
Costs up till 2050 in billion euros:

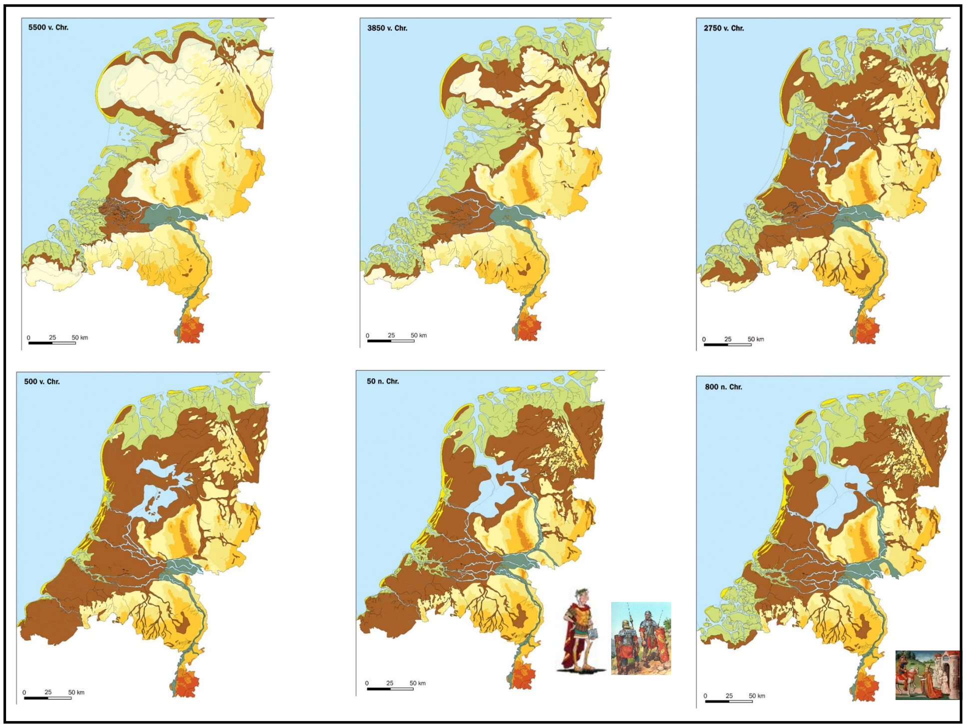
rivers: upper part	5.7
rivers: lower part	5.6
low-lands	1.7
coastal zone	8.0
infrastructure	3.5
purchase of ground	2.0
	-----+
	26.5 billion euros

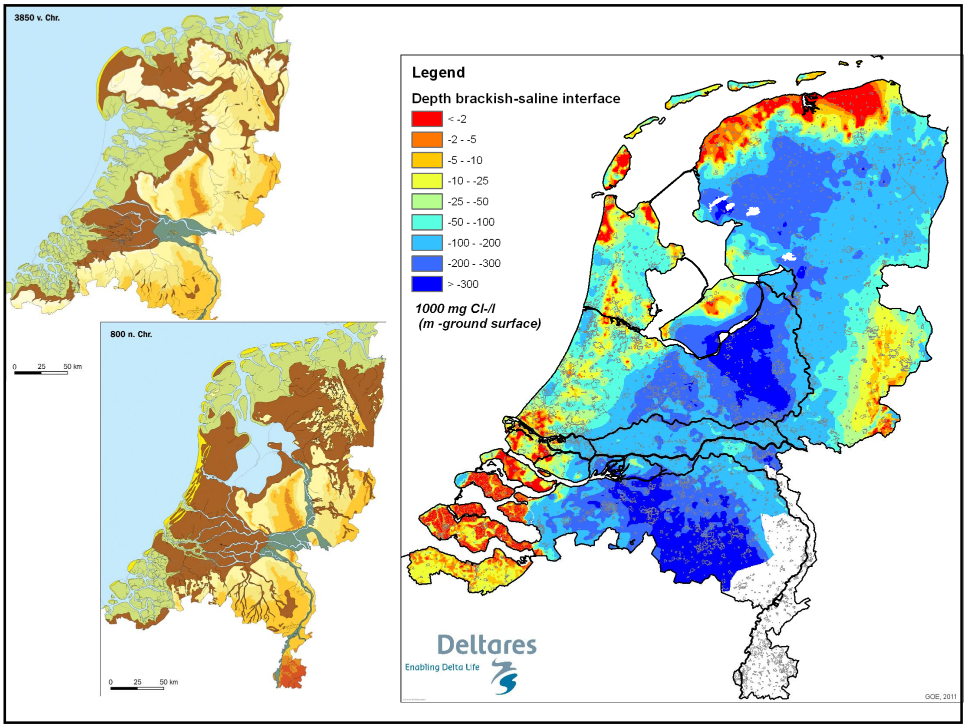
Salt water intrusion in the Netherlands



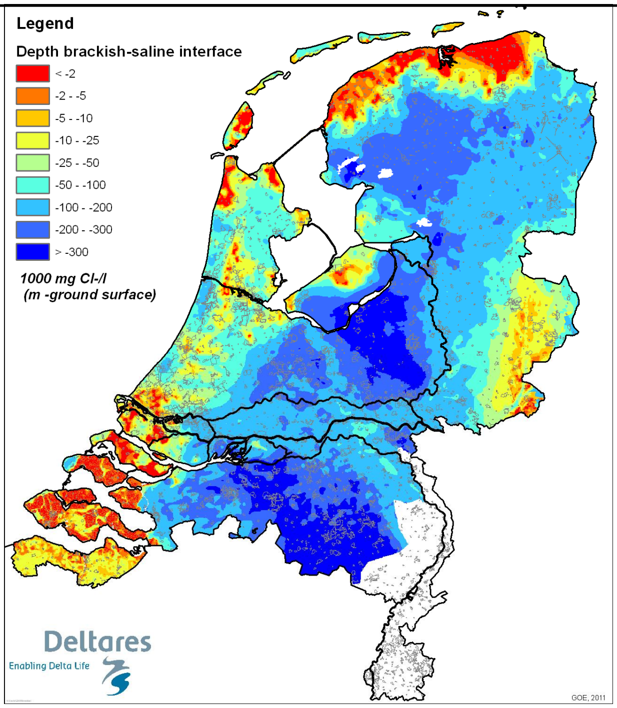
Present ground surface in the Netherlands



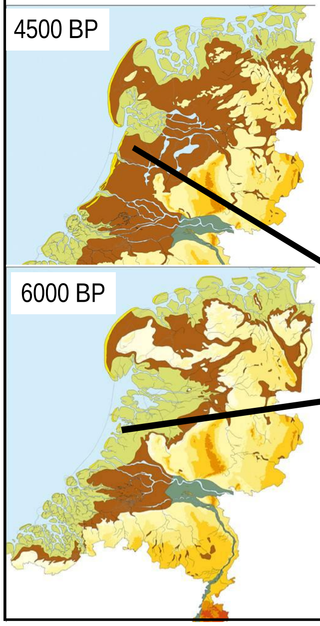

5500 v. Chr.
3850 v. Chr.
2750 v. Chr.
500 v. Chr.
50 n. Chr.
800 n. Chr.
0 25 50 km

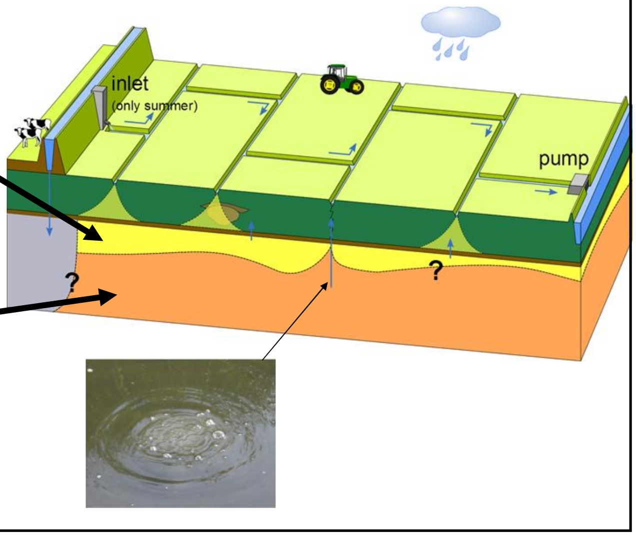

3850 v. Chr.
800 n. Chr.
0 25 50 km
Legend
Depth brackish-saline interface
< -2
-2 - -5
-5 - -10
-10 - -25
-25 - -50
-50 - -100
-100 - -200
-200 - -300
> -300
1000 mg Cl-/l
(m -ground surface)
Deltares
Enabling Delta Life
GOE, 2011

Fresh-Salt interface



Hydrogeology





Salinisation of the Dutch subsurface

Physical transport processes:

- advective: e.g. trans- and regressions
- dispersive: mixing with marine deposits
- diffusive: e.g. IJsselmeer lake
- chemical: solution, precipitation, ion-exchange

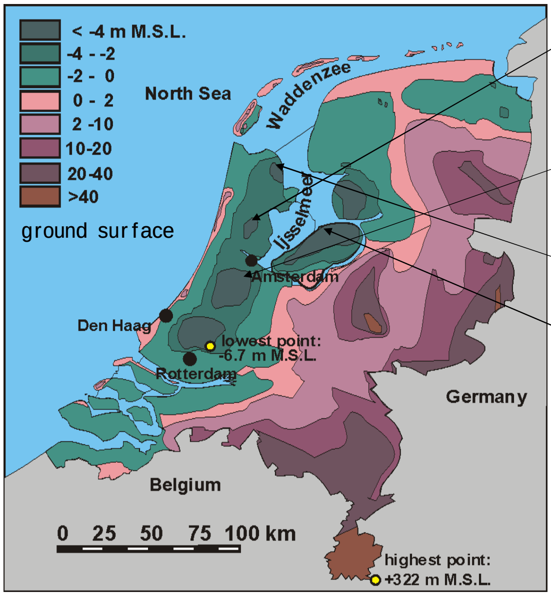
Anthropogenic causes:

- land subsidence
- polder level lowering
- groundwater extractions

Future developments (climate change):

- sea level rise
- changes in recharge

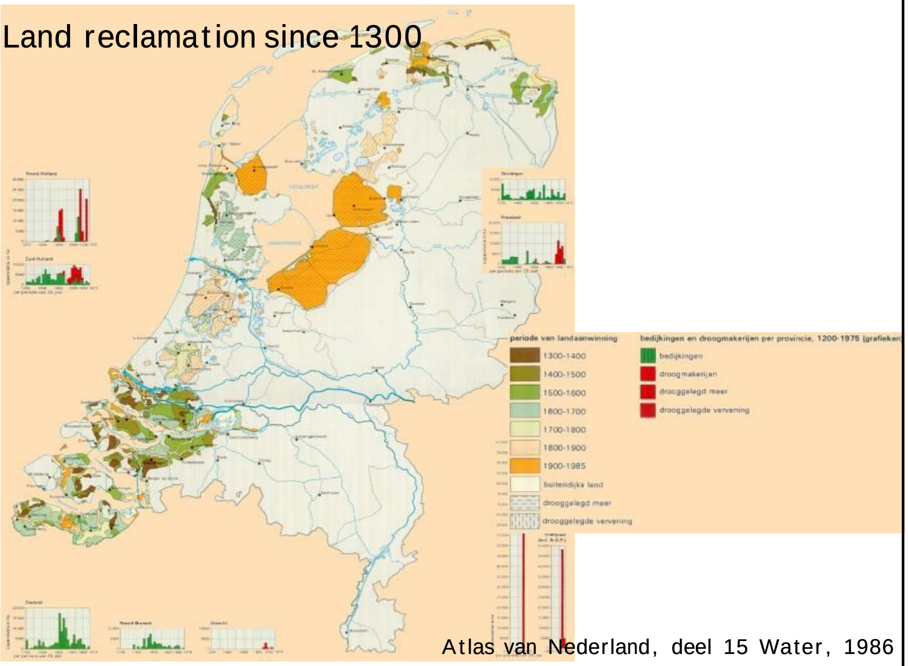
Abrupt land subsidence



position polders:

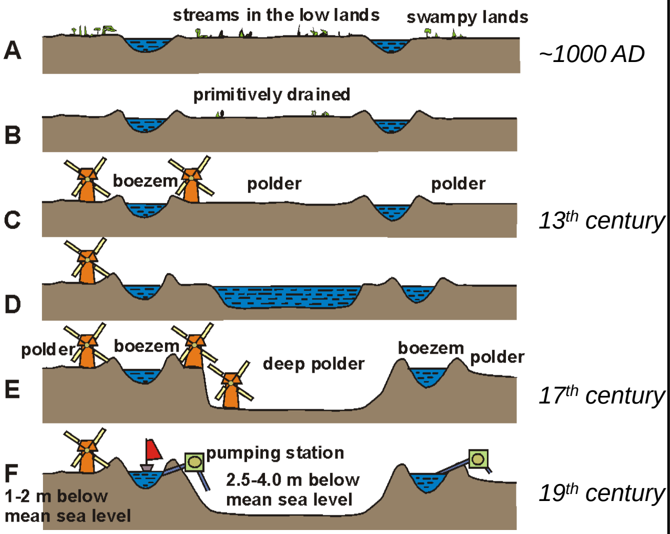
Beemster	1608-1612
Wormer	1625-1626
Schermer	1633-1635
Purmer	1618-1622
Haarlemmermeer polder	1850-1852
Wieringermeer polder	~1930
Flevo polders	1950-60s

Land reclamation since 1300



Atlas van Nederland, deel 15 Water, 1986

Development of the Dutch ‘Polder’ Landscape



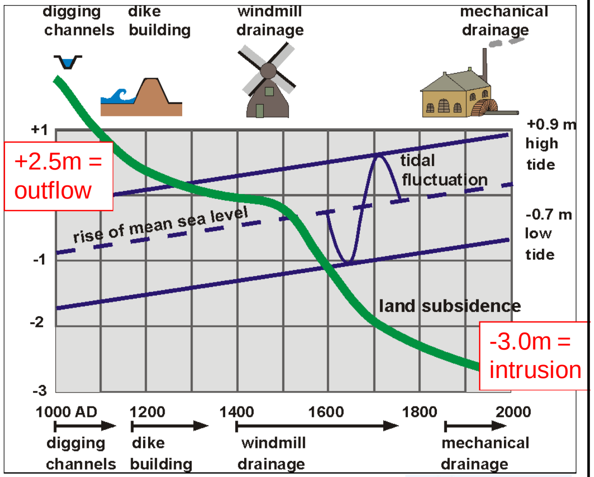
From fresh water outflow to salt water inflow

Causes:

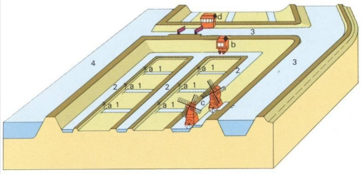
- Autonomous processes
- Land subsidence
- Abrupt land reclamation

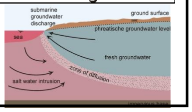
- Climate change
- Sea level rise
- Change in net recharge

Historical subsidence of the ground surface in Holland

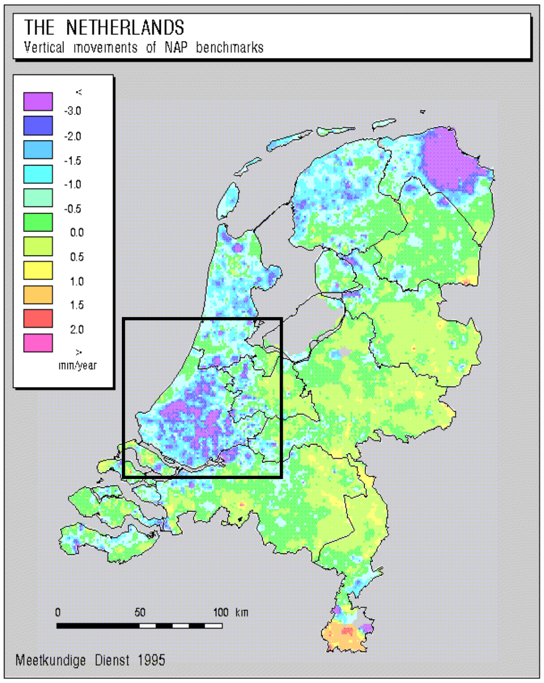


Ground surface





Land subsidence related to M.S.L.



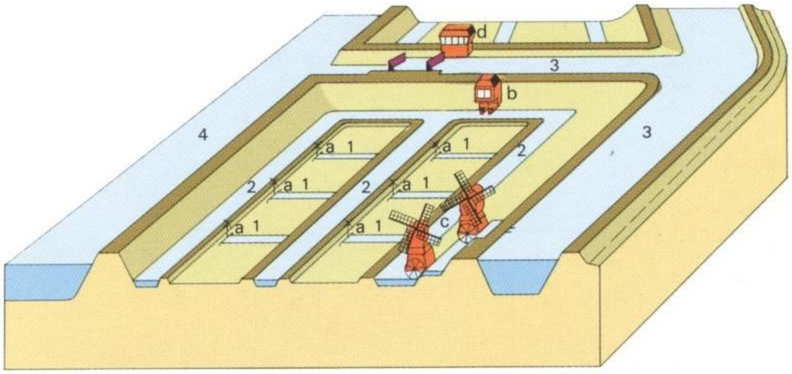
Land subsidence

up to 1 m per century

The polder system

A land below the sea with an excess of water needs..

a sophisticated drainage system



The polder system

Many agricultural plots with different water levels throughout the season

The polder system

The polder system

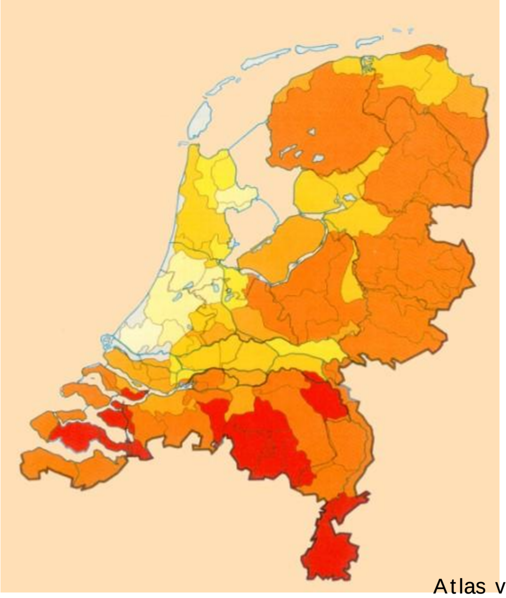
Bulb farms at the landside of the sand dunes

Salt damage in 1976 (very dry year)

Salt damage [percentage] in potential crop-production

Atlas van Nederland, deel 15 Water, 1986

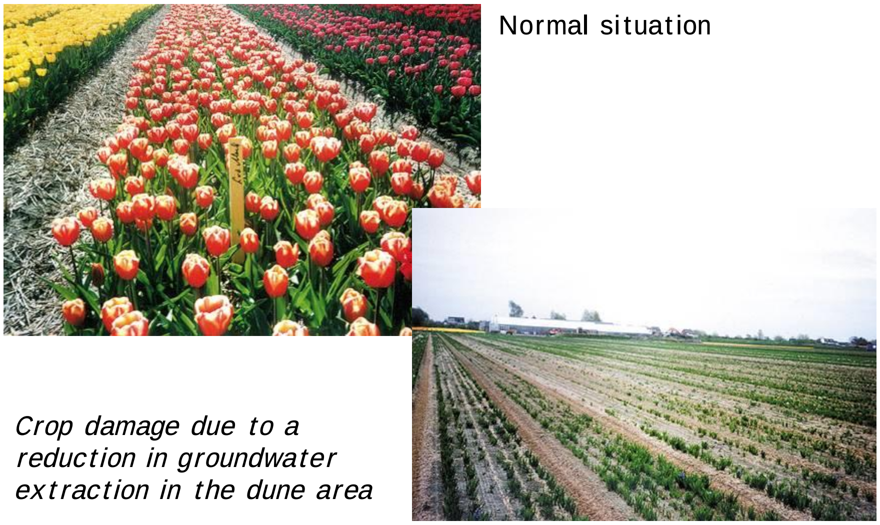
Drought damage in 1976 (very dry year)



Drought damage [percentage] in potential crop-production

Atlas van Nederland, deel 15 Water, 1986

‘Wetting’ damage



Normal situation

Crop damage due to a reduction in groundwater extraction in the dune area

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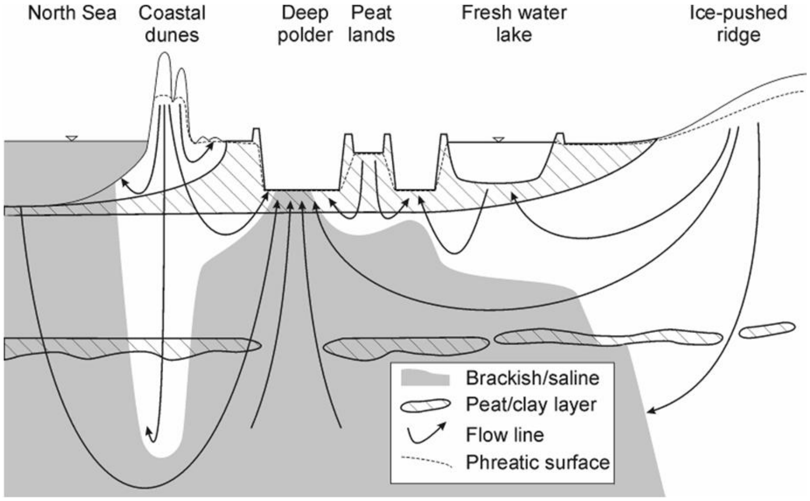
Now focus on groundwater…



Threats to water management due to climate change:

Short term threats:

- -flooding
- -dike collapse
- -drought

asks for operational water management

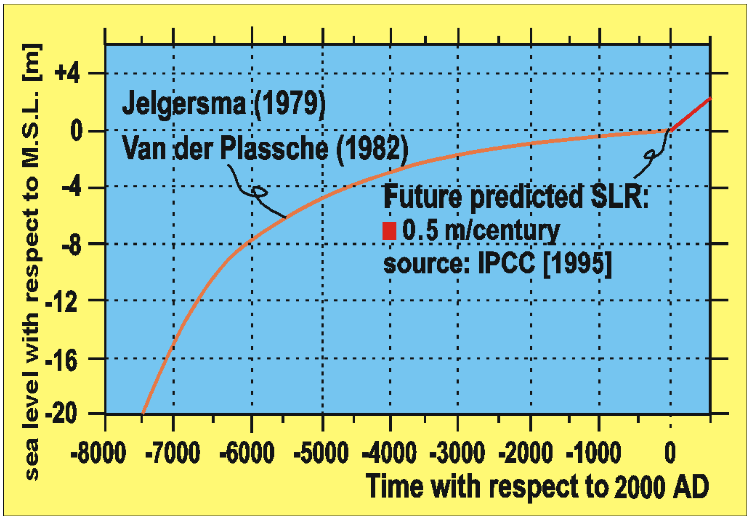
Long term threats:

- -salt water intrusion
- -land subsidence
- -smaller fresh groundwater resources

asks for strategic water management

Dutch setting

Past and future sea level rise in the Netherlands

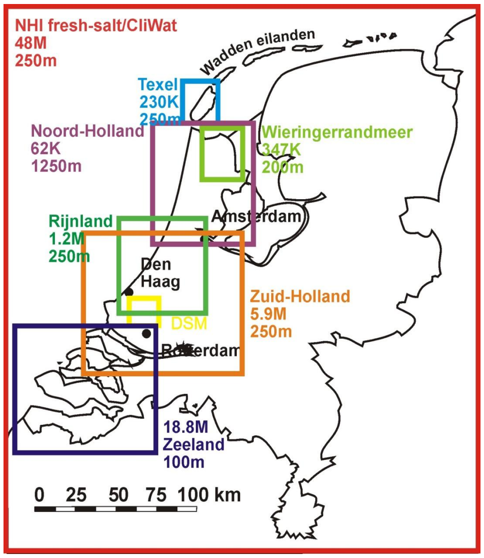


Numerical variable density models at Deltares

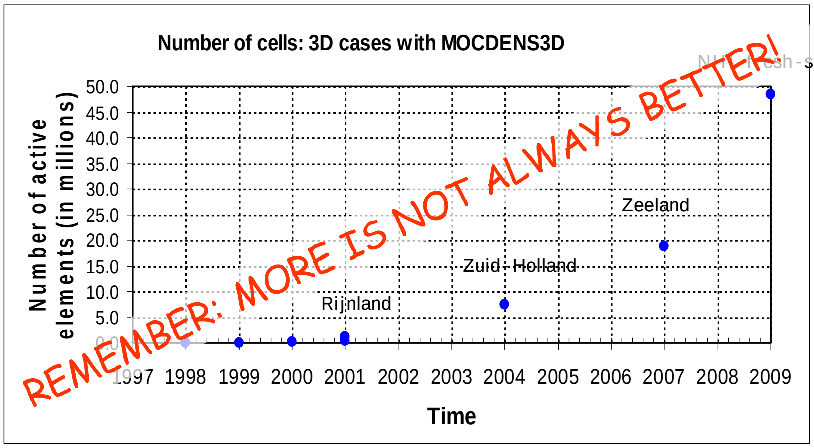
Characteristics:
- variable-density groundwater
- fresh, brackish and saline
- 3D, non-steady
- coupled solute transport

Code (MODFLOW family):
MOCDENS3D
SEAWAT

Assessing effects:
- autonomous salinisation
- sea level rise
- changing recharge pattern
- land subsidence
- changing extraction rates
- adaption measures



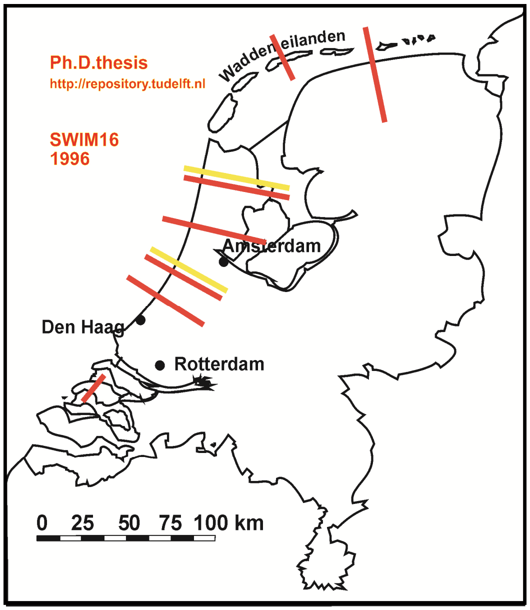
‘DO NOT DO THIS AT HOME!’ (DATA PROBLEM)



REMEMBER: MORE IS NOT ALWAYS BETTER!

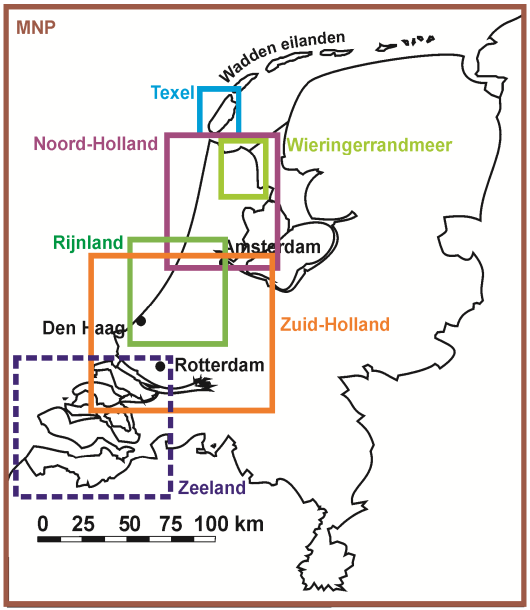
Modelling effect sea level rise on salt water intrusion

2D models



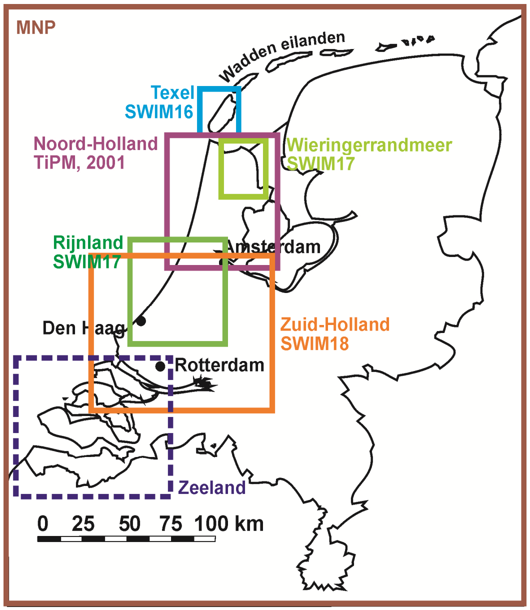
Modelling effect sea level rise on salt water intrusion

3D models



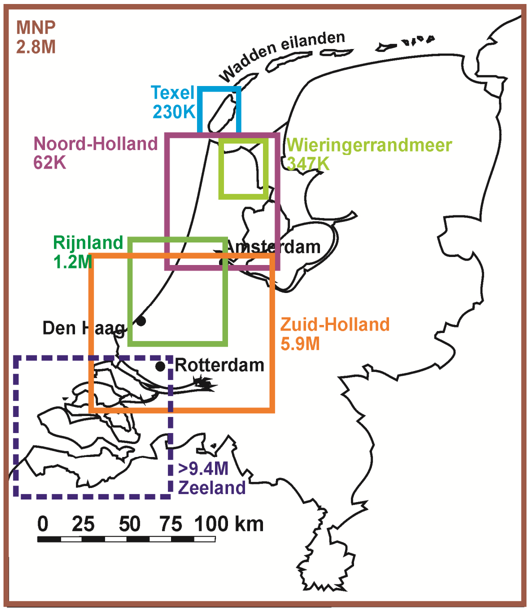
Modelling effect sea level rise on salt water intrusion

3D models
SWIM



Modelling effect sea level rise on salt water intrusion

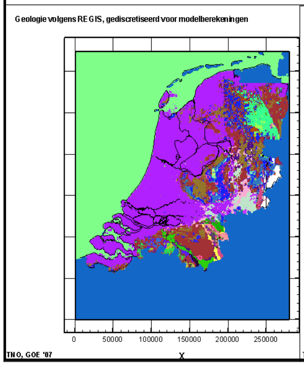
3D models
number cells



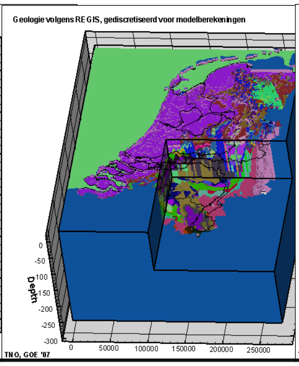
Recent model study for the whole Netherlands on the effect of sea level rise of water management (1)

Using the national subsoil parametrisation

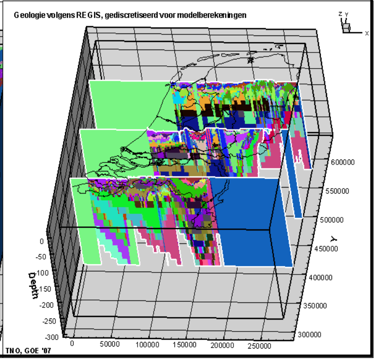
- REGIS V2
- Top geological system from +10m up to -280m M.S.L.
- 31 modellayers with thicknesses: 2*5m; 10*2m; 8*5m en 11*20m
- cellsize 1000x1000m (coarse)



Geologie volgens REGIS, gediscretiseerd voor modelberekeningen



Geologie volgens REGIS, gediscretiseerd voor modelberekeningen



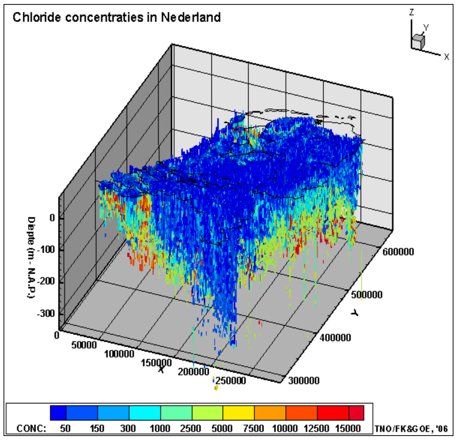
Geologie volgens REGIS, gediscretiseerd voor modelberekeningen

---

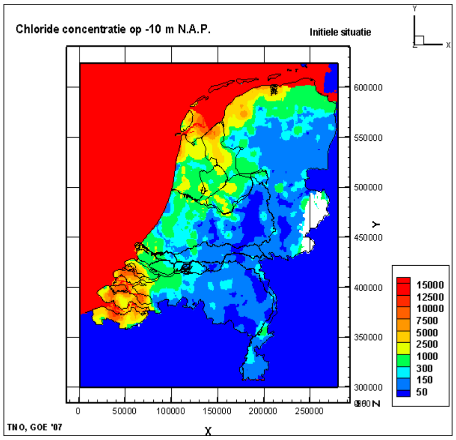
Recent model study for the whole Netherlands on the effect of sea level rise of water management (2)

Using the national 3D salt concentration in groundwater

Zoet-Zout REGIS: ~65000 measuring points (analyses, VES, Borehole)



Chloride concentraties in Nederland

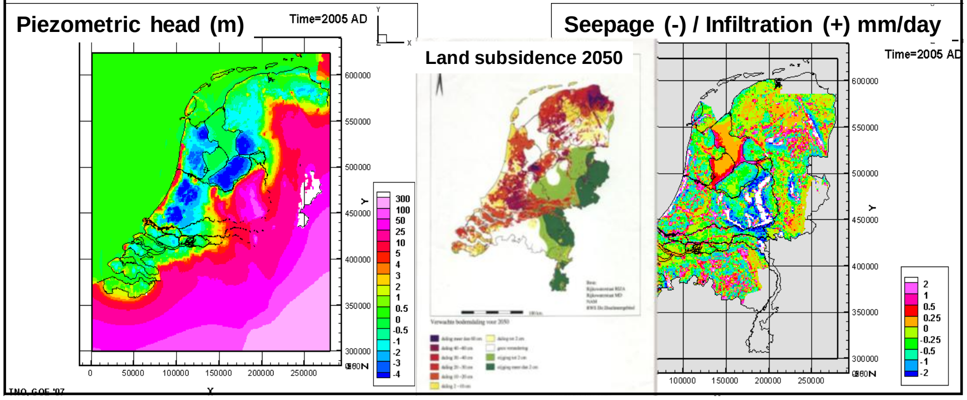


Chloride concentratie op -10 m N.A.P.

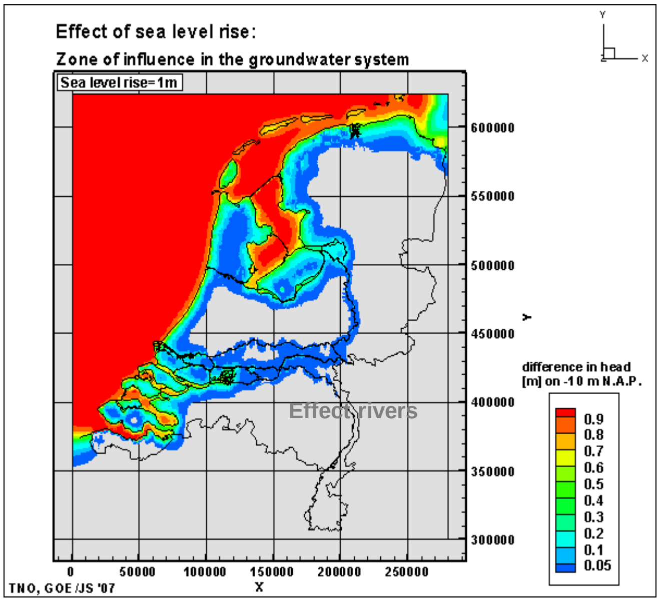
Initiele situatie

Recent model study for the whole Netherlands on the effect of sea level rise of water management (3)

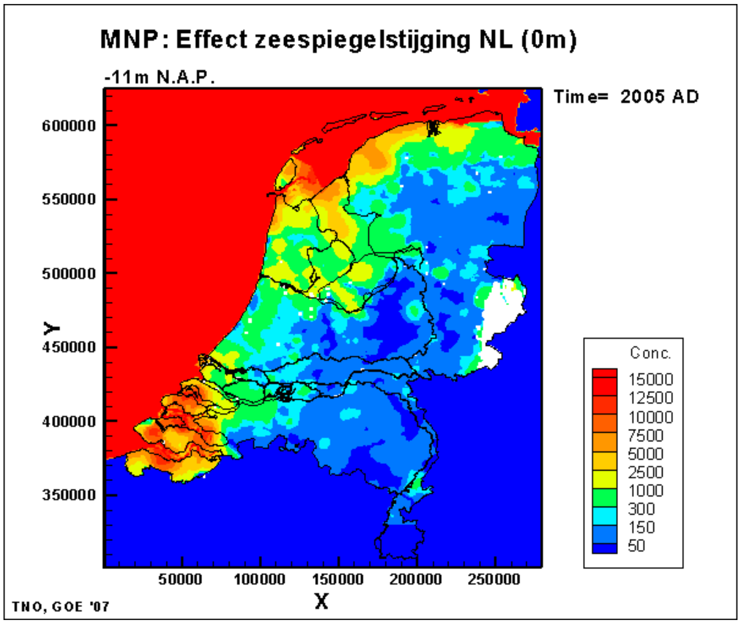
- Variable-density 3D groundwater flow model and coupled solute transport
  - 10 scenario’s, including extreme sea level rise
  - including land subsidence estimates



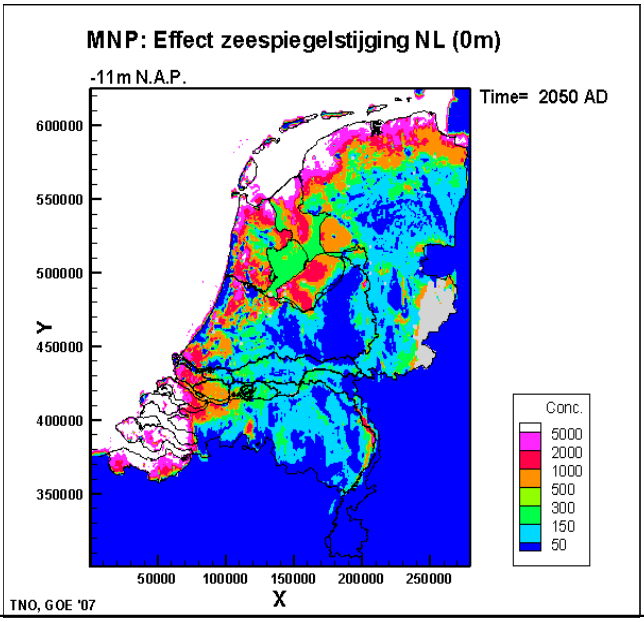
Results: zone of influence 1m sea level rise



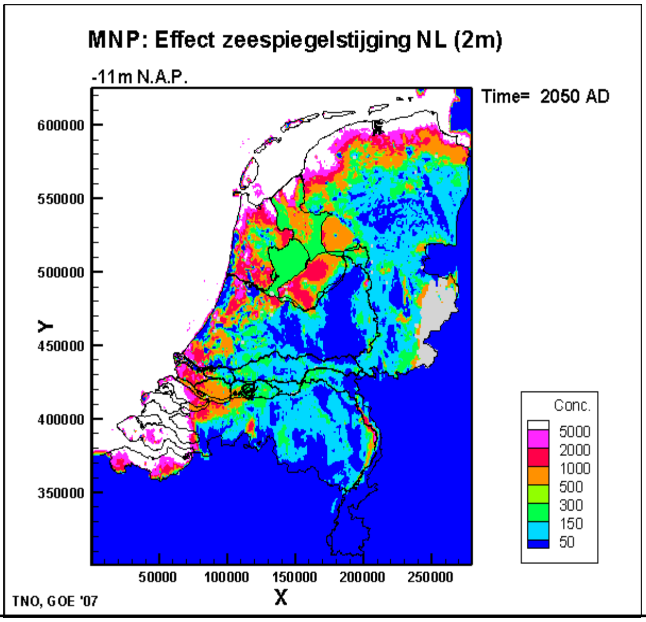
Salinisation over the period 2000-2050



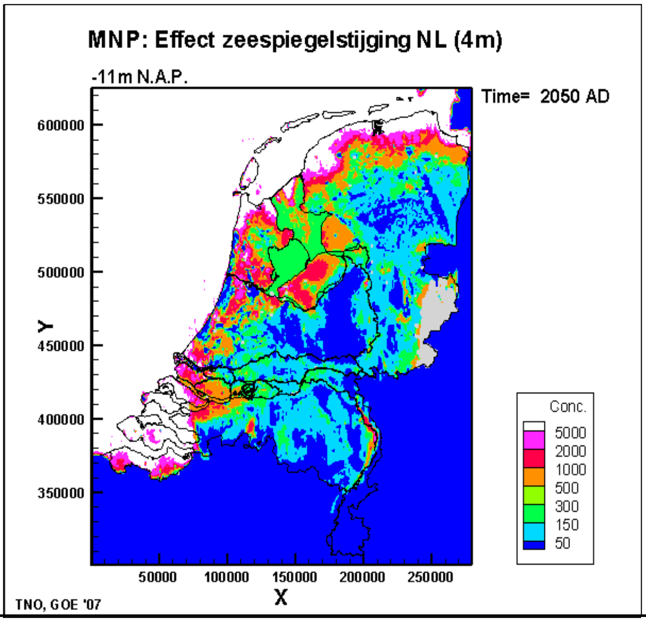
Salinisation subsoil at 0m sea level rise in 2050



Salinisation subsoil at 2m sea level rise in 2050

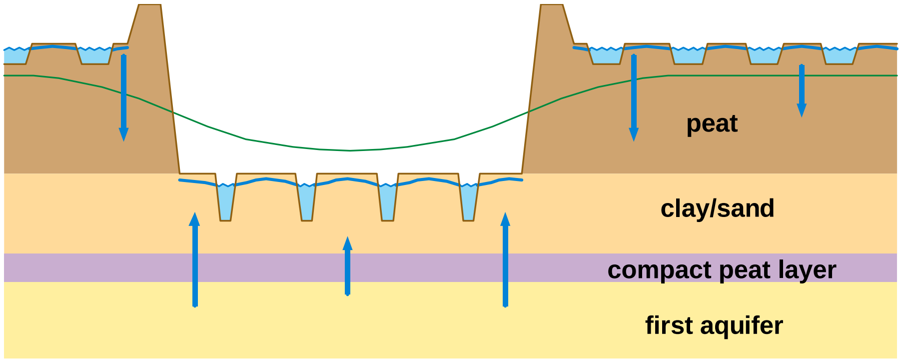


Salinisation subsoil at 4m sea level rise in 2050

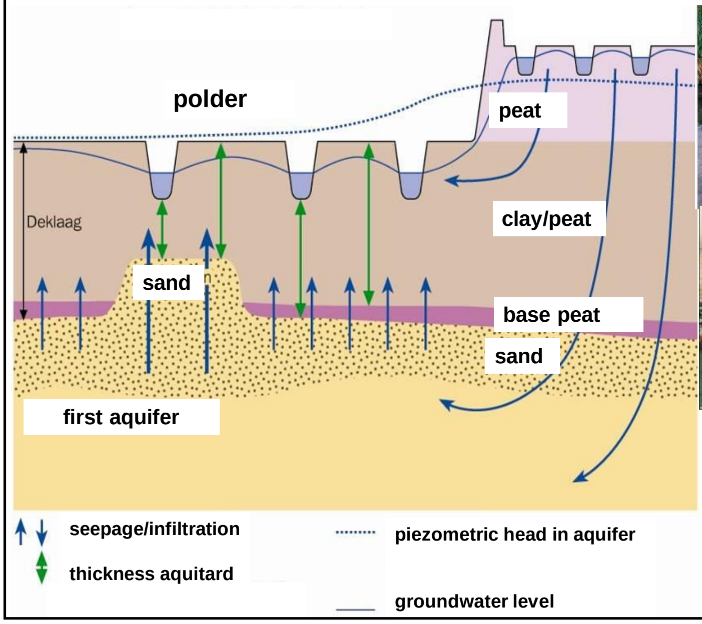


Salty wells

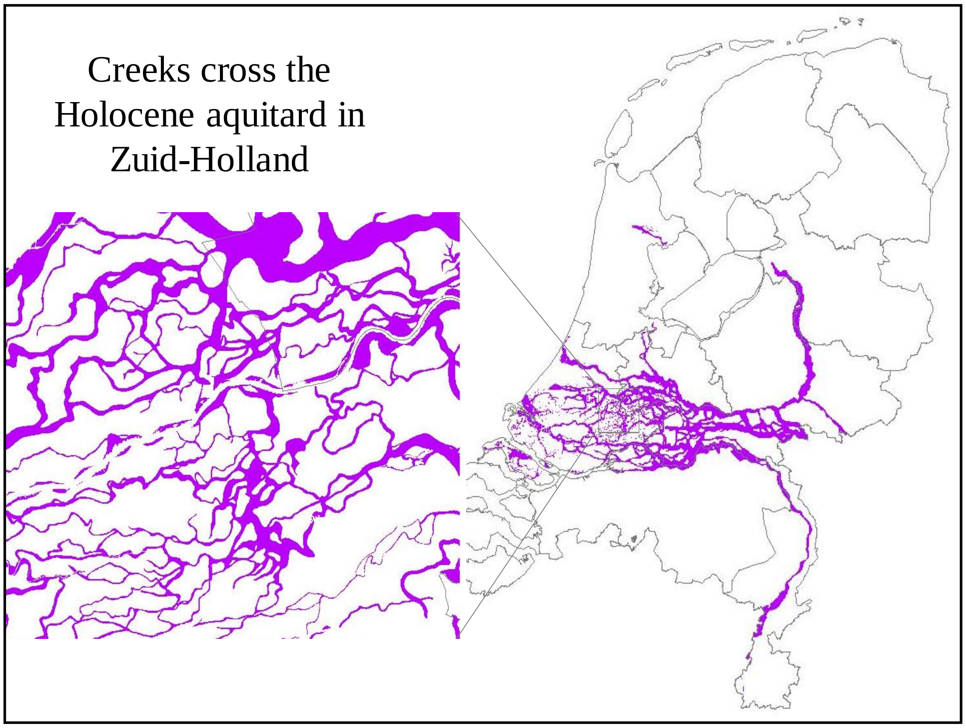
Seepage and infiltration situation around deep polders



Risk of instable Holocene aquitards (1)

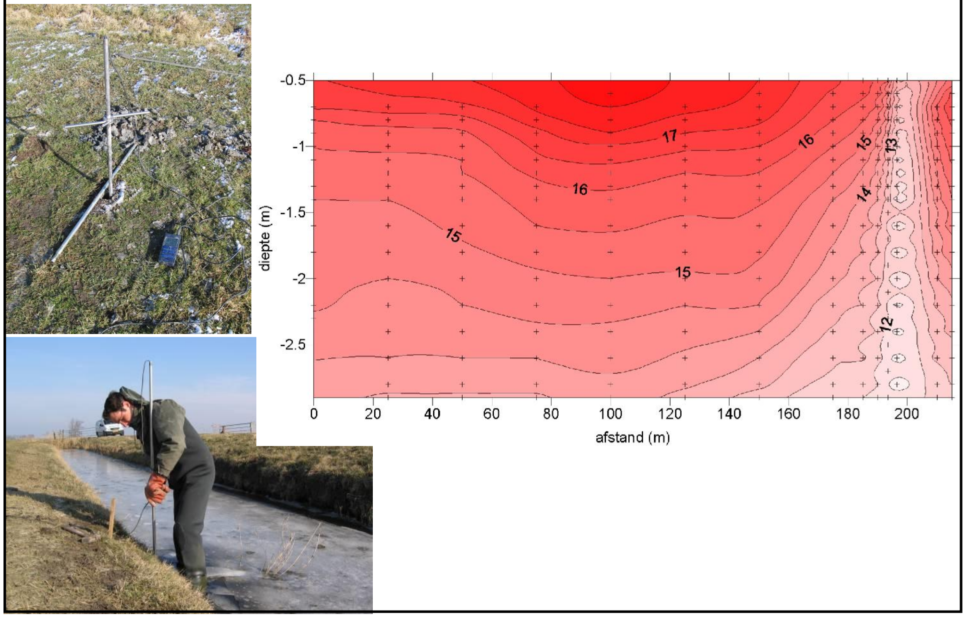


Creeks cross the Holocene aquitard in Zuid-Holland

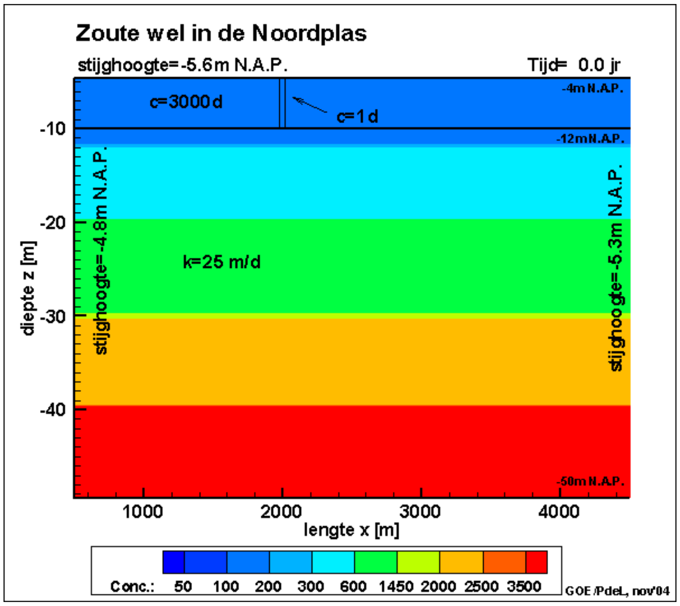


‘*Wells*’ (weak spots in Holocene layer)

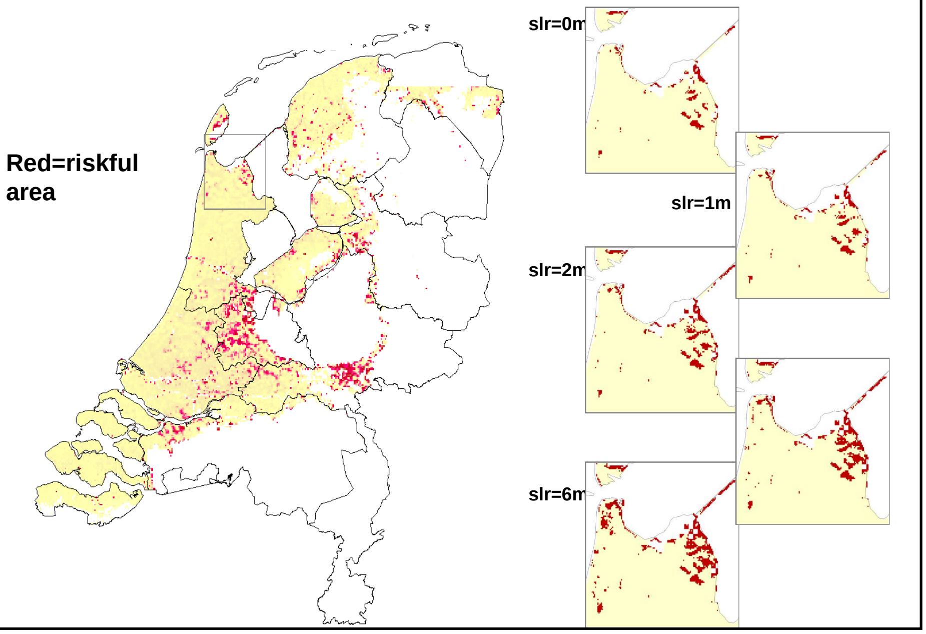
Temperature measurements



Simulation of salt groundwater towards *wells*

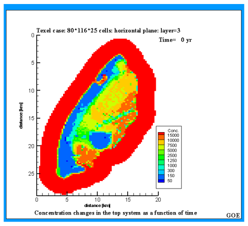


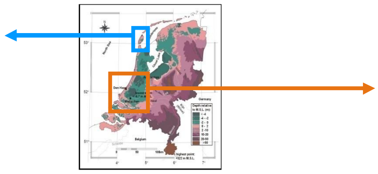
Risk of instable Holocene aquitards (2)

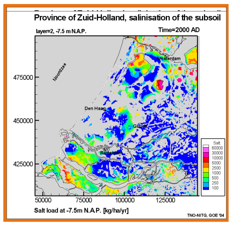


Red=riskful area

Quantification hydrogeological impacts of sea level rise







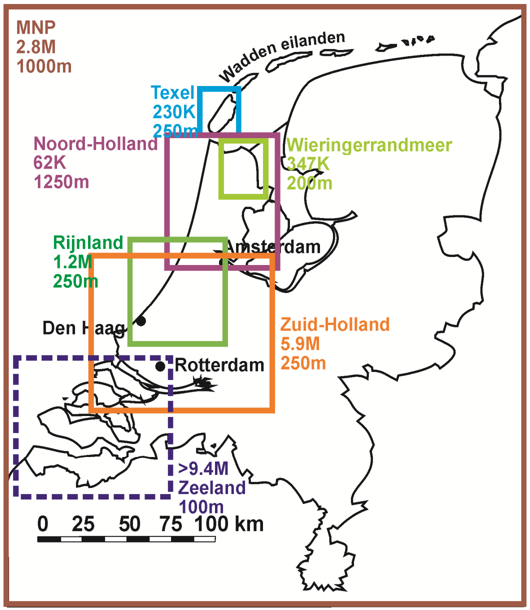
Situation at 2100 AD with sea level rise of 0.5m/century,

Including land subsidence at Zuid-Holland (max 1.0m/century)

	Texel	Zuid-Holland
Increase seepage (%)	+22	+4
Increase salt load (%)	+46	+34
Hinge area: from infiltration to seepage (% land surface)	+3	+5

Modelling effect sea level rise on salt water intrusion

3D models
number cells
grid size



Characteristics 3D Cases (I): geometry & subsoil

Case	Kop van Noord-Holland	Texel	Wieringer-meerpolder	Rijnland
total land surface [km^2]	2150	130	200	1100
L_x*L_y modelled area [km]	65*51	20*29	23*27	52*60
depth system [m –N.A.P]	290	302	385	190
aquifer hydr.cond. [m/d]	5-70	5-30	15-40	12-70
aquitard hydr.cond. [m/d]	0.12-0.001	0.01-1	0.012-0.056	2.5E-4-0.8
porosity	0.35	0.3	0.25	0.25
anisotropy [k_z/k_x]	0.4	0.4	0.25	0.1
long. dispersivity α_L [m]**	2	2	2	1
# head&conc. observations	not applicable*	111	95	1632
characteristics head calibration	not applicable*	$\lvert\Delta\phi\rvert$=0.24 m σ=0.77 m	$\lvert\Delta\phi\rvert$=0.34 m σ=0.21 m	$\lvert\Delta\phi\rvert$=0.60 m σ=0.77 m

* calibration with seepage & salt load in polders

**molecular diffusion=10^{-9} m^2/s; trans. disp.=1/10 long. disp.

Characteristics 3D Cases (II): model parameters

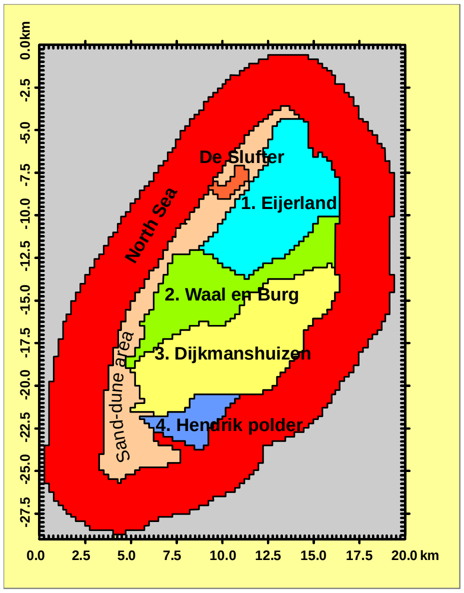
Case	Kop van Noord-Holland	Texel	Wieringer-meerpolder	Rijnland (=391 EM RAM)
horizontal cell size [m]	1250*1250	250*250	200*200	250*250
vertical cell size [m]	10	1.5 to 20	2 to 70	5 to 10
total # active cells	~40.000	~126.000	~312.000	~1.200.000
# cells	41*52*29	80*116*23	116*136*22	209*241*24
# particles per cell	27	8	8	8
total time [yr]	1000	500	50	500

convergence head criterion= $10^{-5}/10^{-4}$ m

flow time step Δt=1 year

Model of the island of Texel

Characteristics of the island of Texel (I)



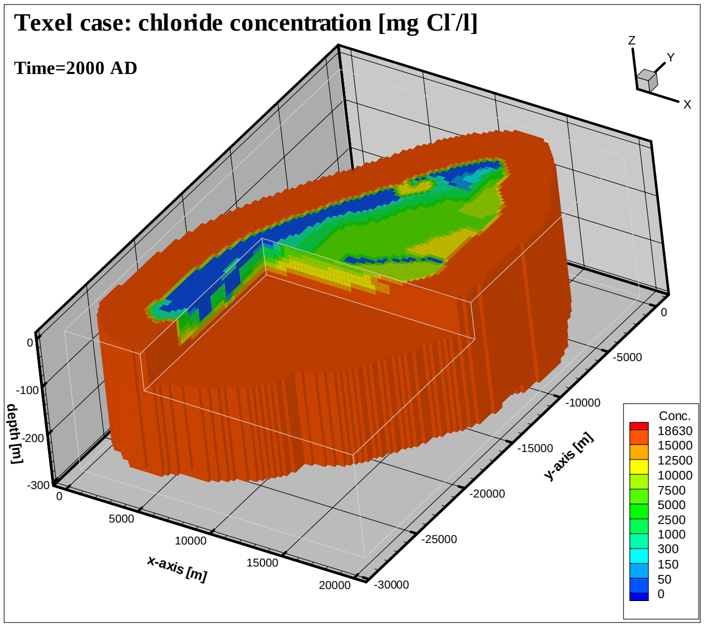
- Tourist island in summer time
- Land surface: 130 km^2
- Polder areas:
  - 🟦 1. Eijerland
  - 🟩 2. Waal en Burg
  - 🟨 3. Dijkmanshuizen
  - 🟦 4. Hendrik polder

🟫 Sand-dune area at western side

🟧 'De Slufter' is a tidal salt-marsh

🟥 North Sea surrounds the island

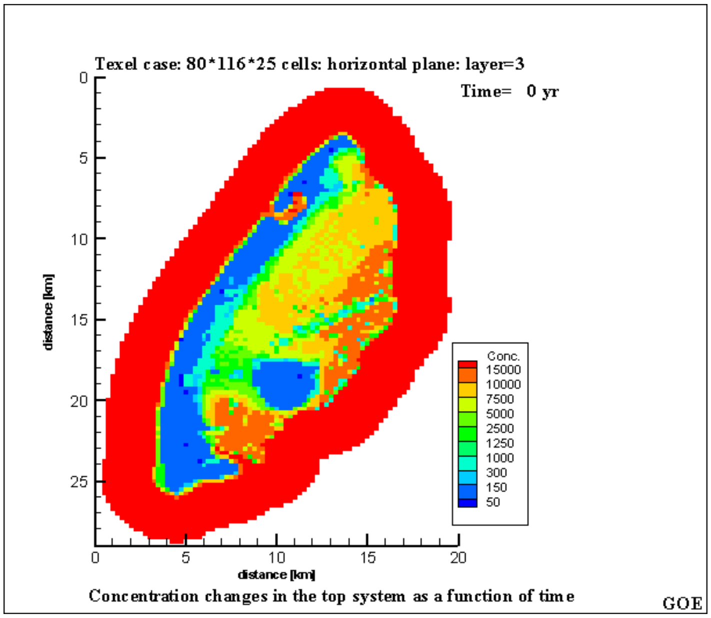
Texel: present 3D chloride distribution



Texel case: chloride concentration [mg Cl^-/l]

Time=2000 AD

Texel: reference case=autonomous development



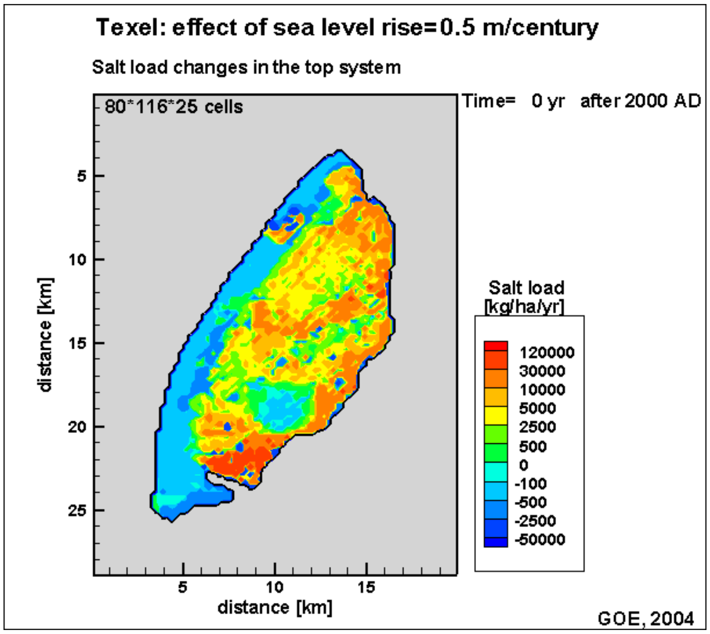
Texel case: 80*116*25 cells: horizontal plane: layer=3

Time= 0 yr

Concentration changes in the top system as a function of time

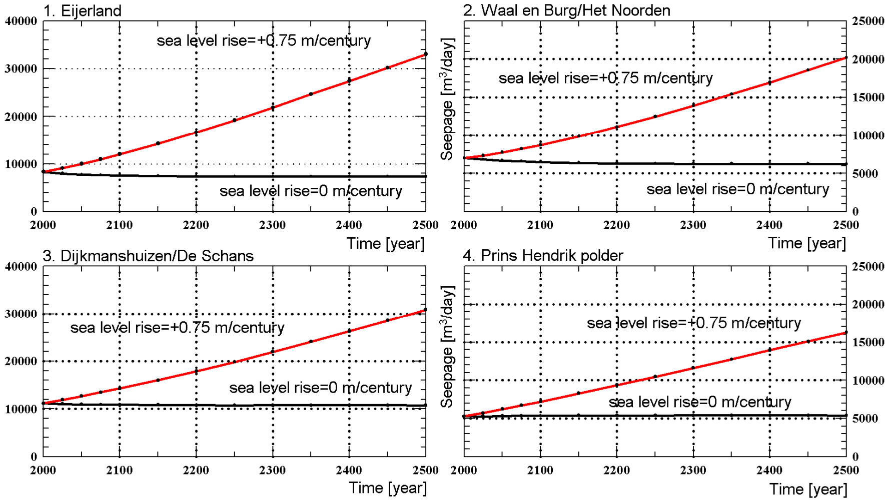
Texel

Texel: effect of sea level rise on salt load

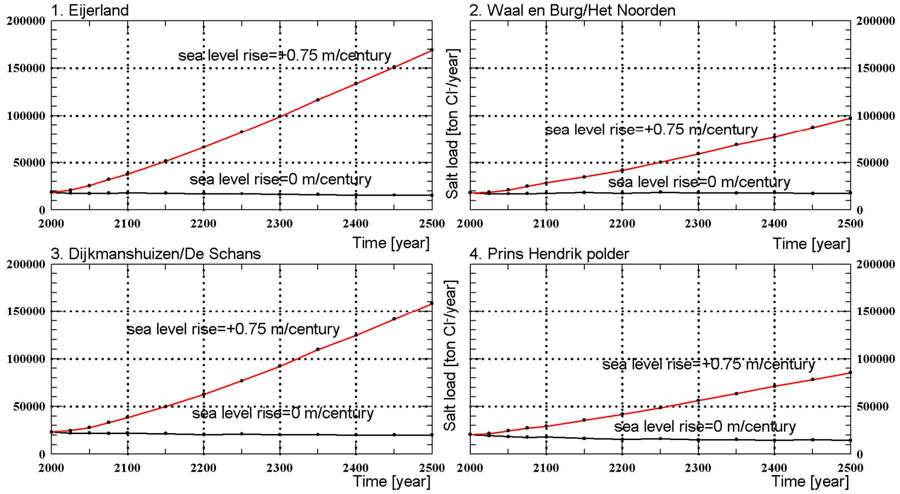


Texel

Texel: change in seepage of the four polders



Texel: change in salt load of the four polders



Model of the Province of Zuid-Holland

Case study: Province of Zuid-Holland

European water framework directive

“in 2015, state of all groundwaters and surface waters must be good“

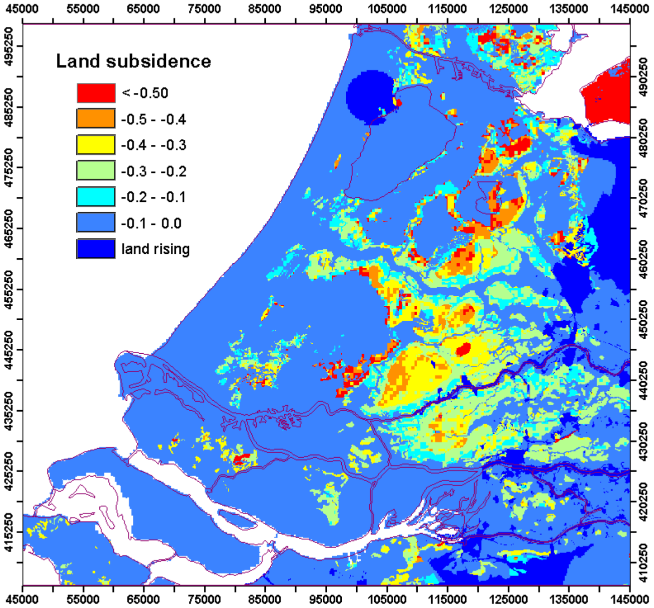
Identification of all fresh groundwater bodies in the province

How fast is the salinisation process?

More seepage, more salt load?

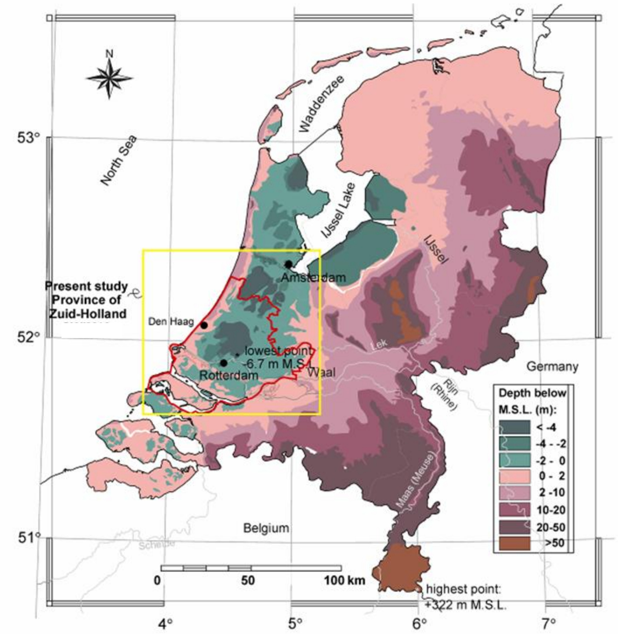
Land subsidence

2050



Source:
RIZA

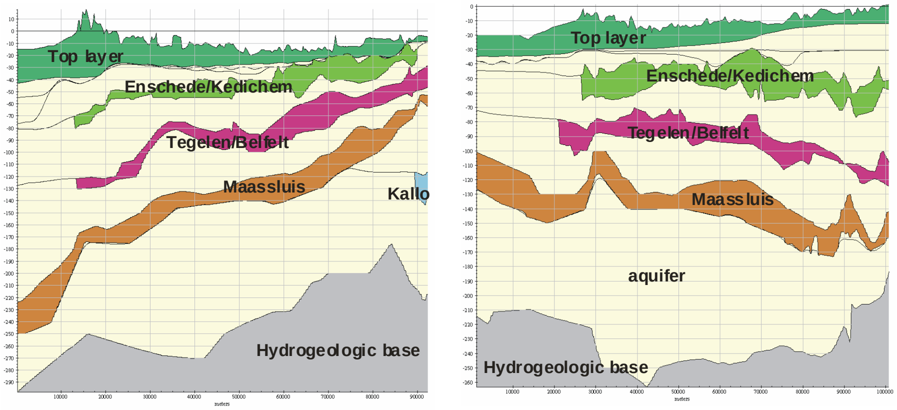
Location of the Province of Zuid-Holland



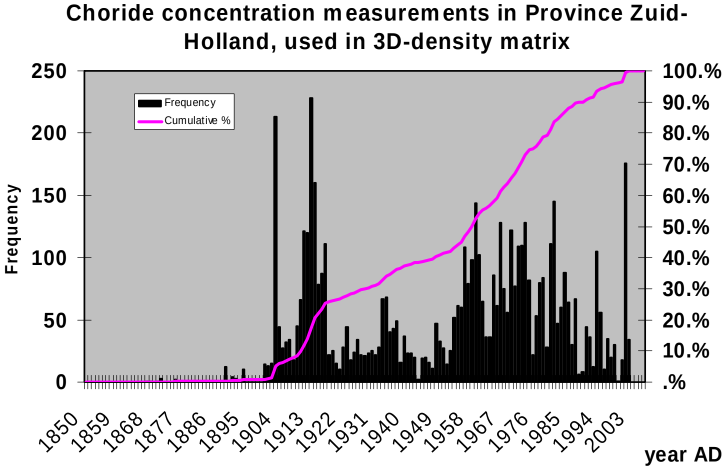
Numerical model description

- variable-density groundwater flow
- coupled solute transport
- MOCDENS3D
- area: 100km * 92.5km * 300m depth
- 400 *370 cells, 40 layers
- ~4 million active cells
- uses most accurate Dutch 3D subsurface schematization available
- 9 aquifers and aquitards
- uses 5772 chloride concentration measurements

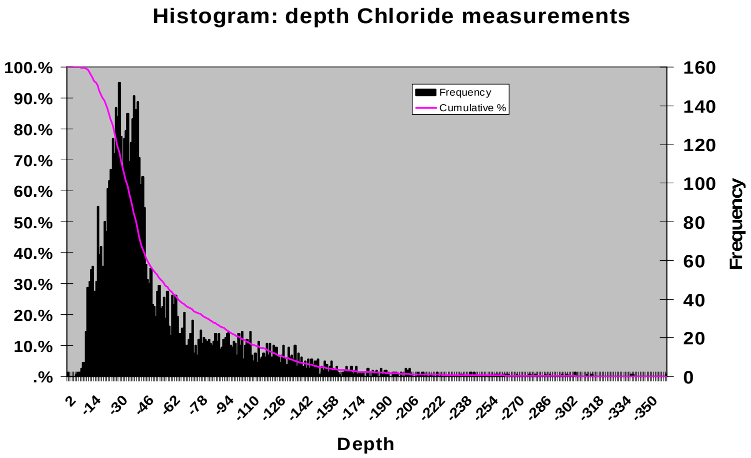
Position and name of aquitards



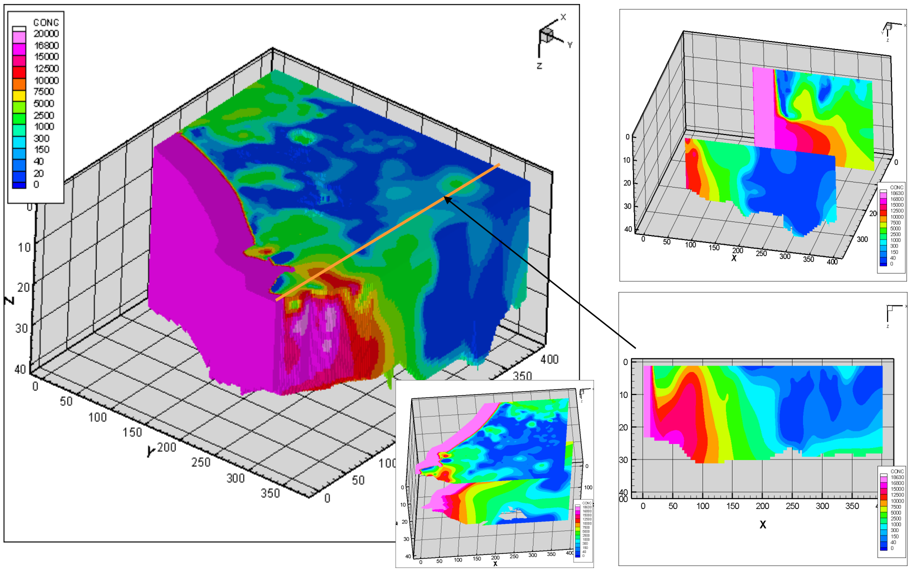
3D interpolation of chloride-concentration



3D interpolation of chloride-concentration



Initial chloride distribution

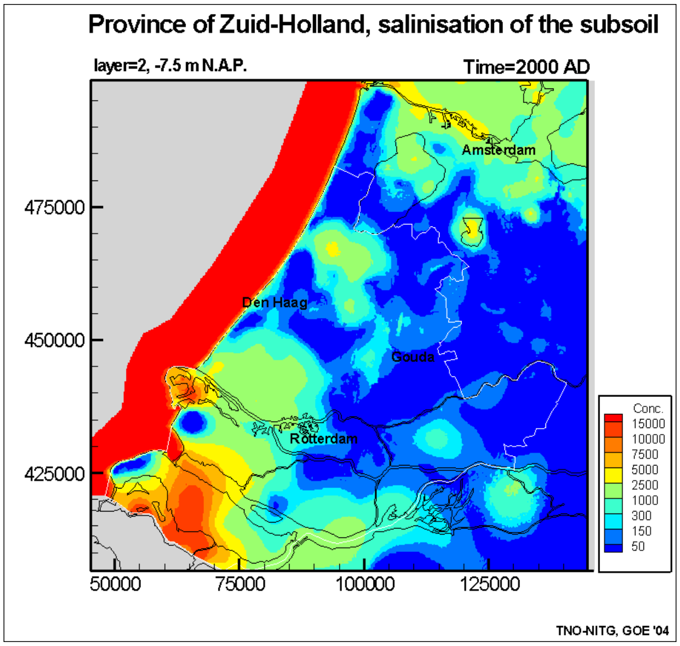


Present freshwater volume

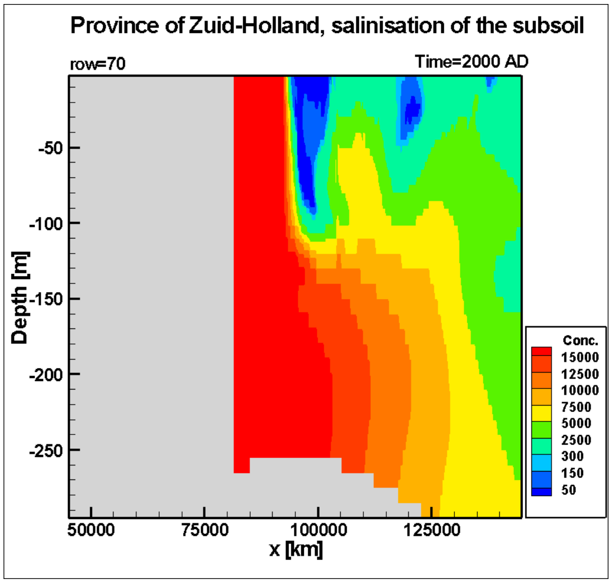
27 billion m^3

36% fresh, 14% brackish, 50% saline

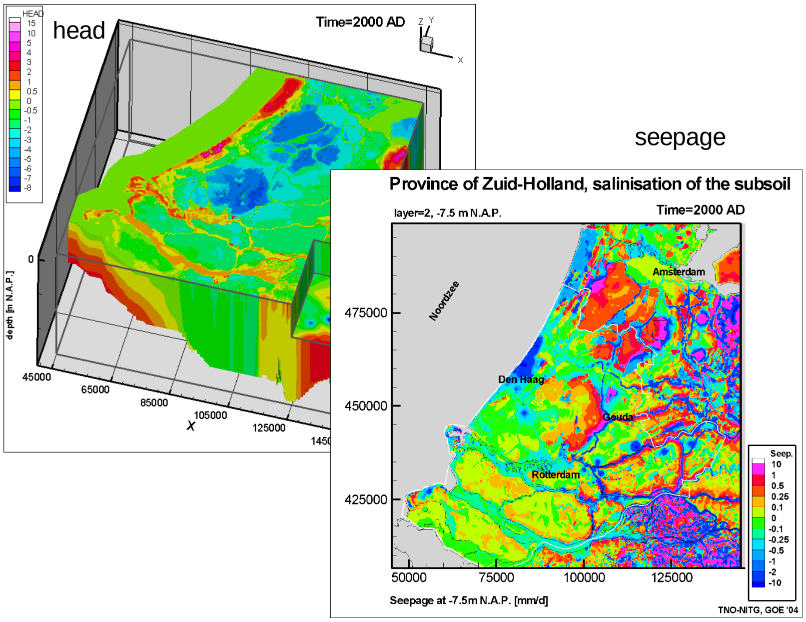
Results: Chloride conc. in 200 yrs



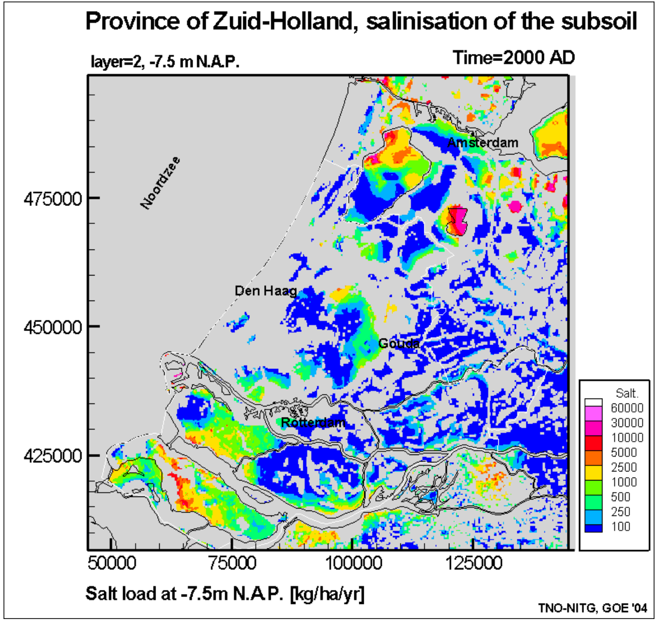
Results: Chloride conc. in 200 yrs



Results: freshwater head and seepage at 2000 AD



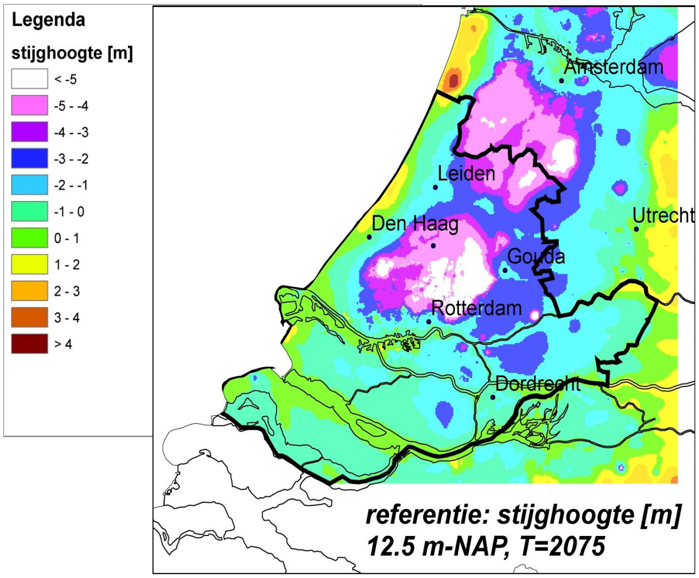
Results: Salt load in 200 yrs



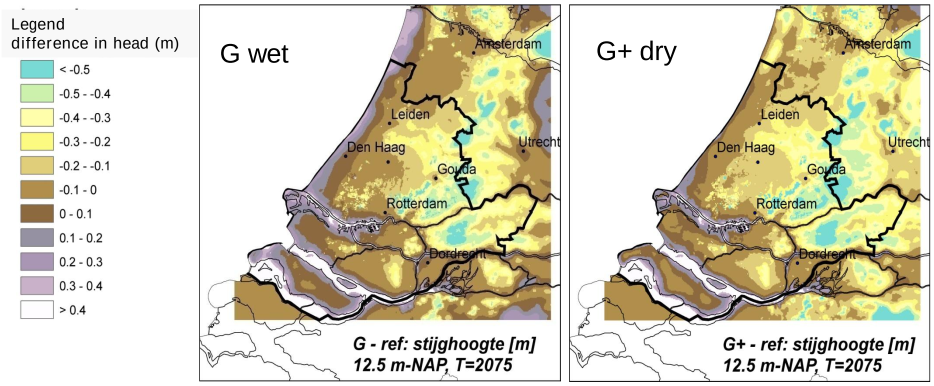
Effect sea level rise, change in natural groundwater recharge and land subsidence on freshwater head in aquifer

Some regional modelling results

Freshwater head at -12.5 M.S.L.



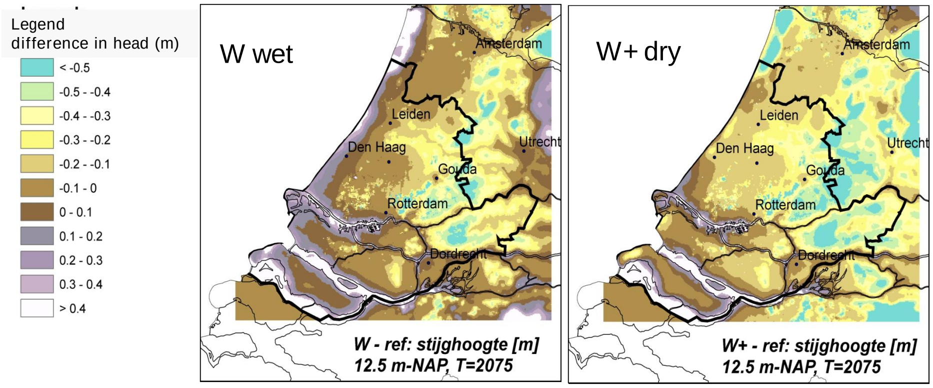
Difference in freshwater head on op -12.5 N.A.P.: G scenarios



Sea level rise is 60 cm

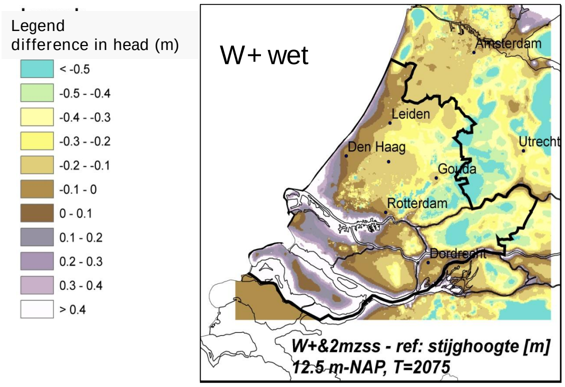
Including change in natural groundwater recharge

Difference in freshwater headon op -12.5 N.A.P.: W scenarios



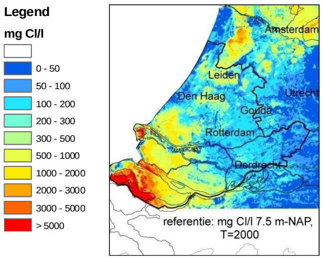
Sea level rise is 85 cm

Difference in freshwater headon op -12.5 N.A.P.: W scenarios



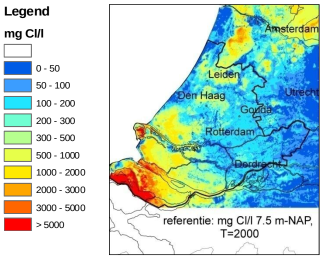
Sea level rise is 200 cm

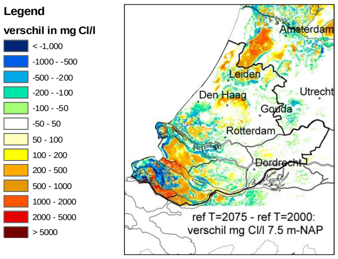
Salinisation/freshening Netherlands?: Present situation



modelstudy

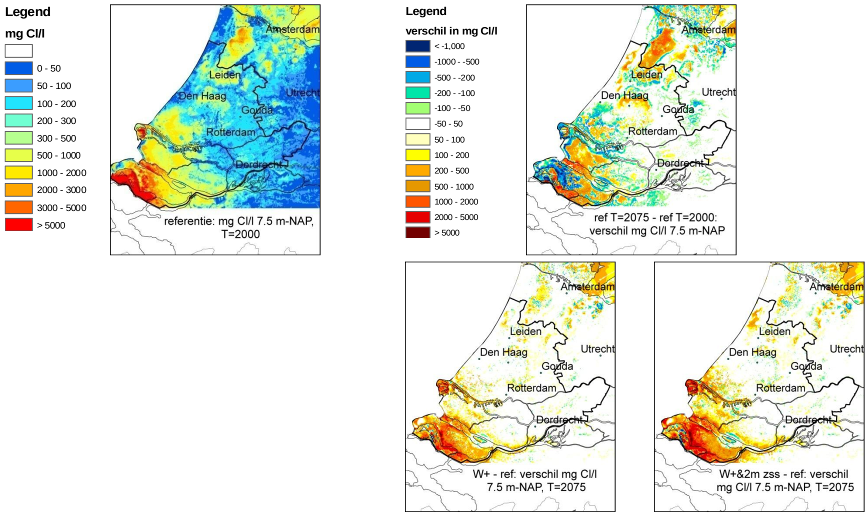
Salinisation/freshening Netherlands?: Autonomous processes





modelstudy

Salinisation/freshening Netherlands?: climate change



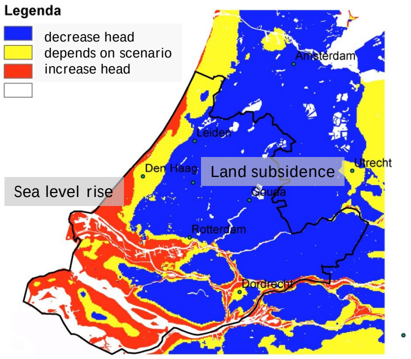
85 cm sea level rise

200 cm sea level rise

modelstudy

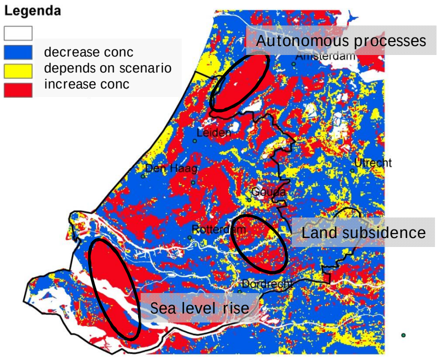
Effect climate scenarios in 2075 on

freshwater head



Increase or decrease head for all climate scenarios G, G+, W, W+

salinisation



Increase or decrease concentration for all climate scenarios G, G+, W, W+

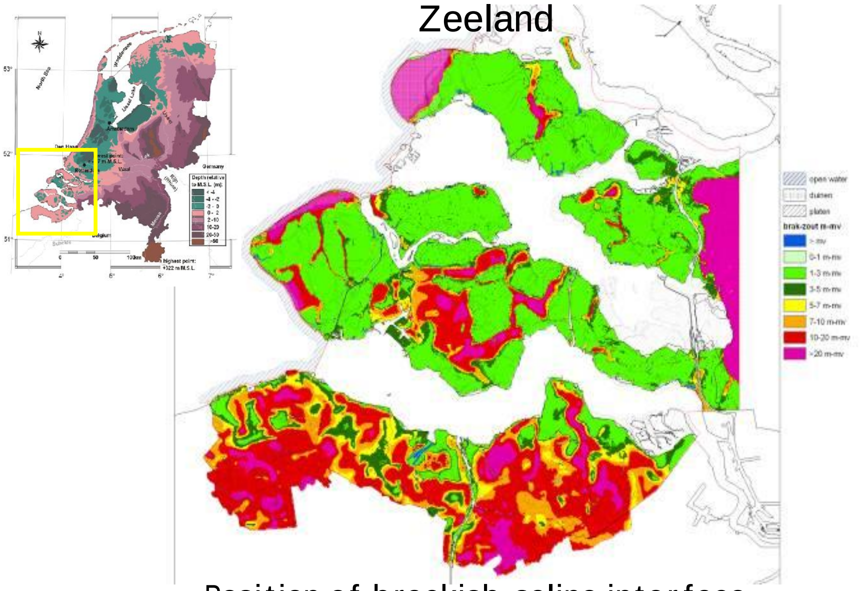
Modelstudie PZH

Rainwater lenses in an agricultural setting

Shallow dynamic freshwater bodies flowing upon brackish-saline groundwater

- density dependent
- dynamics: seasonal & long-year

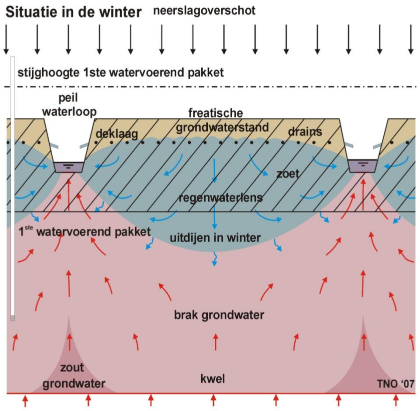
Salinisation of the phreatic groundwater in Zeeland



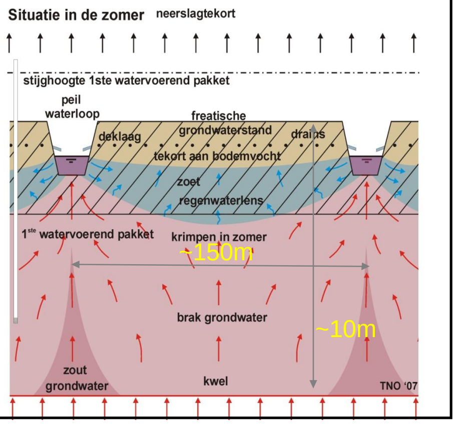
Position of brackish-saline interface

Salinisation of the phreatic groundwater in Zeeland

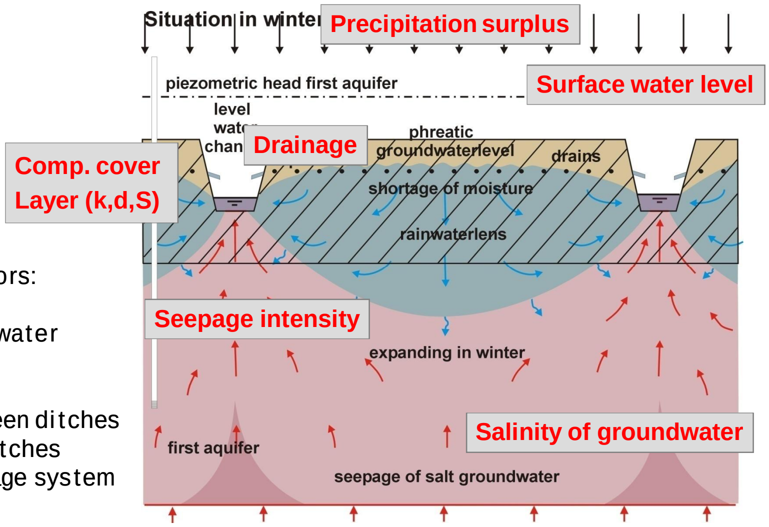
Dynamic rainwater lenses floating on saline groundwater



thickness rainwater lens varies due to the dynamics in seasonal and long-year natural groundwater recharge



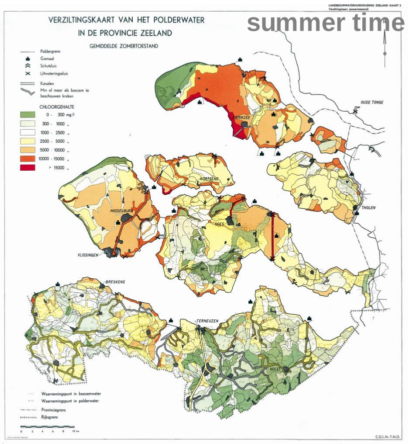
Factors controlling fresh-salt interface

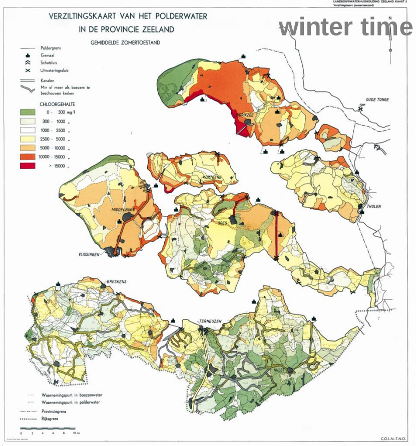


Important factors:

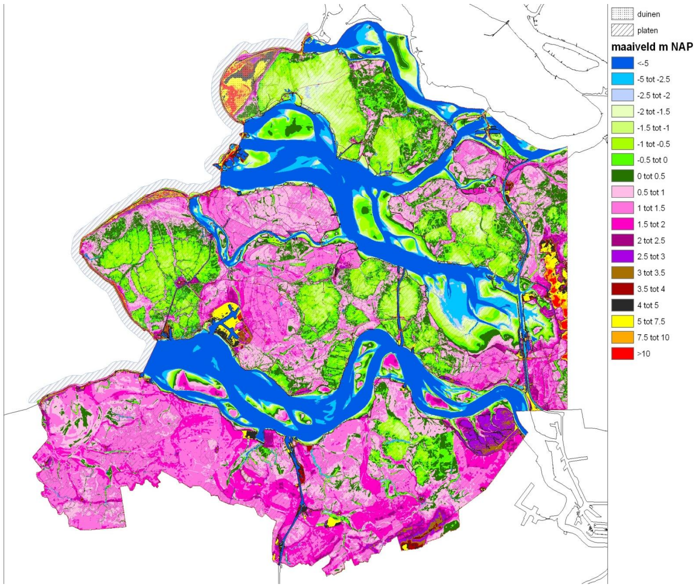
-natural groundwater recharge
-geology
-distance between ditches
-water levele ditches
-capacity drainage system

Salinisation surface water

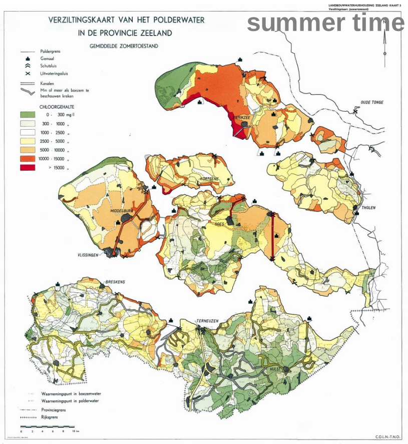


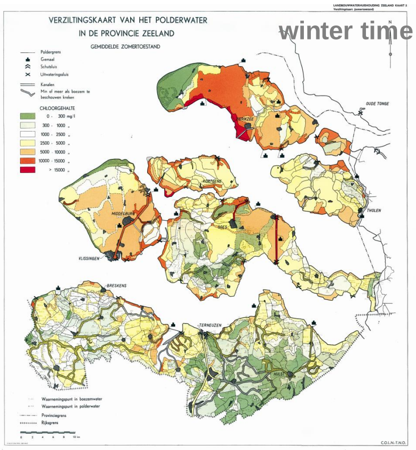


Position of the ground surface



Salinisation surface water





Problem definition dynamic freshwater lenses

Salt in the agricultural plots originates from:

- surface water system (irrigation water)
- groundwater system (salt load to the root zone)

The salinisation will increase due to:

- sea level rise
- climate change
- water level management

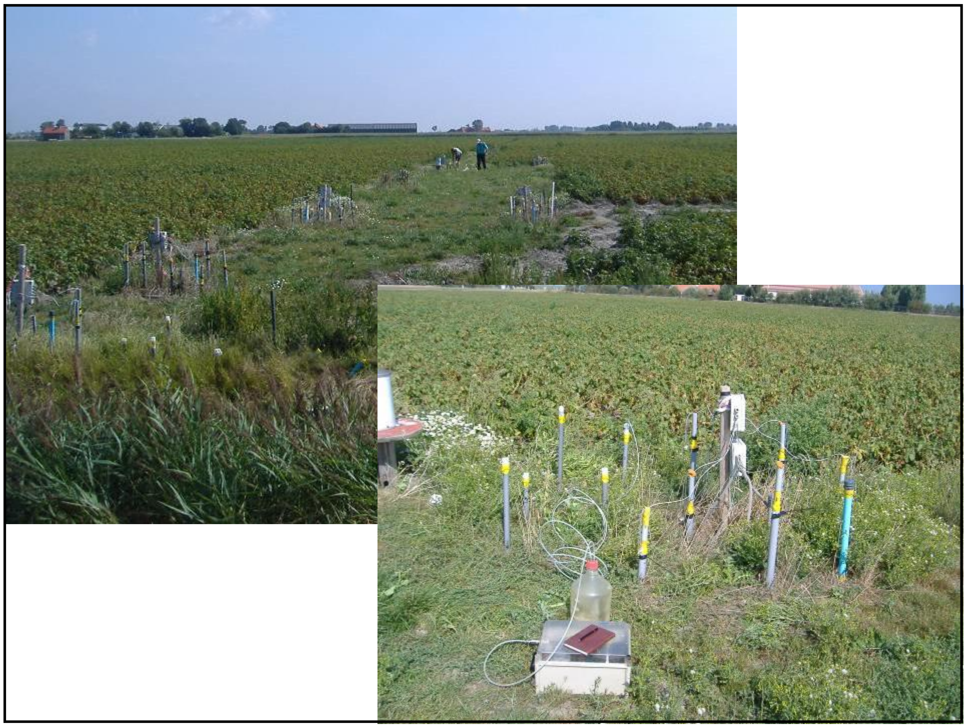
How to tackle the problem?

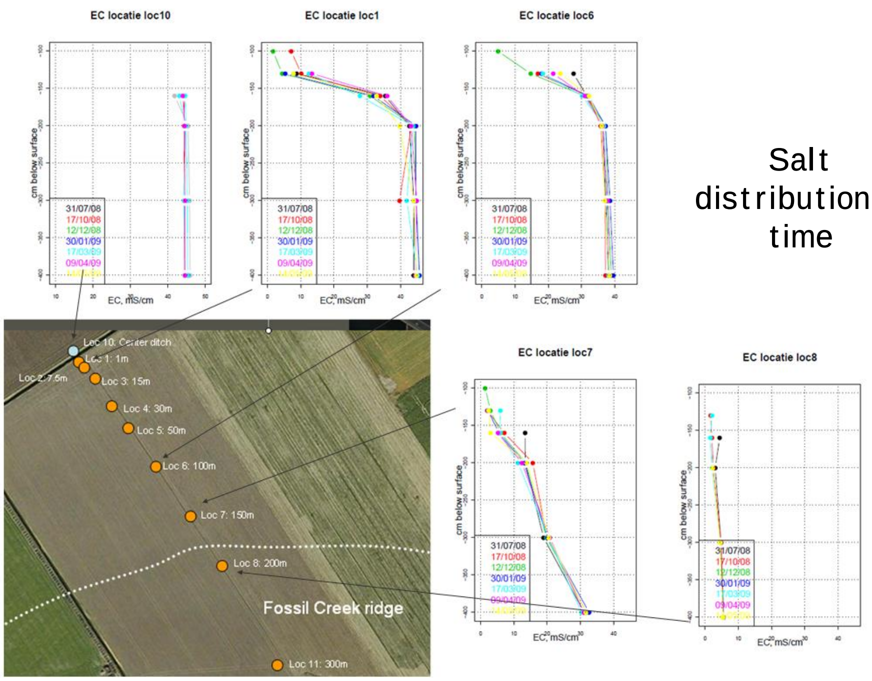
Field measurements at parcels

- fresh-brackish-salt interface at local scale using T-EC-probe and later CVES and ERT
- groundwater level and quality
- surface water level and quality

Modelling

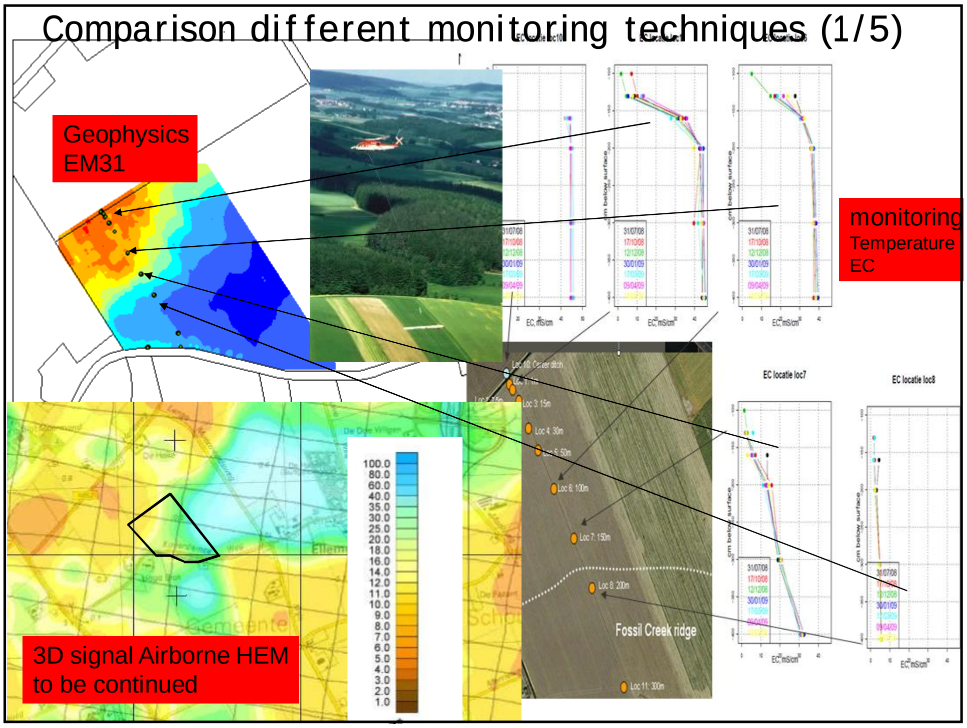
- density dependent groundwater flow
- two different scales:
  - regional scale: transect perpendicular at coast
  - local scale: parcel between two ditches





Salt distribution in time

- TEC
- sampling
- EM31
- CVES
- HEM
- ECPT
- Numerical models (2D and 3D)

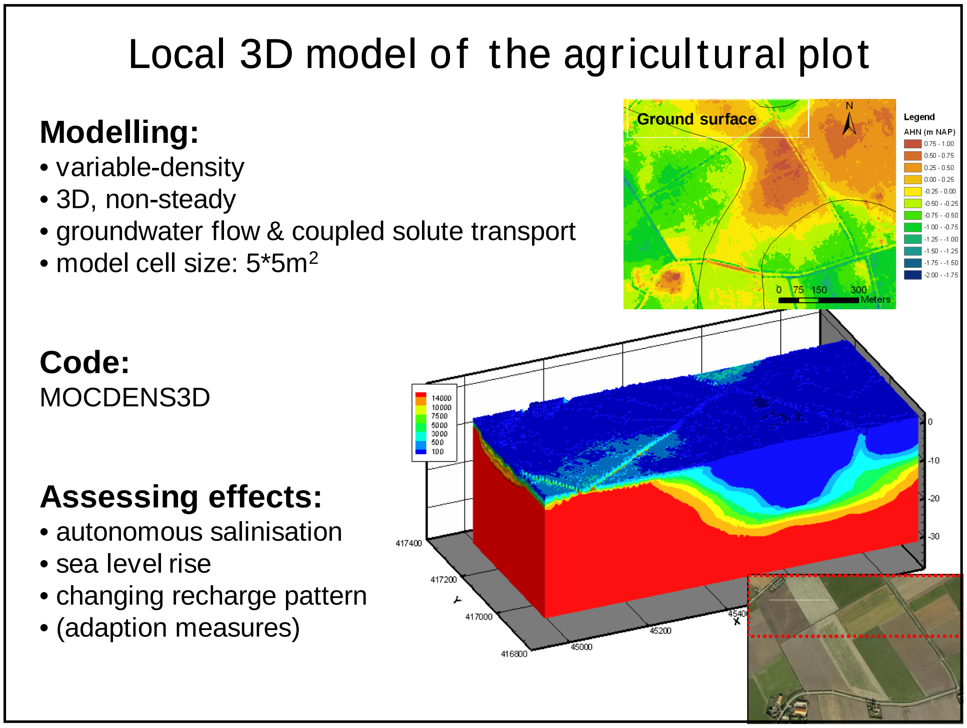


Comparison different monitoring techniques (1/5)

Geophysics EM31

monitoring Temperature EC

3D signal Airborne HEM to be continued



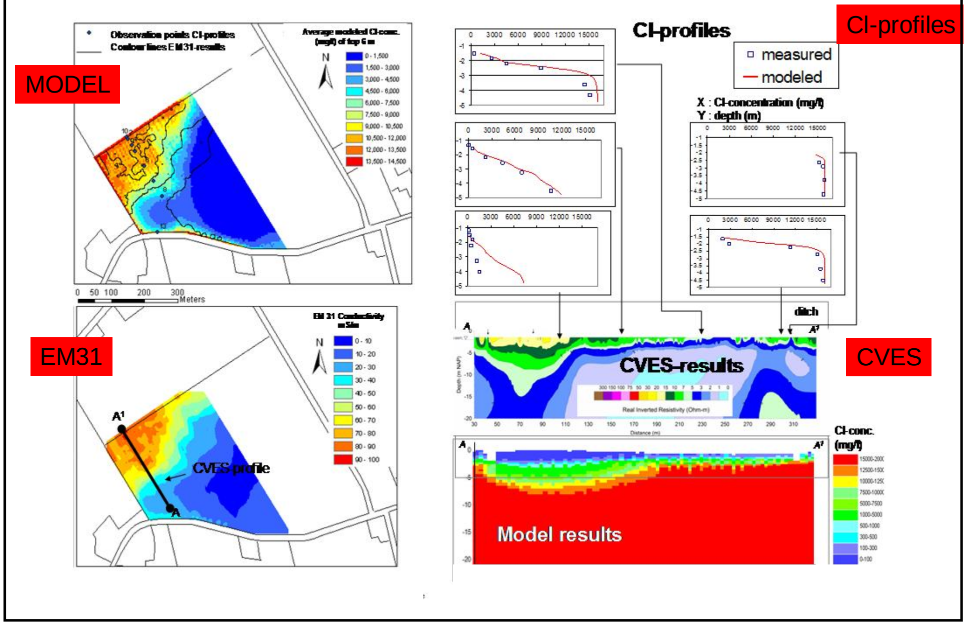
Local 3D model of the agricultural plot

Modelling:
- variable-density
- 3D, non-steady
- groundwater flow & coupled solute transport
- model cell size: 5*5m^2

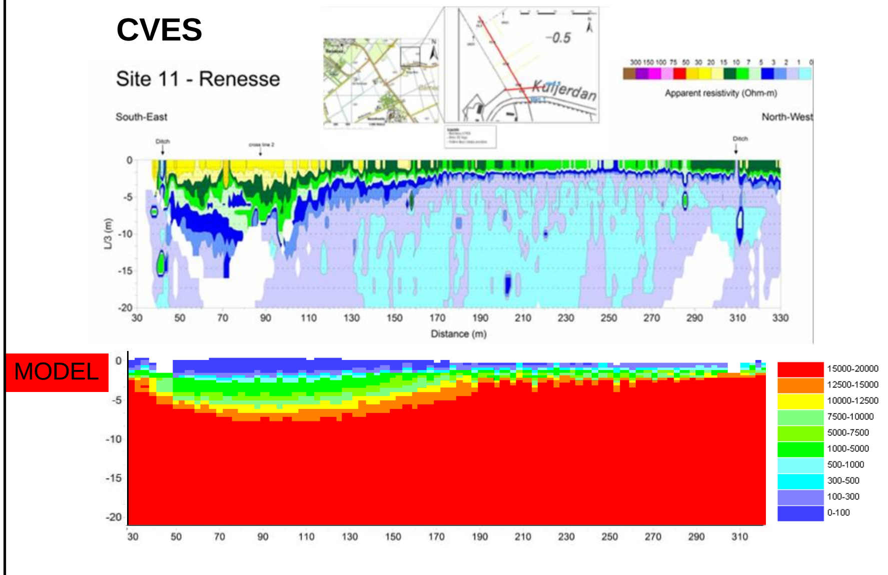
Code:
MOCDENS3D

Assessing effects:
- autonomous salinisation
- sea level rise
- changing recharge pattern
- (adaption measures)

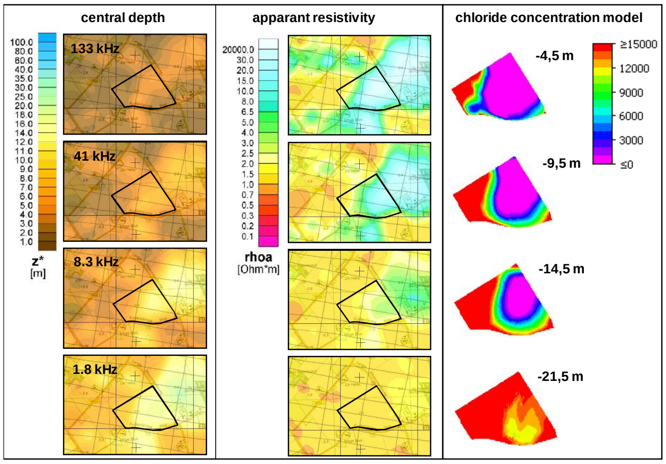
Comparison model with EM31, CVES, profiles



Comparison 3D model and CVES

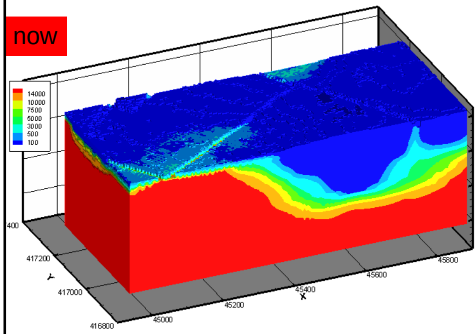


HEM data

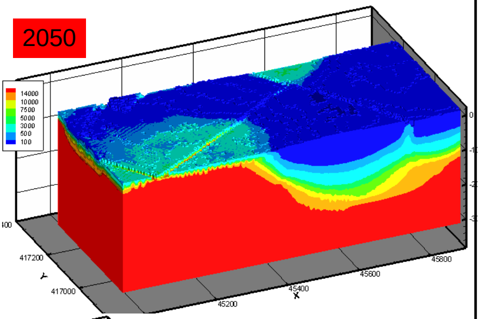


Climate change scenario (dry): model result

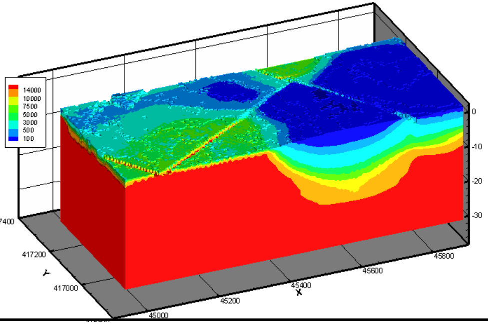
now



2050



2100



To be continued...

- Implementing more realisations of 3D geology and initial 3D fresh-saline
  - Analyse the differences
- Running climate change scenarios (on national and regional level)
  - Effect on surface water (salt load)
  - Effect on root zone (rainwater lenses)
  - Effect on freshwater volumes (drinking water)
- Compare model results of different scales and give recommendations

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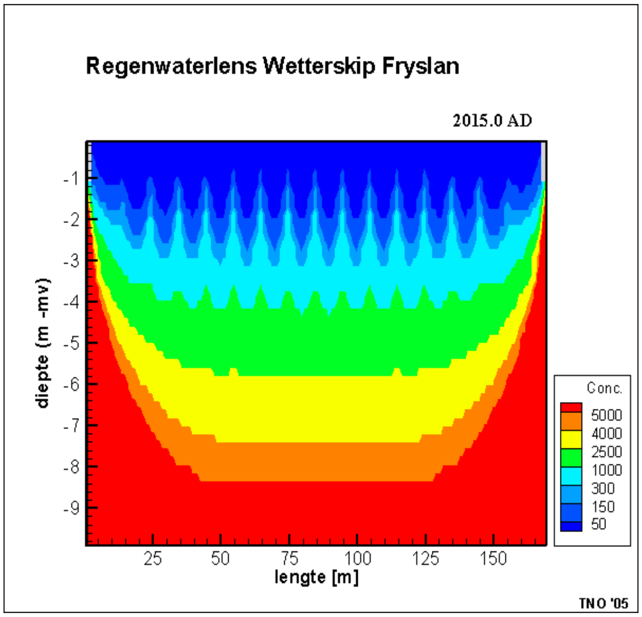
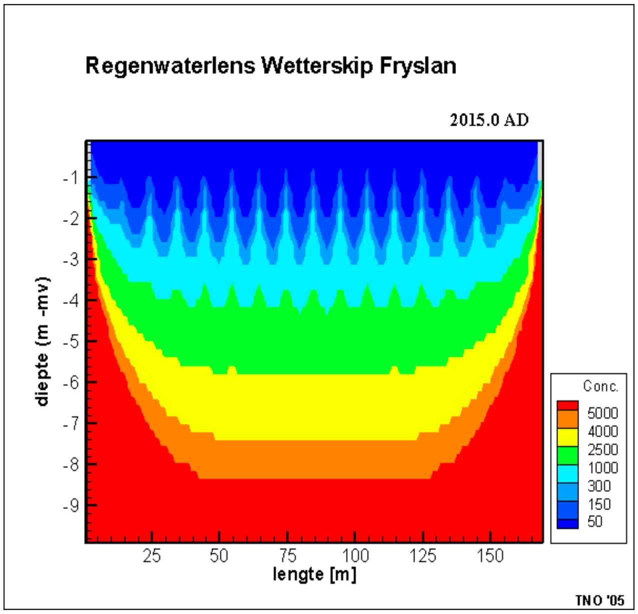
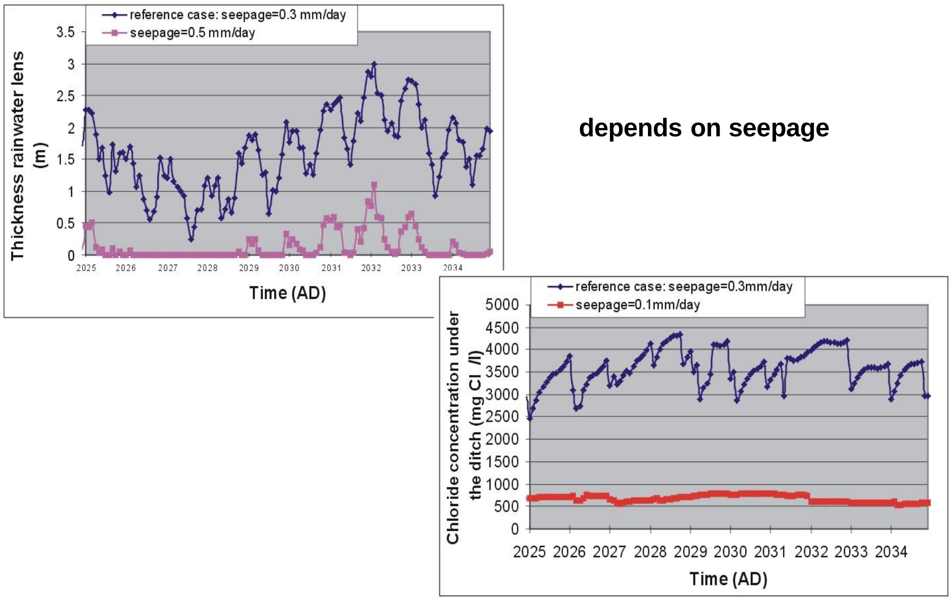
Model the dynamics of fresh-brackish-salt interface



Model the dynamics of fresh-brackish-salt interface



Thickness of the lens and salt load to surface water varies



depends on seepage

Conclusions (salinisation Dutch aquifers):

- Salinisation in the Netherlands is a non-stationary process
- Three physical processes threaten the Dutch aquifers:
  - autonomous development
  - land subsidence
  - sea level rise
- Increase in seepage and salt load can be severe during the coming 50/100 years
- Modelling techniques are available to assess possible effects

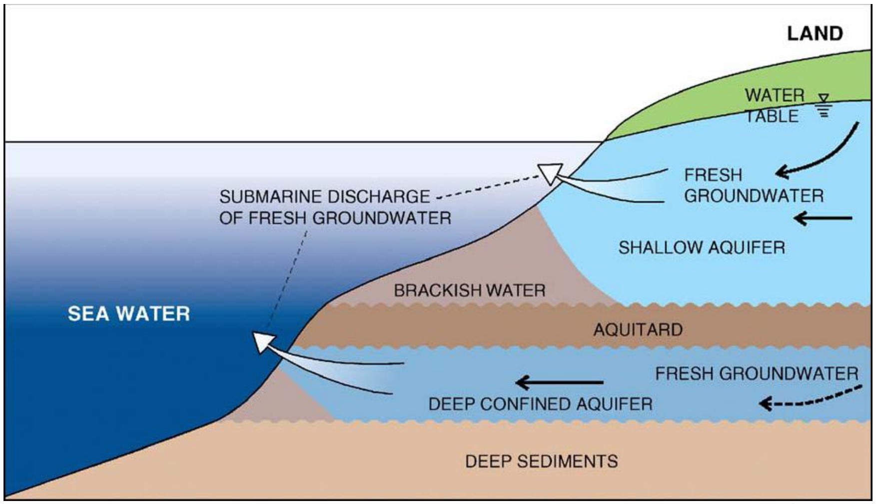
Recommendations (salinisation Dutch aquifers):

- Number of quality measurements should be increased

- Feasibility study is necessary to implement potential technical measures to compensate salt water intrusion

What is Submarine Groundwater Discharge (SGD)?

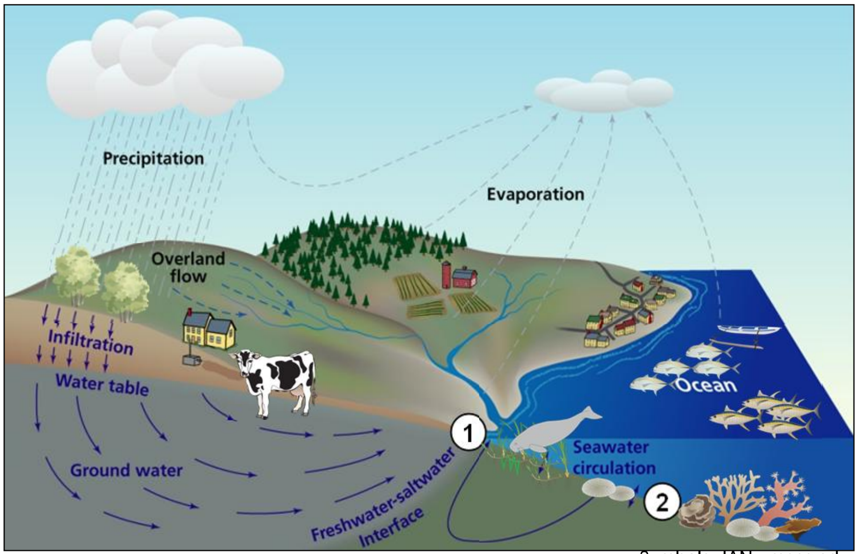
any flow of water out across the sea floor



Burnett et al, 2006

Why study SGD?

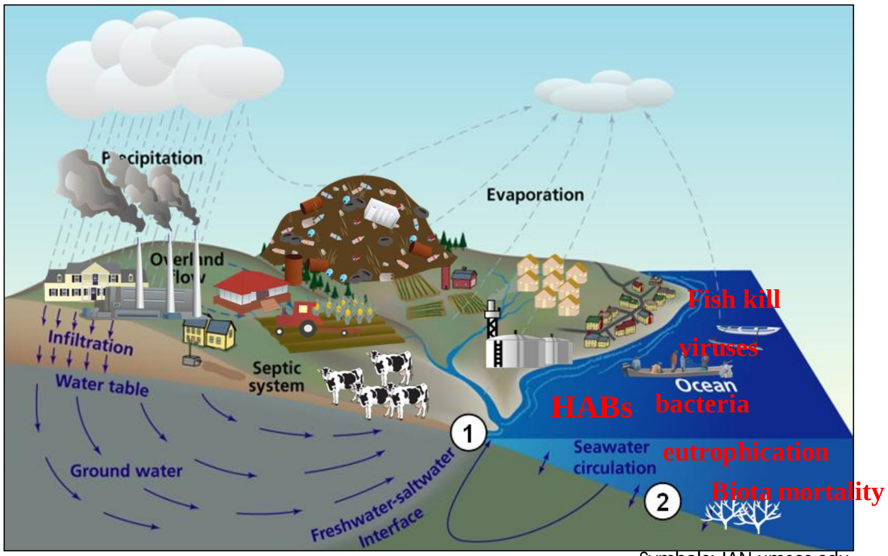
Nutrients are transported from land to sea via SGD pathway



Symbols: IAN.umces.edu

Why study SGD?

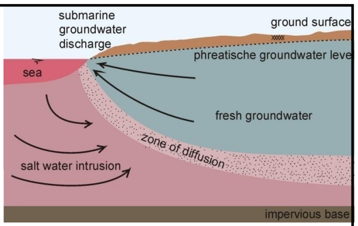
Nutrients are transported from land to sea via SGD pathway

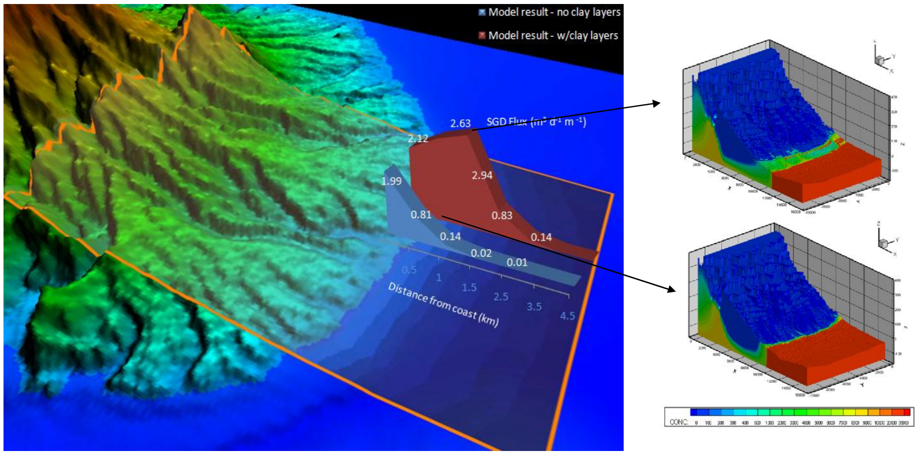


Symbols: IAN.umces.edu

Philippines

Submarine Groundwater Discharge





Conclusions (modelling of variable-density flow)

- Don’t use the Henry problem to test your variable-density code
- Use enough cells to model the Hydrocoin and Elder problem

For modelling 3D systems:

- Remember the Peclet discretisation limitation for cell sizes (unless you’re using the method of characteristics!)
- Longitudinal dispersivity should not be too large (e.g. <10m)
- It’s important to derive a very accurate density distribution (as that significantly effects the velocity field!)
- Watch out for numerical problems at the outflow face to the sea

Challenges for the future

- Improve the 3D density matrix, e.g. by more types of measurements
- Implement effect of climate change and sea level rise on coastal aquifers
- Optimalisation of (ground)water management in coastal aquifers by using 3D variable-density flow models
- Improve calibration of 3D models by using transient data of solute concentrations
- Incorporate reactive multicomponent solute transport

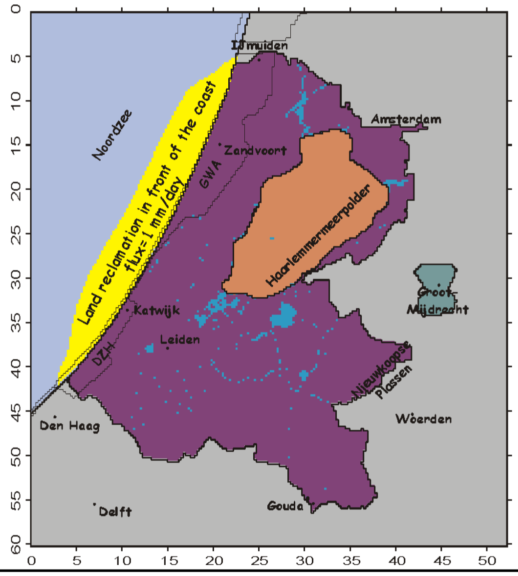
Solutions

Possible measures to compensate salt water intrusion

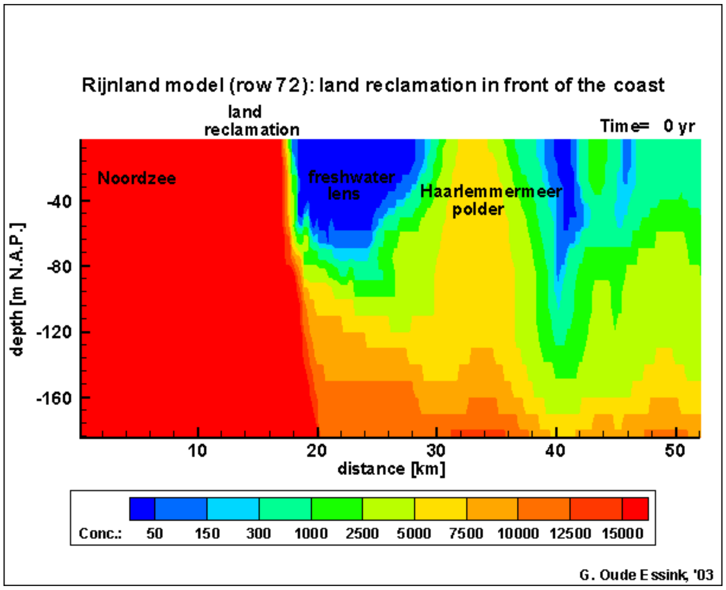
1. Land reclamation in front of the coast
2. Inundation of low-lying polders
3. Extraction of saline/brackish groundwater
4. Infiltration of fresh surface water
5. Creating physical barriers

Rijnland

1. Rijnland model: land reclamation case



1. Land reclamation in front of the coast



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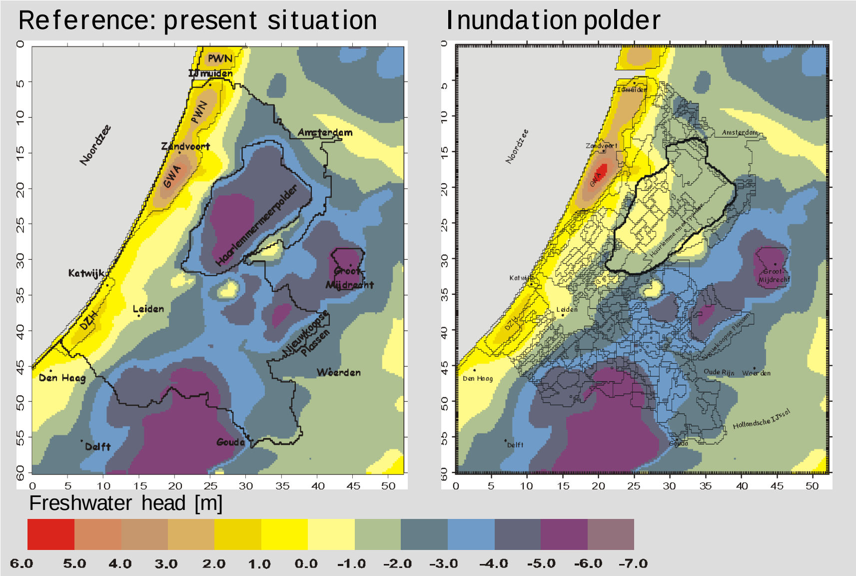
2. Rijnland model: Inundation Haarlemmermeerpolder

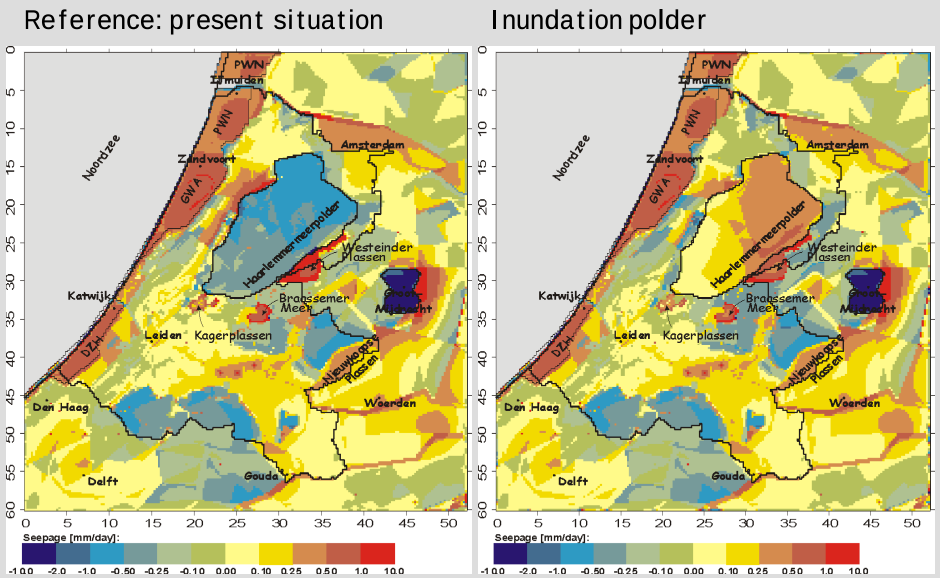
Calculated present phreatic water head



Rijnland

2. Rijnland model : Inundation Haarlemmermeerpolder

Calculated seepage and infiltration on –10 m M.S.L.

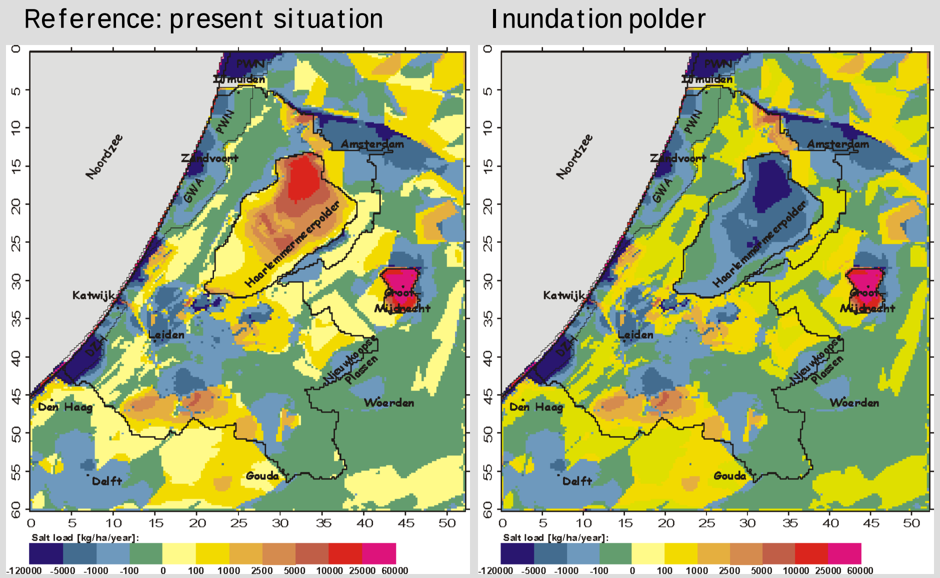

Reference: present situation

Inundation polder

Rijnland

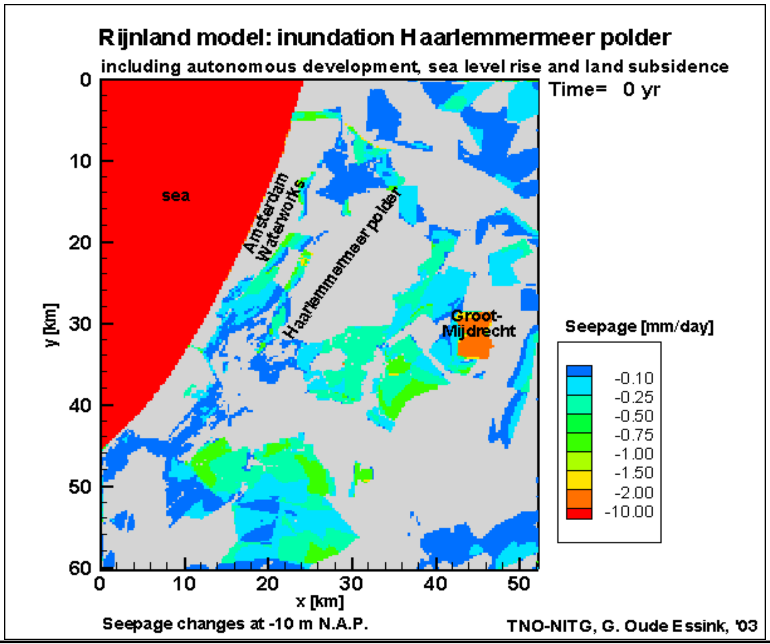
2. Rijnland model: Inundation Haarlemmermeerpolder

Calculated salt load on –10 m M.S.L.


Reference: present situation

Inundation polder

2. Rijnland model: Inundation Haarlemmermeerpolder



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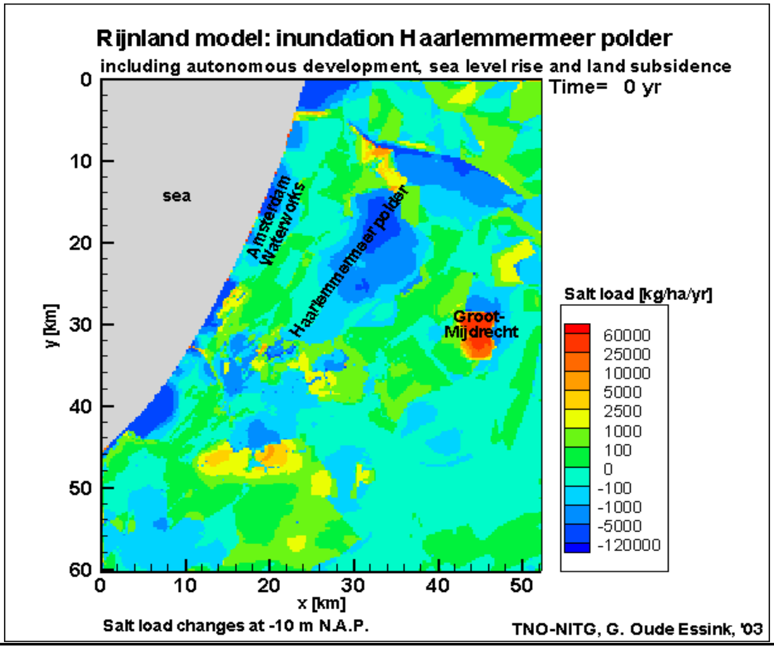
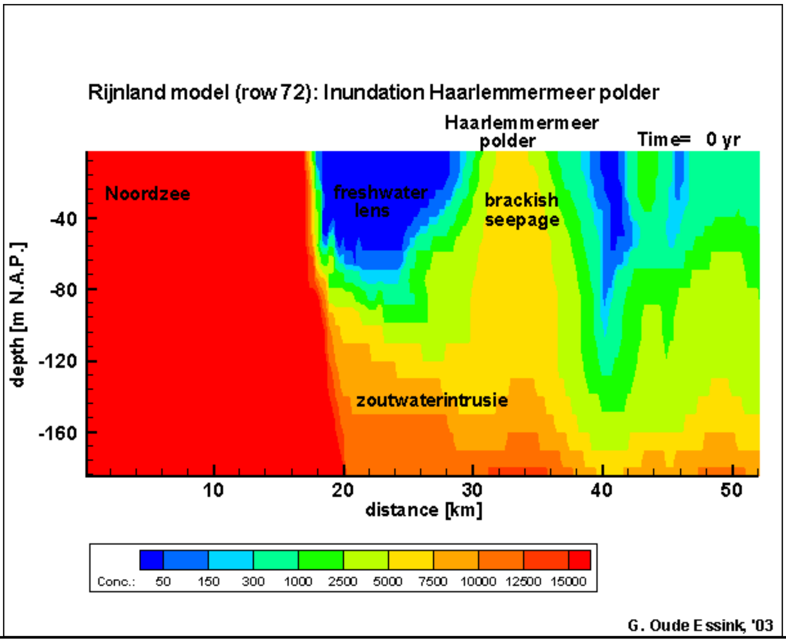
2. Rijnland model: Inundation Haarlemmermeerpolder



Rijnland

2. Rijnland model: Inundation Haarl.polder (conc, 500 jr)


Rijnland model (row 72): Inundation Haarlemmermeer polder

G. Oude Essink, '03

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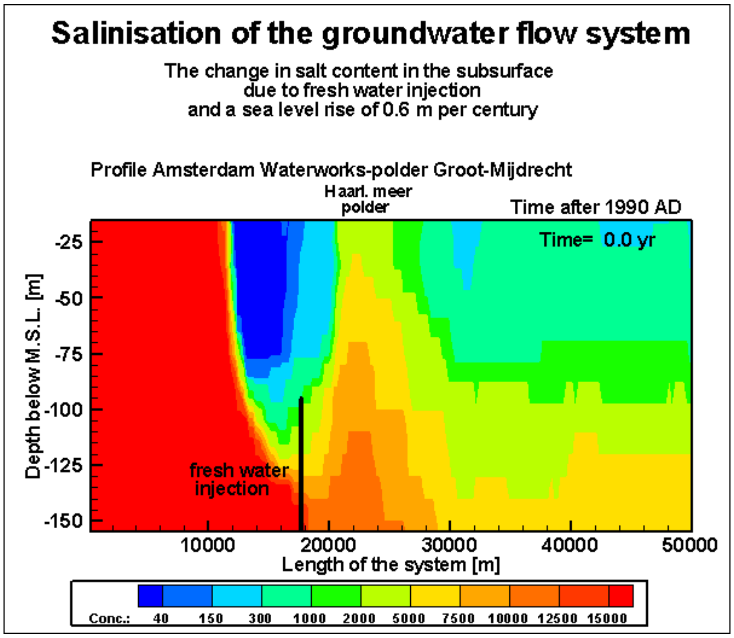
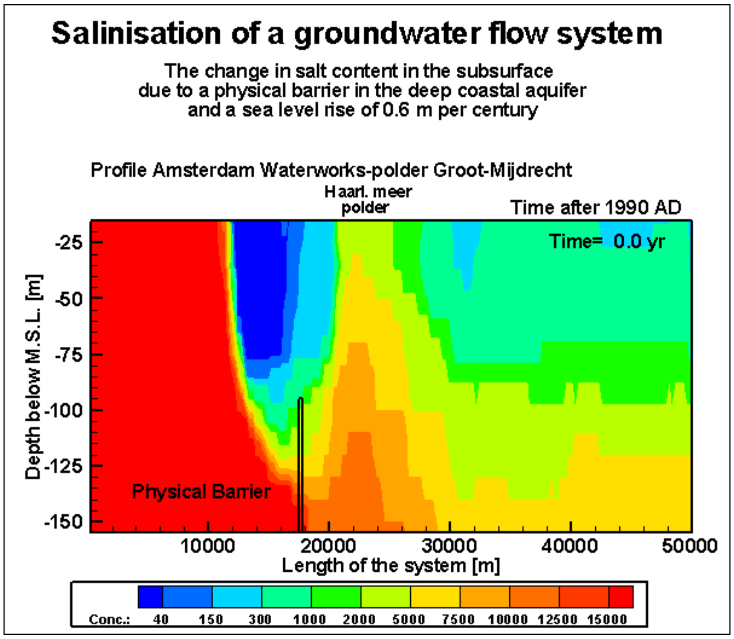
4. Injection of fresh water (conc, 1000 yr)


Salinisation of the groundwater flow system

The change in salt content in the subsurface
due to fresh water injection
and a sea level rise of 0.6 m per century

Profile Amsterdam Waterworks-polder Groot-Mijdrecht

5. Physical barrier (conc, 1000 yr)



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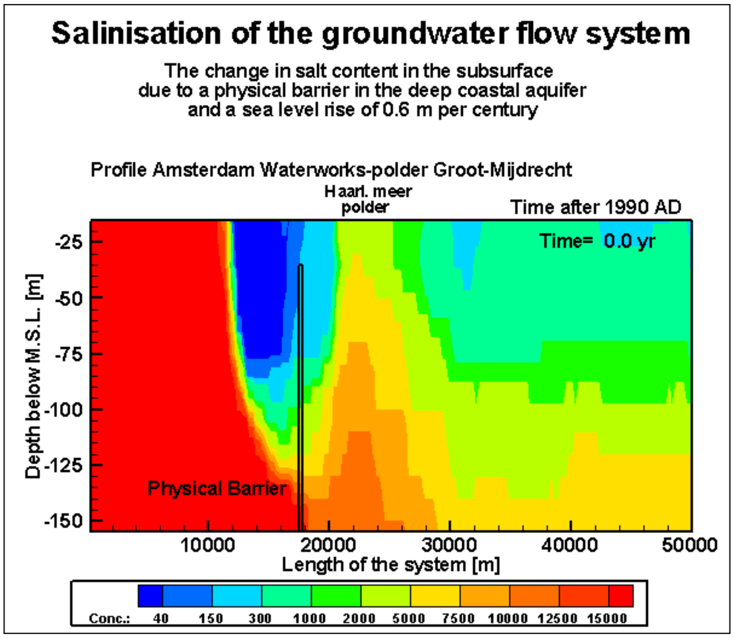
5. Physical barrier (conc, 1000 yr)



Solute transport models

Combine
the groundwater flow equation
and
the advection-dispersion equation
by means of
an equation of state

Solute transport equation

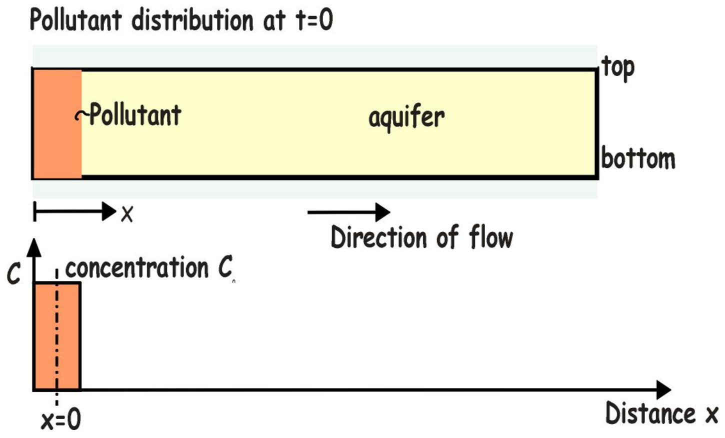
Partial differential equation (PDE):

$$R_d \frac{\partial C}{\partial t} = \frac{\partial}{\partial x_i}\left(D_{ij}\frac{\partial C}{\partial x_j}\right) - \frac{\partial}{\partial x_i}(CV_i) + \frac{(C-C)'W}{n_e} - R_d \lambda C$$

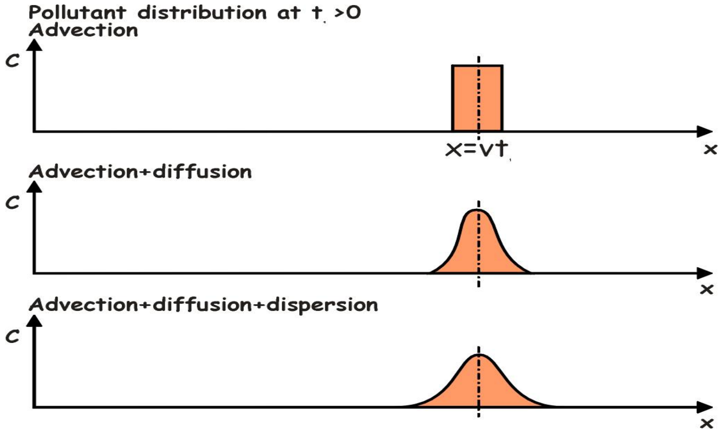
change dispersion advection source/sink decay
in concentration diffusion

D_{ij}=hydrodynamic dispersion [$L^2 T^{-1}$]
R_d=retardation factor [-]
λ=decay-term [T^{-1}]

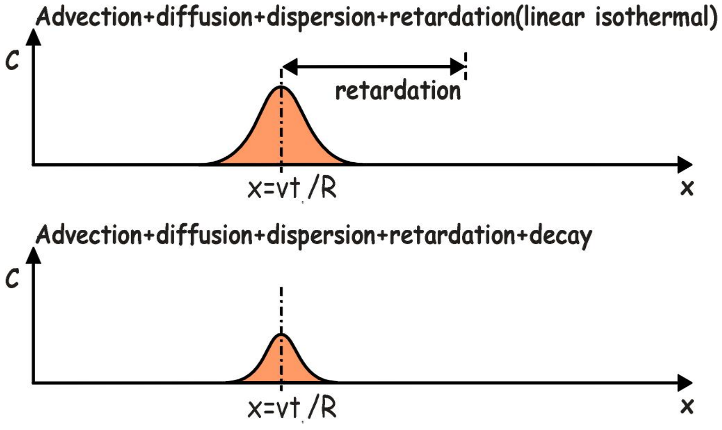
Solute transport equation: column test (I):



Solute transport equation: column test (II):



Solute transport equation: column test (III):



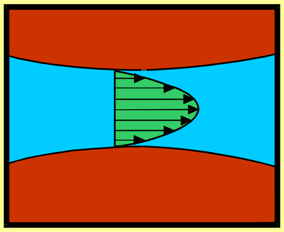
Hydrodynamic dispersion

hydrodynamic dispersion
=
mechanical dispersion+ diffusion

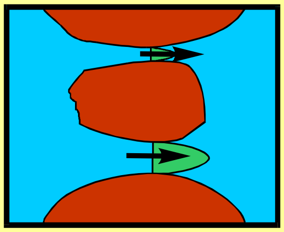
mechanical dispersion:
- tensor
- velocity dependant

diffusion:
- molecular process
- solutes spread due to concentration differences

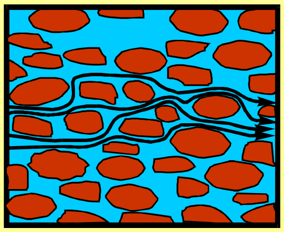
Mechanical dispersion



Differences in velocity in the pore



Differences in velocity due to variation in pore-dimension



Differences in velocity due to variation in velocity direction

Solute transport equation: diffusion (I)

diffusion is a slow process: diffusion equation

only 1D-diffusion means: R_d=1, V_f=0, λ=0 and W=0

$$\frac{\partial C}{\partial t} = D\frac{\partial^2 C}{\partial z^2}$$

similarity with non-steady state groundwater flow equation

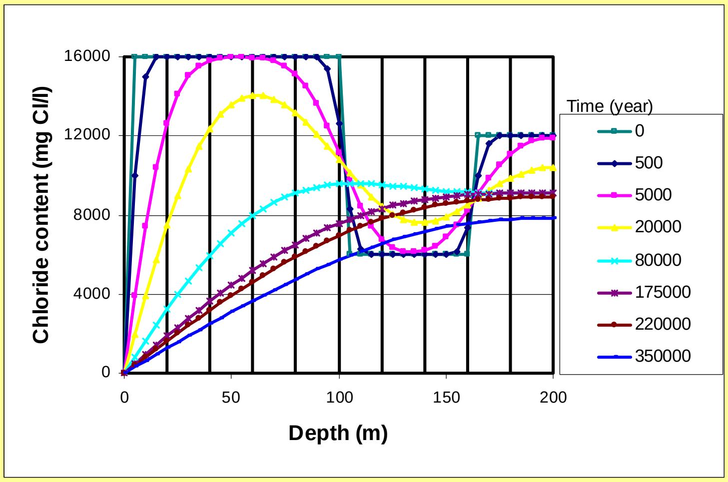
$$S\frac{\partial \phi}{\partial t} = T\frac{\partial^2 \phi}{\partial x^2} + N \qquad \frac{T\Delta t}{S\Delta x^2} < 0.5$$

$$\phi_i^{t+\Delta t} = \phi_i^t + \frac{N\Delta t}{S} + \frac{T\Delta t}{S\Delta x^2}\left(\phi_{i+1}^t - 2\phi_i^t + \phi_{i-1}^t\right)$$

$$C_i^{t+\Delta t} = C_i^t + \frac{D\Delta t}{\Delta z^2}\left(C_{i+1}^t - 2C_i^t + C_{i-1}^t\right) \qquad \frac{D\Delta t}{\Delta z^2} < 0.5$$

Solute transport equation: diffusion (II)

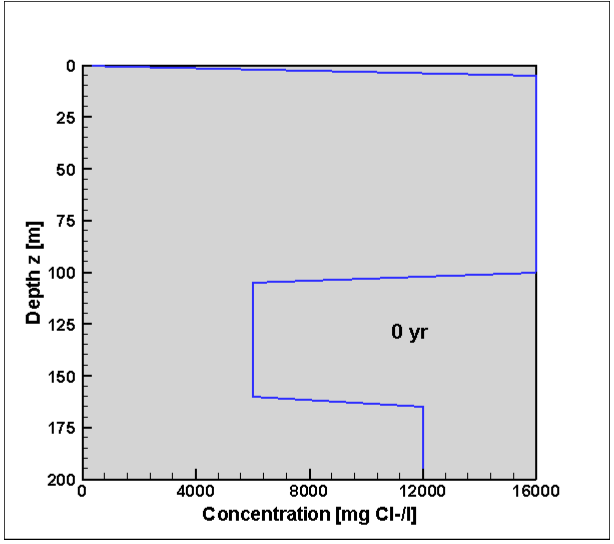
diffusion is a slow process: diffusion equation $\frac{\partial C}{\partial t} = D\frac{\partial^2 C}{\partial z^2}$



modelling

Solute transport equation: diffusion (III)

Animation as a function of 350.000 years



MOCDENS3D

Groundwater flow equation (MODFLOW, 1988)

Darcy

$$q_x = -\frac{\kappa_x \rho_f g}{\mu}\frac{\partial \phi_f}{\partial x}; \quad q_y = -\frac{\kappa_y \rho_f g}{\mu}\frac{\partial \phi_f}{\partial y}; \quad q_z = -\frac{\kappa_z \rho_f g}{\mu}\left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

Continuity

$$-\left[\frac{\partial \rho q_x}{\partial x} + \frac{\partial \rho q_y}{\partial y} + \frac{\partial \rho q_z}{\partial z}\right] = \frac{\partial n \rho}{\partial t} + W$$

buoyancy term

Freshwater head

$$\phi_f = \frac{p}{\rho_f g} + z$$

Advection-dispersion equation (MOC3D, 1996)

$$\frac{\partial C}{\partial t} = \frac{1}{nR_f}\frac{\partial}{\partial x_i}\left(nD_{ij}\frac{\partial C}{\partial x_j}\right) - \frac{V_i}{R_f}\frac{\partial C}{\partial x_i} + \frac{\sum[W(C' - C)]}{nR_f} - \lambda C$$

Equation of state: relation density & concentration

$$\rho_{\mathrm{i,j,k}} = \rho_f(1 + \beta C_{i,j,k})$$

MOCDENS3D

MOCDENS3D is based on MODFLOW

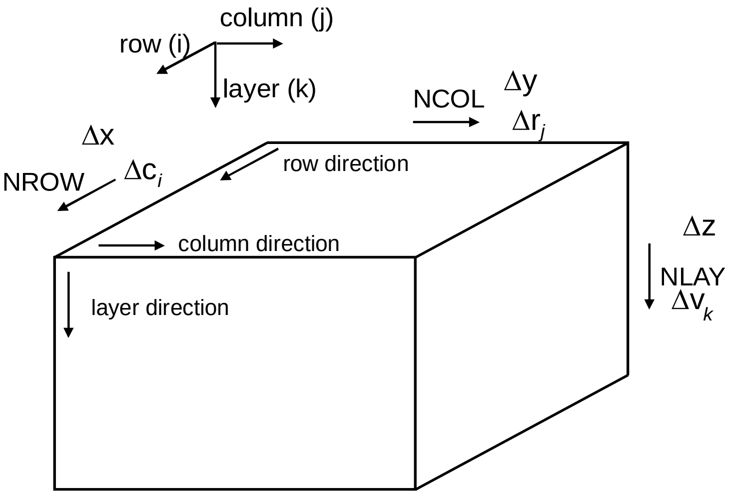
a modular 3D finite-difference ground-water flow model

(M.G. McDonald & A.W. Harbaugh, from 1983 on)

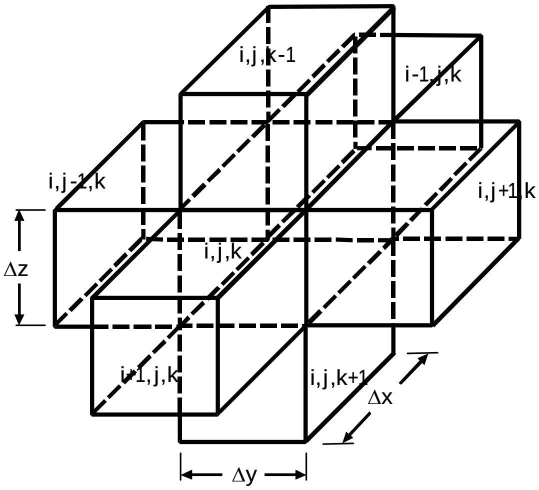
- USGS, ‘public domain’
- non steady state
- heterogeneous porous medium
- anisotropy
- coupled to reactive solute transport
    - MOC3 (Konikow *et al*, 1996)
    - MT3D, MT3DMS (Zheng, 1990)
    - RT3D
    - PHT3D (Prommer, 2004)
- easy to use due to numerous Graphical User Interfaces (GUI’s)
    - PMWIN, GMS, Visual Modflow, Argus One, Groundwater Vistas, etc.

MODFLOW

Nomenclature MODFLOW element [i,j,k]



MODFLOW: start with water balance of one element [i,j,k]



Continuity equation (I)

In - Out = Storage

$$\frac{\partial}{\partial x}\left(k_{xx}\frac{\partial\phi}{\partial x}\right)+\frac{\partial}{\partial y}\left(k_{yy}\frac{\partial\phi}{\partial y}\right)+\frac{\partial}{\partial z}\left(k_{zz}\frac{\partial\phi}{\partial z}\right)-W=S_s\frac{\partial\phi}{\partial t}$$

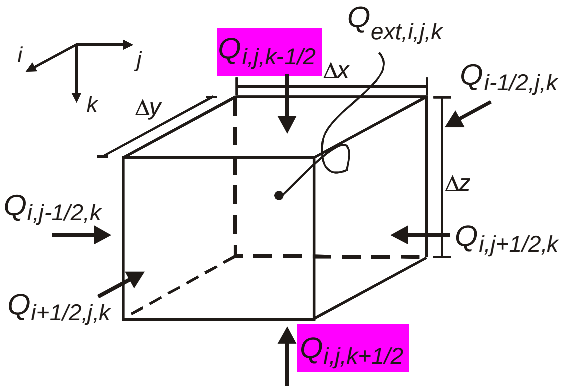
$$\sum Q_i = S_s\frac{\Delta\phi}{\Delta t}\Delta V$$

MOCDENS3D

Continuity equation (II)

$$\sum Q_i = S_s \frac{\Delta\phi}{\Delta t}\Delta V$$

In = positive



$$Q_{i,j-1/2,k} + Q_{i,j+1/2,k} + Q_{i-1/2,j,k} + Q_{i+1/2,j,k} + Q_{i,j,k-1/2} + Q_{i,j,k+1/2} + Q_{ext,i,j,k}$$
$$= SS_{i,j,k}\frac{\phi^{t}_{i,j,k} - \phi^{t+\Delta t}_{i,j,k}}{\Delta t}\Delta V$$

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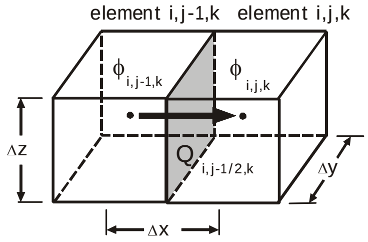
Flow equation (Darcy's Law)



$$Q = surface * q = surface * k\frac{\partial\phi}{\partial x}$$

$$Q_{i,j-1/2,k} = k_{i,j-1/2,k}\,\Delta y\,\Delta z\,\frac{\phi_{i,j-1,k} - \phi_{i,j,k}}{\Delta x}$$

$$Q_{i,j-1/2,k} = CR_{i,j-1/2,k}\left(\phi_{i,j-1,k} - \phi_{i,j,k}\right)$$

where $CR_{i,j-1/2,k} = \frac{k_{i,j-1/2,k}\,\Delta y\,\Delta z}{\Delta x}$ is the conductance [L^2/T]

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Density dependent vertical flow equation

$$q_z = -\frac{\kappa_z \rho_f g}{\mu}\left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

$$q_z = -k_z\left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

$$Q_z = surface * q_z$$

$$= surface * k_z\left(\frac{\partial \phi_f}{\partial z} + \frac{\rho - \rho_f}{\rho_f}\right)$$

$$Q_{i,j,k-1/2} = k_{i,j,k-1/2}\,\Delta x\,\Delta y\left(\frac{\phi_{f,i,j,k-1} - \phi_{f,i,j,k}}{\Delta z} + BUOY_{i,j,k-1/2}\right)$$

$$Q_{i,j,k-1/2} = CV_{i,j,k-1/2}\left(\phi_{f,i,j,k-1} - \phi_{f,i,j,k} + BUOY_{i,j,k-1/2}\Delta z\right)$$

where $BUOY_{i,j,k-1/2} = \left(\frac{(\rho_{i,j,k-1/2} + \rho_{i,j,k})/2 - \rho_f}{\rho_f}\right)$ =buoyancy term [-]

where $CV_{i,j,k-1/2} = \frac{k_{i,j,k-1/2}\,\Delta x\,\Delta y}{\Delta z}$ =conductance [L^2/T]

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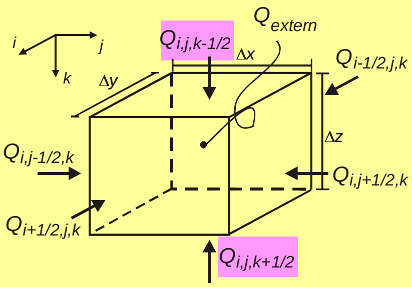
Density dependent groundwater flow equation

$$Q_{i,j-1/2,k} = CR_{i,j-1/2,k}\left(\phi_{f,i,j-1,k} - \phi_{f,i,j,k}\right)$$
$$Q_{i,j+1/2,k} = CR_{i,j+1/2,k}\left(\phi_{f,i,j+1,k} - \phi_{f,i,j,k}\right)$$
$$Q_{i-1/2,j,k} = CC_{i-1/2,j,k}\left(\phi_{f,i-1,j,k} - \phi_{f,i,j,k}\right)$$
$$Q_{i+1/2,j,k} = CC_{i+1/2,j,k}\left(\phi_{f,i+1,j,k} - \phi_{f,i,j,k}\right)$$



$$Q_{i,j,k-1/2} = CV_{i,j,k-1/2}\left(\phi_{f,i,j,k-1} - \phi_{f,i,j,k} + BUOY_{i,j,k-1/2}\Delta v_{k-1/2}\right)$$
$$Q_{i,j,k+1/2} = CV_{i,j,k+1/2}\left(\phi_{f,i,j,k+1} - \phi_{f,i,j,k} - BUOY_{i,j,k+1/2}\Delta v_{k+1/2}\right)$$

$$Q_{i,j-1/2,k} + Q_{i,j+1/2,k} + Q_{i-1/2,j,k} + Q_{i+1/2,j,k} + Q_{i,j,k-1/2} + Q_{i,j,k+1/2} + Q_{ext,i,j,k}$$
$$= SS_{i,j,k}\frac{\phi^{t}_{f,i,j,k} - \phi^{t+\Delta t}_{f,i,j,k}}{\Delta t}\Delta V$$

The term $Q_{ext,i,j,k}$

Takes into account all external sources

Rewriting the term:

$$Q_{ext,i,j,k} = P_{i,j,k}\phi^{t+\Delta t}_{i,j,k} + Q'_{i,j,k}$$

Thé variable density groundwater flow equation

$$Q_{i,j-1/2,k} + Q_{i,j+1/2,k} + Q_{i-1/2,j,k} + Q_{i+1/2,j,k} + Q_{i,j,k-1/2} + Q_{i,j,k+1/2} + Q_{ext,i,j,k}$$

$$= SS_{i,j,k} \frac{\phi^{t}_{f,i,j,k} - \phi^{t+\Delta t}_{f,i,j,k}}{\Delta t} \Delta V$$

and:

$$Q_{ext,i,j,k} = P_{i,j,k}\phi^{t+\Delta t}_{f,i,j,k} + Q'_{i,j,k}$$

gives:

$$\begin{aligned} & CV_{i,j,k-1/2}\phi^{t+\Delta t}_{f,i,j,k-1} + CC_{i-1/2,j,k}\phi^{t+\Delta t}_{f,i-1,j,k} + CR_{i,j-1/2,k}\phi^{t+\Delta t}_{f,i,j-1,k} \\ & + \left(-CV_{i,j,k-1/2} - CC_{i-1/2,j,k} - CR_{i,j-1/2,k} - CR_{i,j+1/2,k} - CC_{i+1/2,j,k} - CV_{i,j,k+1/2} + HCOF_{i,j,k}\right)\phi^{t+\Delta t}_{f,i,j,k} \\ & + CR_{i,j+1/2,k}\phi^{t+\Delta t}_{f,i,j+1,k} + CC_{i+1/2,j,k}\phi^{t+\Delta t}_{f,i+1,j,k} + CV_{i,j,k+1/2}\phi^{t+\Delta t}_{f,i,j,k+1} = RHS_{i,j,k} \end{aligned}$$

with:

$$HCOF_{i,j,k} = P_{i,j,k} - SC1_{i,j,k} / (\Delta t)$$

$$RHS_{i,j,k} = -Q'_{i,j,k} - SC1_{i,j,k}\phi^{t}_{f,i,j,k} / (\Delta t)$$

$$-CV_{i,j,k-1/2}BUOY_{i,j,k-1/2}\Delta v_{k-1/2} + CV_{i,j,k+1/2}BUOY_{i,j,k+1/2}\Delta v_{k+1/2}$$

$$SC1_{i,j,k} = SS_{i,j,k}\Delta V$$

MOCDENS3D

Equation of state

$$BUOY_{i,j,k-1/2} = \left(\frac{(\rho_{i,j,k-1/2} + \rho_{i,j,k})/2 - \rho_f}{\rho_f} \right)$$

$$\rho_{i,j,k} = \rho_f \left(1 + \frac{\rho_s - \rho_f}{\rho_f} \frac{C_{i,j,k}}{C_s} \right)$$

or

$$\rho_{i,j,k} = \rho_f \left(1 + \beta C_{i,j,k} \right)$$

MODFLOW

Method of Characteristics (MOC)

Solve the advection-dispersion equation (ADE)
with the Method of Characteristics

$$\frac{\partial C}{\partial t} = \frac{\partial}{\partial x_i}\left(D_{ij} \frac{\partial C}{\partial x_j} \right) - \frac{\partial}{\partial x_i}(CV_i) + \frac{(C - C)'W}{n_e}$$

Lagrangian approach:

Splitting up the advection part and the dispersion/source part:

- advection by means of a particle tracking technique
- dispersion/source by means of the finite difference method

Advantage of the MOC approach by splitting up the advection-dispersion equation

It is difficult to solve the whole advection-dispersion equation in one step, because the so-called Peclet-number is high in most groundwater flow/solute transport problems.

The Peclet number stands for the ratio between advection and dispersion

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Procedure of MOC: advective transport by particle tracking

- Place a number of particles in each element
- Determine the effective velocity of each particle by (bi)linear interpolation of the velocity field which is derived from MODFLOW
- Move particles during one solute time step Δt_{solute}
- Average values of all particles in an element to one node value
- Calculate the change in concentration in all nodes due to advective transport
- Add this result to dispersive/source changes of solute transport

Steps in MOC-procedure

1. Determine concentration gradients at old timestep k-1
2. Move particles to model advective transport
3. Concentration of particles to concentration in element node
4. Determine concentration gradients on new timestep k*
5. Determine concentration in element node after advective, dispersive/source transport on timestep k

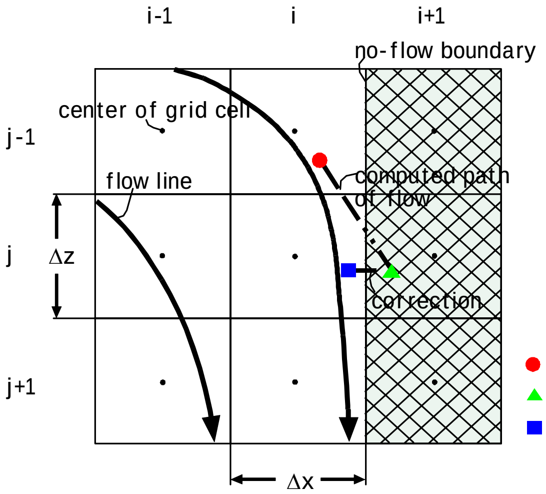
Konikow and Bredehoeft, 1978

Causes of errors in MOC-procedure

1. Concentration gradients
2. Average from particles to node element, and visa versa
3. Concentration of sources/sinks to entire element
4. Empty elements
5. No-flow boundary: reflection in boundary

MOC3D

Reflection in boundary



● particle on previous location

▲ computed location of particle

■ corrected location of particle

MOC3D

Stability criteria (III)

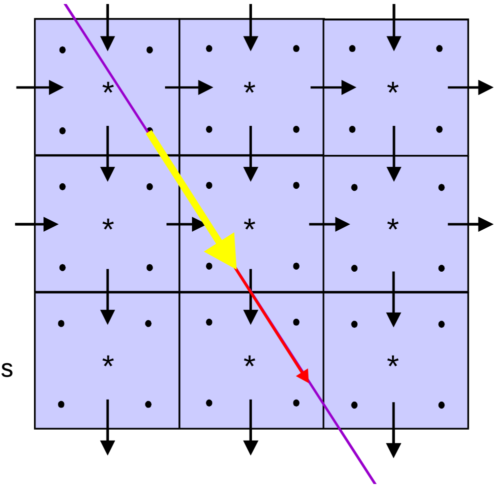
3. Courant criterium

* Node element

• Particle


Velocity direction

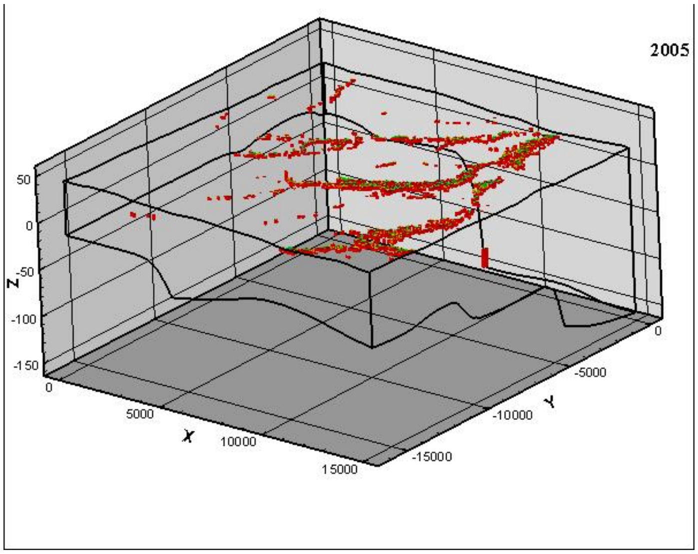

Movement particles



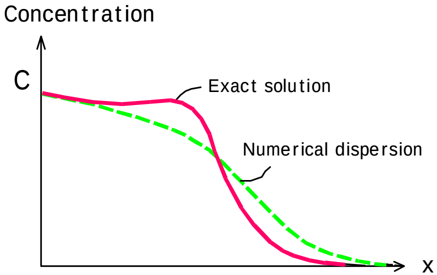
$0<\xi<=\sim 1$

$$\Delta t_s \le \frac{\xi \Delta x}{V_{x,\max}} \qquad \Delta t_s \le \frac{\xi \Delta y}{V_{y,\max}} \qquad \Delta t_s \le \frac{\xi \Delta z}{V_{z,\max}}$$

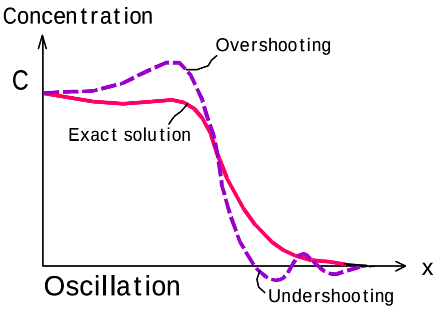
Courant criterion: places where timestep is smaller than 40 days



Numerical dispersion and oscillation



Numerical dispersion



Oscillation

$$\frac{\partial C}{\partial t} = D\frac{\partial^2 C}{\partial z^2} \qquad C_i^{t+\Delta t} = C_i^t + \frac{D\Delta t}{\Delta z^2}\left(C_{i+1}^t - 2C_i^t + C_{i-1}^t\right) \qquad \frac{D\Delta t}{\Delta z^2} < 0.5$$

Numerical dispersion problem (I)

To solve the advection-dispersion equation, standard finite difference and element techniques should consider the following spatial discretisation criterion:

Peclet number $Pe \leq 2 \text{ to } 4$

where: $Pe = \left| \frac{V \Delta x}{D_h} \right|$

V = effective velocity [L/T]
Δx = dimension grid cell [L]
D_h = hydrodynamic dispersion [L^2/T]

Numerical dispersion problem (II)

For advection dominant grondwater flow, the Peclet number can be rewritten as:

$$\Delta x \leq 2\alpha_L \text{ to } 4\alpha_L$$

where α_L = longitudinal dispersivity [L]

What does that mean?

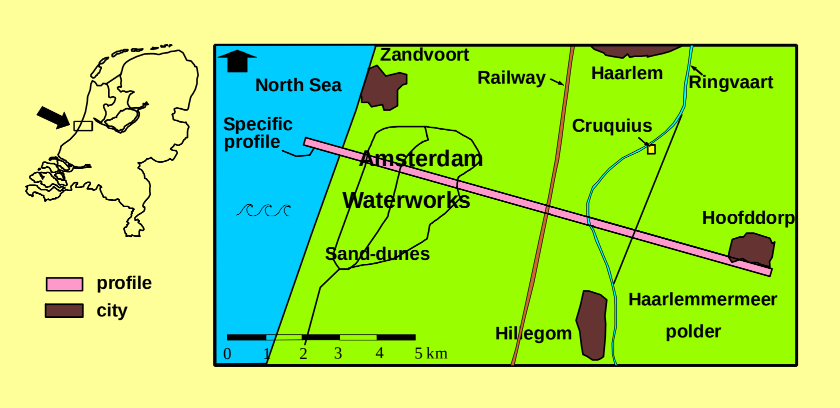
If α_L is small, then Δx should be small too!!

Numerical dispersion problem (III)

Now follows an transient salt water intrusion case to demonstrate why in many coastal aquifers the longitudinal dispersivity α_L [L] should be small

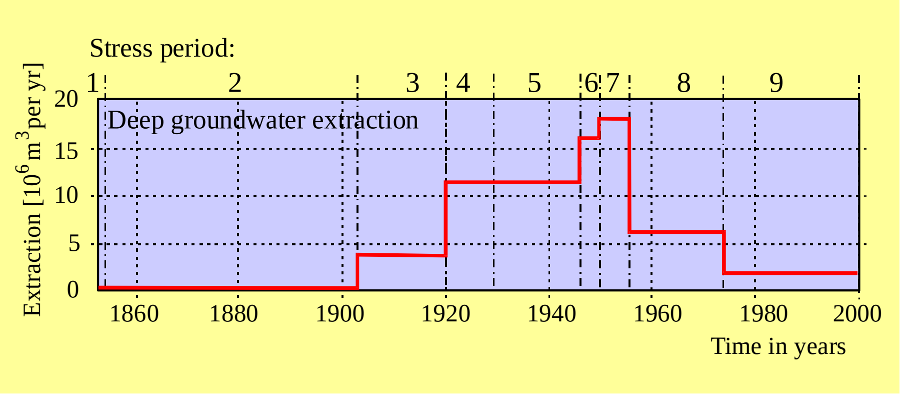
Effect of α_L on the salinisation of the aquifer (I)

Position profile through Amsterdam Waterworks, Rijnland polders and Haarlemmermeer polder



Effect of α_L on the salinisation of the aquifer (II)

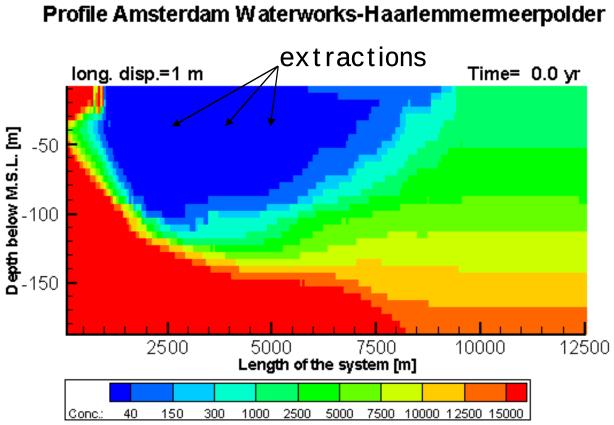
Grondwater extractions out of the middle aquifer in the sand-dune area of Amsterdam Waterworks



Effect of α_L on the salinisation of the aquifer (III)

α_L=1 m

Initial situation: 154 years ago

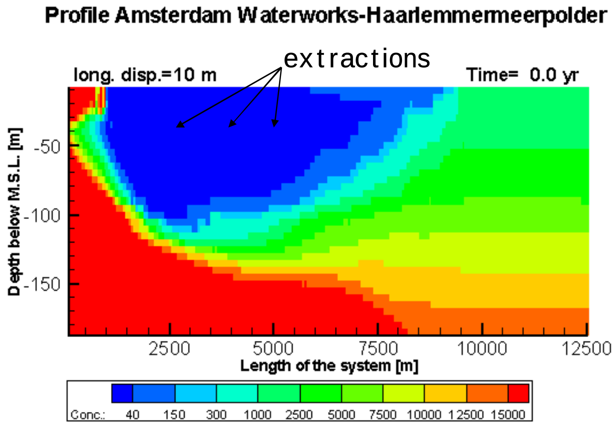


problems

Effect of α_L on the salinisation of the aquifer (IV)

α_L=10 m

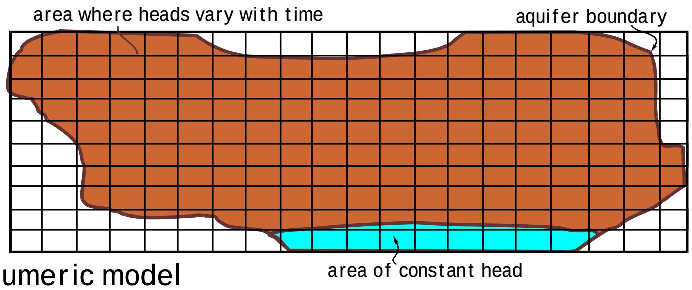
Initial situation: 154 years ago



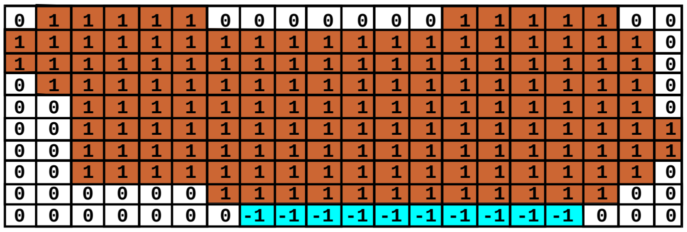
MODFLOW

Boundary conditions in MODFLOW (I)

Example of a system with three types of boundary conditions



Numeric model



0	1	1	1	1	1	0	0	0	0	0	0	0	1	1	1	1	1	0	0
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0
1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0
0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0
0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0
0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
0	0	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	0
0	0	0	0	0	0	1	1	1	1	1	1	1	1	1	1	1	1	0	0
0	0	0	0	0	0	0	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	0	0	0

Boundary conditions in MODFLOW (II)

For a constant head condition: IBOUND<0
For a no flow condition: IBOUND=0
For a variable head: IBOUND>0

Packages in MODFLOW

1. Well package
2. River package
3. Recharge package
4. Drain package
5. Evaporation package
6. General head package

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1. Well package

$$Q_{well} = Q_{i,j,k}$$

Example: an extraction of 10 m^3 per day should be inserted in an element as:

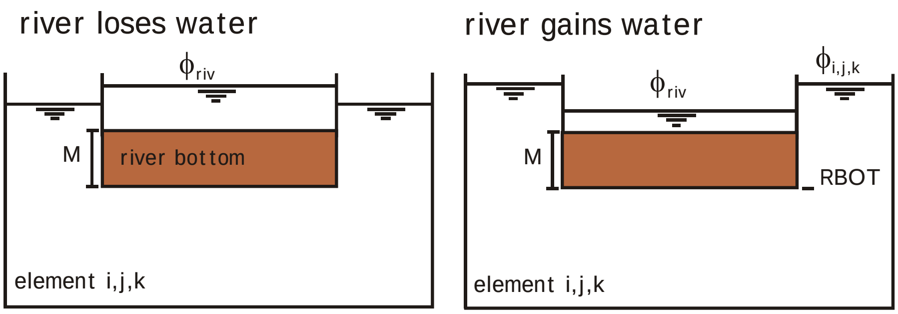
$$Q_{ext,i,j,k} = P_{i,j,k}\phi^{t+\Delta t}_{i,j,k} + Q'_{i,j,k}$$

$$Q_{ext,i,j,k} = -10$$ (in = positive)

$$Q'_{i,j,k} = -10$$

MODFLOW

2. River package (I)



$$Q_{riv} = KLW\left(\frac{\phi_{riv} - \phi_{i,j,k}}{M}\right)$$

$$Q_{riv} = \frac{KLW}{M}\left(\phi_{riv} - \phi_{i,j,k}\right) \Leftrightarrow Q_{riv} = C_{riv}\left(\phi_{riv} - \phi_{i,j,k}\right)$$

MODFLOW

2. River package (II)

$$Q_{riv} = C_{riv}\left(\phi_{riv} - \phi_{i,j,k}\right)$$

Example: the river conductance C_{riv} is 20 m^2/day and the rivel level=3 m, than this package should be inserted in an element as:

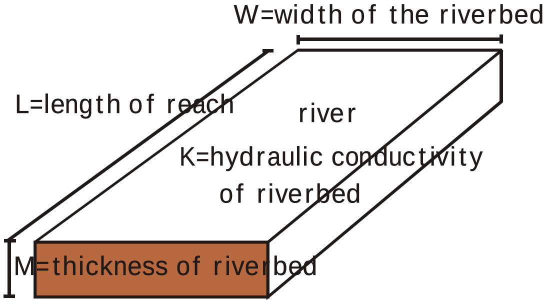
$$Q_{ext,i,j,k} = P_{i,j,k}\phi_{i,j,k}^{t+\Delta t} + Q'_{i,j,k}$$

$$Q_{ext,i,j,k} = 20\left(3 - \phi_{i,j,k}\right)$$

$$Q'_{i,j,k} = 60 \quad \text{and} \quad P_{i,j,k} = -20$$

2. River package (III)

Determine the conductance of the river in one element:



where $C_{riv} = \dfrac{KLW}{M}$ is the

conductance [L^2/T] of the river

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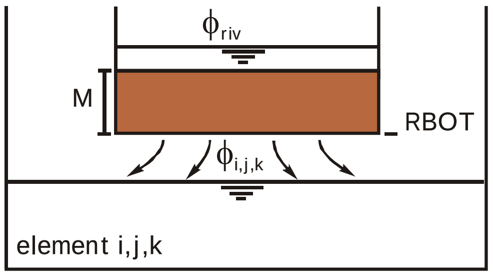
2. River package (IV)

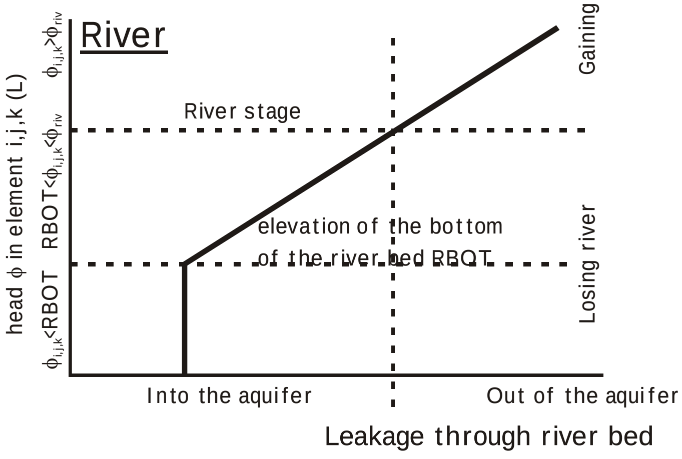
Leakage to the groundwater system



Special case:

if $\phi_{i,j,k}$<RBOT, then $Q_{riv} = C_{riv}\left(\phi_{riv} - RBOT\right)$

2. River package (V)



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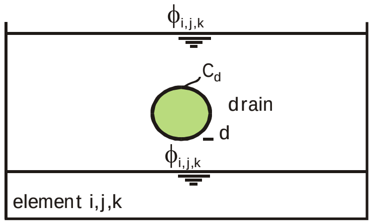
3. Recharge package

$$Q_{rec} = I\Delta x\Delta y$$

MODFLOW

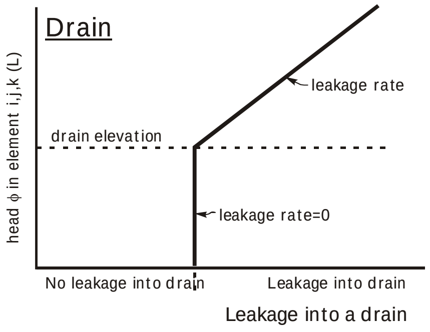
4. Drain package

$$Q_{drn} = C_{drn}\left(\phi_{i,j,k} - d\right)$$



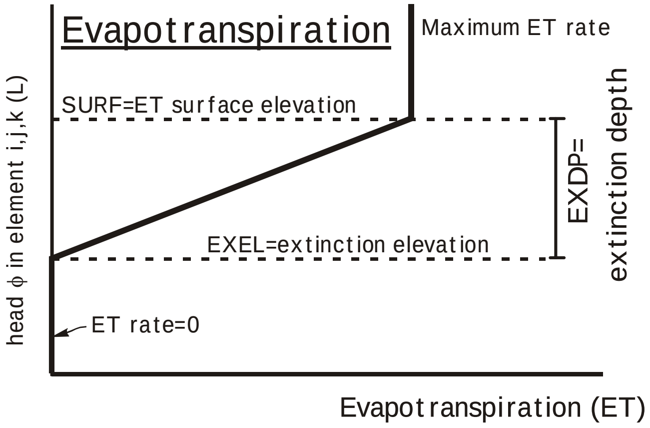
Special case: →

if $\phi_{i,j,k} < d$ than $Q_{drn} = 0$



MODFLOW

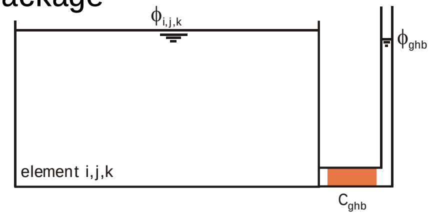
5. Evapotranspiration package

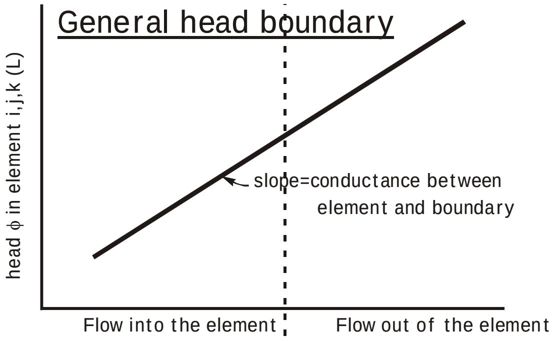


MODFLOW

6. General head boundary package

$$Q_{ghb} = C_{ghb}\left(\phi_{ghb} - \phi_{i,j,k}\right)$$





Flow to a general head boundary

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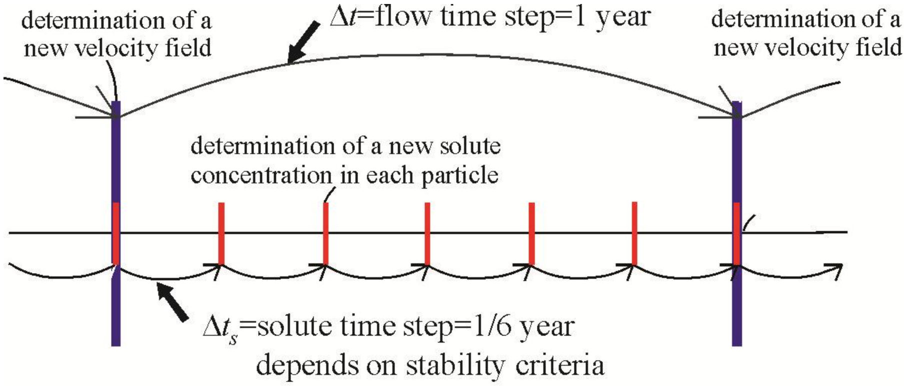
1 (name).bas-file
2 (name).bcf-file
3 (name).moc-file
4 (name).wel-file
5 (name).riv-file
6 (name).drn-file
7 (name).ghb-file
8 (name).sip-file
9 densin.dat-file
10 (name).nam-files

MODFLOW

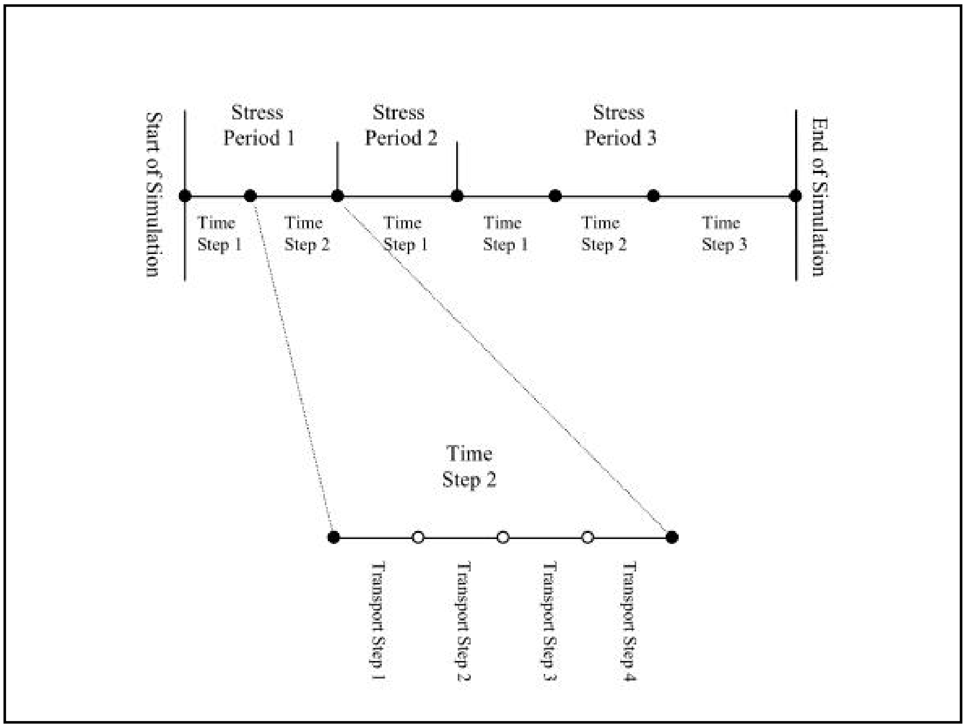
Time indication MODFLOW

ITMUNI=1: seconde
ITMUNI=2: minute
ITMUNI=3: hour
ITMUNI=4: day
ITMUNI=5: year

Flow time step and solute time step



* velocity field remains constant during 1 year
* solute concentration changes during each solute time step


Start of Simulation
Stress Period 1
Stress Period 2
Stress Period 3
End of Simulation
Time Step 1
Time Step 2
Time Step 1
Time Step 1
Time Step 2
Time Step 3
Time Step 2
Transport Step 1
Transport Step 2
Transport Step 3
Transport Step 4