

# Investigating the internal pressure gradient error in $\sigma$ -coordinate ocean models

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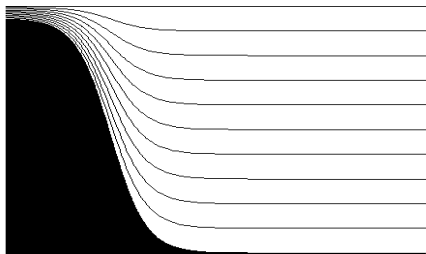
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- Vertical coordinates follow the terrain

$$x^* = x \quad y^* = y \quad \sigma = \frac{z - \eta}{H + \eta} \quad t^* = t$$



- Advantageous when dealing with large variations in topography
- Bottom and top boundary layers represented accurately
- E.g. Princeton Ocean Model (POM), Regional Ocean Model System (ROMS), Bergen Ocean Model (BOM)



The transformation to  $\sigma$ -coordinates introduces an error in the *internal* pressure force



# The internal pressure gradient error

- The horizontal internal pressure gradient in the  $x$ -direction becomes

$$\frac{\partial p_{int}}{\partial x} = gD \int_{\sigma}^0 \left( \frac{\partial \rho}{\partial x^*} - \frac{\sigma}{D} \frac{\partial \rho}{\partial \sigma} \frac{\partial D}{\partial x^*} \right) d\sigma$$

- Near steep topography, the two terms of the integrand can be large, comparable in magnitude, and opposite of sign
- Very sensitive to truncation errors



- Haney [1991] introduced the concept of *hydrostatic consistency* for ocean models
- For a hydrostatically consistent scheme

$$\left| \frac{\sigma}{\delta\sigma} \frac{\delta D}{D} \right| < 1 \quad (1)$$

- When  $\delta\sigma$  approaches zero, (1) will be violated closer to the bottom boundary



# The story: Mellor et al. [1994]

- Condition of hydrostatic consistency is quite restrictive [Mellor et al. 1994]
- The discretisation error is given by

$$E \left( \frac{\delta_x b}{\delta x} \right) = \frac{D \delta_x D}{4 \delta x} \left( \frac{\partial^2 b}{\partial z^2} \right) \left[ (\delta \sigma)^2 - \sigma^2 \left( \frac{\delta_x D}{D} \right)^2 \right]$$

- The error decreases if  $\delta \sigma$  and  $\frac{\delta_x D}{D}$  goes to zero
- Hydrostatic consistency is accordingly not a meaningful concept [Berntsen and Oey, 2010]



# The story: Consolation

Mellor et al. [1994] concluded: The error is not numerically divergent, and therefore *not of great concern*





# The story: SEFK and SESK

Beckmann and Haidvogel [1993]

- Treated the seamount case
- Experienced growing errors

Mellor et al. [1998] – Two kinds of errors

- Sigma Errors of the First Kind (SEFK): 2D errors, will die out
- Sigma Errors of the Second Kind (SESK): Vorticity 3D errors, will not die out



# Possible remedies

- Subtract a background stratification,  $\rho(z)$   
[Gary, 1973]
- Add viscosity  
[Mellor, 1998]
- Smooth the topography  
[Barnier et al., 1998]



# Possible remedies, cont.

- Interpolate back to z-levels  
[Stelling and van Kester, 1994]
- Higher order schemes  
[McCalpin, 1994], [Chu and Fan, 1997]
- Green's theorem approach  
[Shchepetkin and McWilliams, 2003]
- Rotate grid 45 degrees and weight  
[Thiem and Berntsen, 2006]



It is still desirable to find a solution to this problem



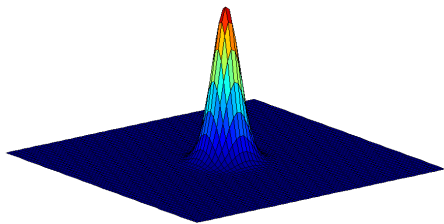
The following will be investigated:

- Finite volume approach for pressure computation
- Higher order schemes
- Expanded computational stencils
- Weighting of different methods



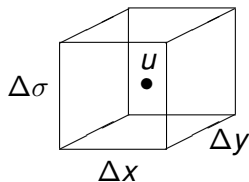
# The model and the test case

- Linearised version of the Princeton Ocean Model
- The seamount test case
- No forcing, horizontal isopycnals – true solution is zero velocities



# The finite volume approach

- Estimating pressure forces over fixed volumes

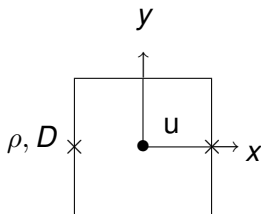


- Discretising the following integral

$$\frac{\partial p}{\partial x} = g \int_{-\frac{1}{2}}^{\frac{1}{2}} \int_{-\frac{1}{2}}^{\frac{1}{2}} \left[ \int_{\sigma}^0 \left( D \frac{\partial \rho}{\partial x} + \frac{\partial D}{\partial x} \rho \right) d\sigma + \sigma \rho \frac{\partial D}{\partial x} \right] dx dy$$



- The standard 2nd order POM method can be interpreted as the simplest in a family of finite volume methods

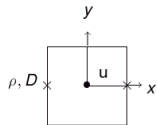


**Figure:** Points  $\rho$ ,  $D$  ( $\times$ ) and  $u$  ( $\bullet$ ) at a  $\sigma$ -level used in the standard 2nd order POM method, Method A.

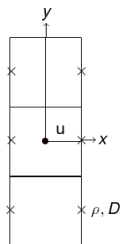




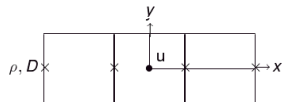
# The new methods



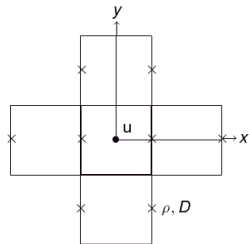
Method A



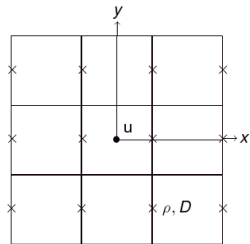
Method B



Method C



Method D



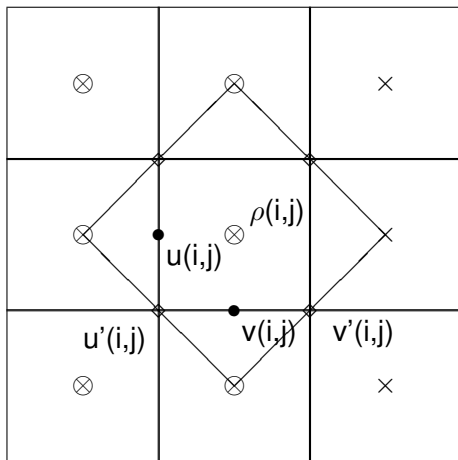
Method E

# The rotated grid

- Consistent Methods A, C, and D were successfully created
- For the stencils of the Methods B and E, a new approach is needed: Rotated grid [Thiem and Berntsen, 2006]



# The rotated grid



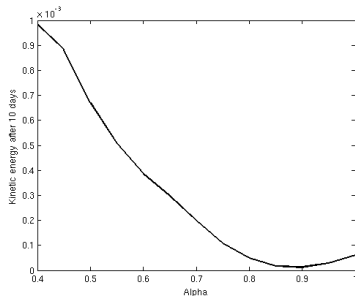
# The rotated grid: A connection

- Using the stencil of Method B –, it can be shown that the rotated approach is a 2nd order finite volume method
- The rotated approach can be weighted with the 2nd order POM method, with a *fixed* weight, to reduce the errors



# The rotated grid: A fixed weight

- The optimal fixed weight can be found by experiment
- The same can be done for the stencil of Method E



**Figure:** The kinetic energy after 10 days as a function of  $\alpha$  for the Method  $B_\alpha$  experiments.



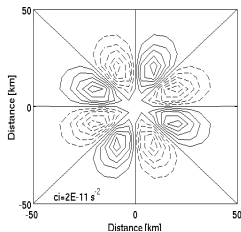
- The two resulting methods, defined by an optimal fixed weight, are called Method  $B_\alpha$  and Method  $E_\alpha$
- End up with *five* consistent methods



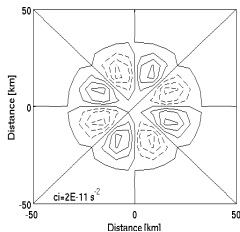
- SESK (Sigma Errors of the Second Kind) are related to vorticity [Mellor et al. 1998]
- Initial SESK closely connected with the later errors
- The vertically integrated initial acceleration of the vorticity is studied



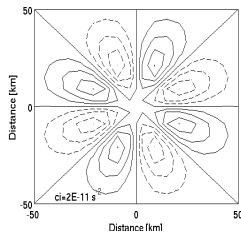
# The initial vorticity error, different methods



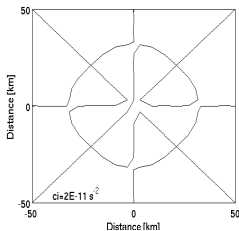
(a) Method A



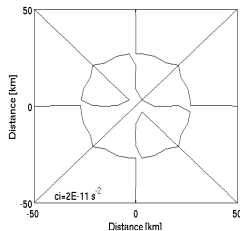
(b) Method B $_{\alpha}$



(c) Method C



(d) Method D

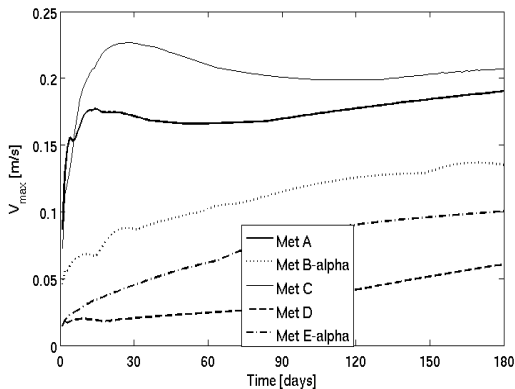


(e) Method E $_{\alpha}$



# The performance of the methods

The maximum velocity, 180 days run



# The optimal weighting

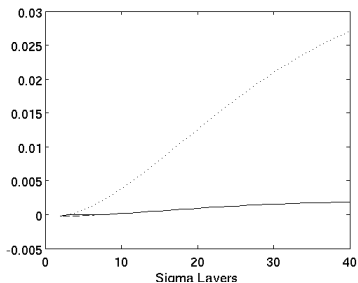
- Possible to find a field of optimal weights?
- Two estimates of the internal pressure gradient, interpolated to give the exact result in each point
- Weights  $\alpha_x(x, y, \sigma)$  and  $\alpha_y(x, y, \sigma)$  fixed in time
- For our case, the result should be zero

$$\alpha_x(x, y, \sigma) \cdot \left( \frac{\partial \rho}{\partial x} \right)_1 + [1 - \alpha_x(x, y, \sigma)] \cdot \left( \frac{\partial \rho}{\partial x} \right)_2 = 0$$

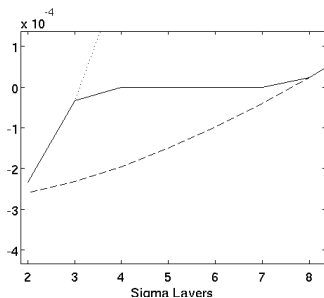


# Results: The optimal weighting

- For interpolation, we need estimates of opposite signs
- The optimal weighting not complete
- Leads to discontinuities, and instability



(a)



(b)



# The way forward

- New pair of methods
- Optimal weighting also time-dependent?
- Weighting in the vertical



# Concluding remarks

- The  $\sigma$ -coordinate system is still being used
- Many advantages to the terrain-following approach
- The severity of the internal pressure gradient problem diminishes with higher resolution



Thank you for your attention!

