

On the use of a depth-dependent barotropic mode for free surface ocean models

Jonsmod 2012

J. Demange, L. Debreu

INRIA and Laboratoire Jean Kuntzmann, Grenoble, France

P. Marchesiello

IRD and LEGOS, Toulouse, France

E. Blayo

University of Grenoble and Laboratoire Jean Kuntzmann, Grenoble, France

May 23, 2012

Inria



- 1 Little review of free-surface ocean model development
- 2 Normal Modes and Internal waves
- 3 The splitting method : Rigid-lid / free-surface
- 4 Test case and compare
- 5 Conclusion, perspectives

Table of Contents

- 1 Little review of free-surface ocean model development
 - A selected background of numerical schemes for free-surface ocean models
- 2 Normal Modes and Internal waves
 - Linearized system
 - Definition normal modes
 - Magnitudes and splitting motivations
- 3 The splitting method : Rigid-lid / free-surface
 - Principle
 - Depth (in)dependent splitting
 - Stability analysis
 - Implementation of a depth dependent splitting
- 4 Test case and compare
 - Test Case
 - Results
- 5 Conclusion, perspectives

Bryan 69 : First splitting & Rigid-lid approximation

Bryan 69 : Rigid-lid approximation & splitting:

- First numerical 3D ocean model.
- Primitive equations, hydrostatic, Boussinesq.
- Rigid-lid approximation = no fast waves.
- Already one splitting method enforced by the elliptic surface pressure problem.
- Mathematically true since there is no free-surface : orthogonality.
- Pb-development : very ill conditioned, assimilation, middle scale, internal waves representation, parallelization

Let the vertical average over the whole water column be indicated by an overbar,

$$\bar{(\cdot)} = \frac{1}{H} \int_{-H}^0 (\cdot) dz \quad (2.29)$$

and the deviation from a vertical average by $(\hat{\cdot})$. Thus the velocity components may be expressed as

$$(u, v) = (\bar{u}, \bar{v}) + (\hat{u}, \hat{v}). \quad (2.30)$$

The \bar{u} , \bar{v} components may be predicted from (2.23) and (2.28). To predict \hat{u} , \hat{v} we make use of (2.3) and (2.4) with the right-hand side of (2.24) substituted for the pressure term. The surface pressure, p_s , is temporarily set to zero:

$$u'_z + \mathcal{L}u - 2\Omega nv - mnv/a = \frac{-mg}{\rho_0 a} \left(\int_z^0 \rho dz \right)_s + F^s \quad (2.31)$$

$$v'_z + \mathcal{L}v + 2\Omega nu + mnv/a = \frac{-g}{\rho_0 a} \left(\int_z^0 \rho dz \right)_s + F^s. \quad (2.32)$$

u' and v' differ from u and v due to the neglect of that part of the pressure gradient force which depends on the surface pressure. To determine \hat{u} and \hat{v} we set

$$(\hat{u}, \hat{v}) = (u' - \bar{u}', v' - \bar{v}'). \quad (2.33)$$

In the determination of \hat{u} and \hat{v} the error due to the neglect of surface pressure in u' and v' is of no consequence, since that error is independent of z and is therefore eliminated by subtracting out \bar{u}' and \bar{v}' .

Free surface model and splitting

1 Bryan 69 : Rigid-lid approximation & splitting

2 R.Madala 77, P.D.Killworth et al. 91: Free surface model and splitting

- Free surface equation : $\partial_t \eta + \nabla UH = 0$
- Pb n°1 : No more Poisson like solver but one more equation (U needed).
- Pb n°2 : Introduction of surface gravity waves (very fast).
- Solution : In linear study the vertical average of velocity seems to be orthogonal to the rest of the flow (barotropic aka external mode) \implies Compute apart the barotropic (external) system (splitting method).
- Pb n°3: Mathematically **not** true, since there is a free-surface : false orthogonality.
- Pb n°4: Not possible to exprime the exact barotropic (averaged) part of the non linear term : $u \nabla u$ and friction terms ??
- Pb-development : stability, physics of internal waves, filter, explicit (subcycling) or implicit ?

Numerical stability study and filter

- 1 Bryan 69 : Rigid-lid approximation & splitting
- 2 R.Madala 77, P.D.Killworth et al. 91: Free surface model and splitting
- 3 R.Higdon et al. 96, V.M. Kamenkovich et al. 08, and Shchepetkin et al. 05 :
Numerical stability study and filter
 - Numerical stability analysis on simplified cases of the barotropic splitting using the rigid-lid approximation (external mode). \implies Need of a filter in the non-linear case. (R.Higdon et al. 96, V.M. Kamenkovich et al. 98)
 - Conservation of constant trough the splitting method scheme \implies modification of the tracer advection velocity. (Shchepetkin 03)
 - Pb : Large damping

Splitting : Barotropic mode vs External mode, improvement ?

- 1 Bryan 69 : First splitting & Rigid-lid approximation
- 2 R.Madala 77, P.D.Killworth et al. 91: Free surface model and splitting
- 3 R.Higdon et al. 96, V.M. Kamenkovich et al. 98, and Shchepetkin et al. 05 : Numerical stability study and filter
- 4 And now :

Keeping the orthogonality in the linear case \implies reduce the need and effects of the filter in the non-linear case ??

A few notions you have to keep in mind

Rigid-Lid / Free-Surface

Internal gravity waves

Orthogonality

Linear theory

Table of Contents

- 1 Little review of free-surface ocean model development
 - A selected background of numerical schemes for free-surface ocean models
- 2 Normal Modes and Internal waves
 - Linearized system
 - Definition normal modes
 - Magnitudes and splitting motivations
- 3 The splitting method : Rigid-lid / free-surface
 - Principle
 - Depth (in)dependent splitting
 - Stability analysis
 - Implementation of a depth dependent splitting
- 4 Test case and compare
 - Test Case
 - Results
- 5 Conclusion, perspectives

Linearized system

Linearized primitive equations :

$$\left\{ \begin{array}{l} \partial_t u + \frac{1}{\rho_0} \partial_x p = 0 \\ \partial_x u + \partial_z w = 0 \\ \rho = -\frac{1}{g} \partial_z p \\ \partial_t \rho + w \partial_z \bar{\rho} = 0 \end{array} \right. \Rightarrow \left\{ \begin{array}{l} \partial_t u + \frac{1}{\rho_0} \partial_x p = 0 \\ \partial_x u - \Lambda \left(\frac{1}{\rho_0} \partial_t p \right) = 0 \\ \rho = -\frac{1}{g} \partial_z p \\ w = -N^{-2} \partial_{zt} p \end{array} \right.$$

Boundary conditions

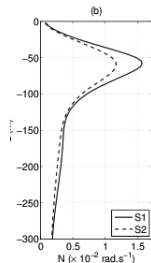
$$\left\{ \begin{array}{l} w(x, -H, t) = 0 \\ w(x, 0, t) = \partial_t \eta \end{array} \right. \quad \textit{Flat bottom}$$

Notations:

■ $\Lambda = \partial_z(N^{-2}\partial_z)$

■ The Brunt-Vaisala frequency :

$$N^{-2} = -\frac{\rho_0}{g} (\partial_z \bar{\rho})^{-1}$$



Definition of normal modes

Variables projection:

- 2D projected variables :

$$\forall n : \begin{cases} u_n(x, t) = \langle u, M_n \rangle \\ p_n(x, t) = \langle p, M_n \rangle \end{cases}$$

$$\begin{cases} u = \sum_{n=1}^{\infty} u_n M_n \\ p = \sum_{n=1}^{\infty} p_n M_n \\ \rho = -g \sum_{n=1}^{\infty} p_n \partial_z M_n \end{cases}$$

Definition of vertical modes M_n :

- Scalar product : $\langle f, g \rangle = \frac{1}{H} \int_{-H}^0 f(z)g(z)dz$

- $\begin{cases} \Delta M_n = -c_n^{-2} M_n \\ \langle M_n, M_m \rangle = \delta_{mn} \end{cases}$

- Boundary conditions :

$$\begin{cases} \frac{dM_n}{dz}(-H) = 0 \\ M_n(0) = -gN^{-2} \frac{dM_n}{dz}(0) \end{cases}$$

Equations projection: decoupled hyperbolic system

We get an hyperbolic system on each independent characteristic variable :

$$\forall n : \begin{cases} \partial_t y^+ + c_n \partial_x y^+ = 0 \\ \partial_t y^- - c_n \partial_x y^- = 0 \end{cases} \quad \text{with : } y_{\pm} = \frac{1}{2} \left(u_n \pm \frac{1}{c_n \rho_0} p_n \right)$$

The primitive system can be entirely decomposed in a sum of **independent** internal waves (y_n^{\pm}), evolving with their **own constant speed** ($\pm c_n$)

Magnitudes and splitting motivations

Under the approximation of a **constant stratification** : $\partial_z N = 0$

Depth dependent mode definition

- Top boundary condition on modes : $M_n(0) = -gN^{-2} \frac{dM_n}{dz}(0)$
- **Barotropic mode** : $\partial_z M_0 \neq 0, c_0 \simeq \sqrt{gH}$
- Baroclinic modes : $\forall k \geq 1, c_k \simeq \frac{NH}{k\pi}$

Rigid-lid approximation : $\partial_t \eta = 0$

- Top boundary condition on modes : $\frac{dM_n}{dz}(0) = 0$
- **External mode** : $\partial_z M_0 = 0, c_0 = \infty$
- Baroclinic modes : $\forall k \geq 1, c_k = \frac{NH}{k\pi}$

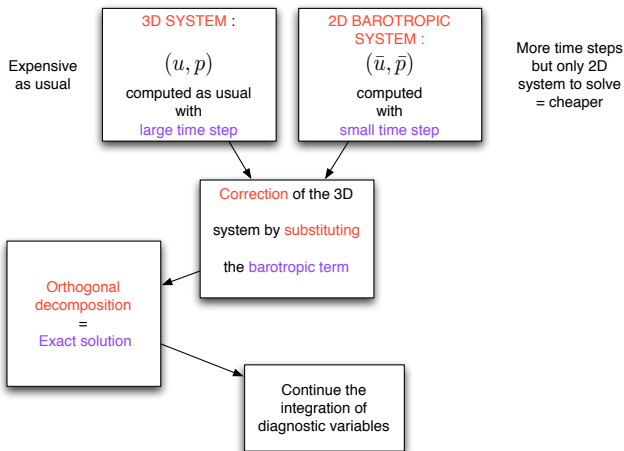
Problem : $CFL_0 = \frac{c_0 \Delta T}{dx} \gg 1 \implies$ **Very strong constraint**

A solution : Computing apart the 2D barotropic mode containing fastest terms

Table of Contents

- 1 Little review of free-surface ocean model development
 - A selected background of numerical schemes for free-surface ocean models
- 2 Normal Modes and Internal waves
 - Linearized system
 - Definition normal modes
 - Magnitudes and splitting motivations
- 3 The splitting method : Rigid-lid / free-surface
 - Principle
 - Depth (in)dependent splitting
 - Stability analysis
 - Implementation of a depth dependent splitting
- 4 Test case and compare
 - Test Case
 - Results
- 5 Conclusion, perspectives

The splitting method principle



- └ The splitting method : Rigid-lid / free-surface

- └ Depth (in)dependent splitting

Depth dependent / independent splitting

Depth dependent barotropic splitting

$$\bar{u} = u_0 = \frac{1}{H} \int_{-H}^0 u M_0$$

$$\bar{p} = p_0 = \frac{1}{H} \int_{-H}^0 p M_0$$

System :

$$\begin{cases} \partial_t u_0 + \frac{1}{\rho_0} \partial_x p_0 = 0 \\ \partial_t p_0 + c_0^2 \rho_0 \partial_x u_0 = 0 \end{cases}$$

$$c_0 \simeq \sqrt{gH}$$

Correction :

$$\begin{aligned} u &= u^{3d} + [u_0 - \langle u^{3d}, M_0 \rangle] M_0(z) \\ p &= p^{3d} + [p_0 - \langle p^{3d}, M_0 \rangle] M_0(z) \end{aligned}$$

and as diagnosis : $\rho = -g \sum_n \rho_n \partial_z M_n$

External mode (depth independent) splitting

$$\bar{u} = u_a = \frac{1}{H} \int_{-H}^0 u$$

$$\bar{p} = \rho_0 g \eta$$

System :

$$\begin{cases} \partial_t u_a + g \partial_x \eta = - \int_{-H}^0 (p - \rho_0 g \eta) \\ \partial_t \eta + \partial_x H u_a = 0 \end{cases}$$

$$c_0^* = \sqrt{gH}$$

Correction :

$$\begin{aligned} u &= u^{3d} + [U - \langle u^{3d}, 1 \rangle] \\ p^{3d}(0) &= \rho_0 g \eta \end{aligned}$$

no correction of the density !

Stability analysis and correction of the external mode splitting probable instability

The depth dependent barotropic mode splitting is stable by construction.

And the external mode splitting ? Why it could be unstable ?

In the external mode splitting some components of the true barotropic flow (u_0, p_0) are still integrated with the baroclinic time step. (Killworth *et al.*, 1991)

⇒ Sources of instability

Analytical stability analysis

- Instability already proved on simplified cases (two layers) : (Higdon and Bennett, 1996 ; Kamenkovic and Nechaev, 2008)
- Detailed stability analysis still in progress.

Correction of this potential instability

- A filter on the 2D system or an additional diffusivity term is required (Shchepetkin, 2005), even in the linear case.
- Implement a depth-dependent barotropic splitting !

- The splitting method : Rigid-lid / free-surface

- Implementation of a depth dependent splitting

Implementation of a depth dependent splitting

To easily implement the splitting on a code with an **explicit density equation** and a **diagnosis pressure variable** we have to rewrite the 2d system as a **density/velocity terms** !

$$\begin{cases} \partial_t u_0 + \frac{g}{\lambda \rho_0} \partial_x \left[+ \frac{\rho_0}{gH} M_b(0) \eta - \bar{\rho} \right] = 0 \\ \partial_t \bar{\rho} + \frac{\rho_0}{g} \partial_x [M_0(0) u_a - u_0] = 0 \\ \partial_t \eta + \partial_x H u_a = 0 \end{cases}$$

With : $\bar{\rho}(x, t) = \int_{-H}^0 \rho(x, z, t) N^{-2} \partial_z M_0(z) dz$

The correction, then, is directly put on the velocity (as usual) **and density** before the diagnostic step of pressure :

$$u^{n+1,c}(z) = u^{n+1}(z) + [u_0^{n+1} - \overline{u^{n+1}}] M_0(z)$$

$$\rho^{n+1,c}(z) = \rho^{n+1}(z) + \left[\frac{\bar{\rho}^{n+1} - \overline{\rho^{n+1}}}{\lambda - \frac{M_0(0)}{gH}} \right] \partial_z M_0(z)$$

Table of Contents

- 1 Little review of free-surface ocean model development
 - A selected background of numerical schemes for free-surface ocean models
- 2 Normal Modes and Internal waves
 - Linearized system
 - Definition normal modes
 - Magnitudes and splitting motivations
- 3 The splitting method : Rigid-lid / free-surface
 - Principle
 - Depth (in)dependent splitting
 - Stability analysis
 - Implementation of a depth dependent splitting
- 4 Test case and compare
 - Test Case
 - Results
- 5 Conclusion, perspectives

Test Case

Barotropic analytic test case to compare the two methods :

- Initialization with the barotropic solution (potentially unstable):

$$\rho = -g * 0.10 \sin \frac{2\pi x}{Lx} \partial_z M_0$$

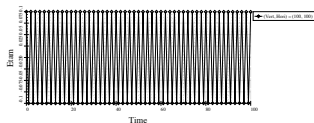
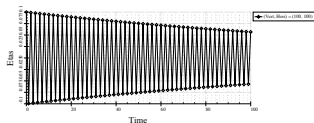
$$u = \rho_0 c_0^2 * 0.10 \sin \frac{2\pi x}{Lx} M_0(z)$$

- Analytic solution : computed with the characteristic method.
- Configuration : cyclic domain, flat bottom, $H = 4km$, $L = 15km$, $dx = 75m$, $dz = 200m$.
- Parameters : $N=10^{-3}$ s., $CFL_0 = 0.5$, $CFL_1 = 0.2$
- Code : 2D-xz
- Coordinates : Geopotential vertical coordinates on Arakawa C-grid.
- Numerical schemes : Forward-Backward + Upwind schemes + Barotropic Splitting.

Instability and filter effects

First results :

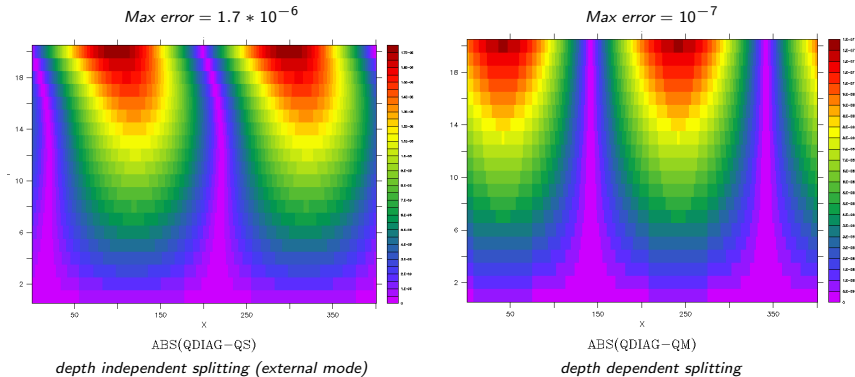
- the depth independent (*a.k.a. external mode*) splitting is unstable. We add a power-function shaped filter (*Shchepetkin, 2005*) \Rightarrow Large damping of the free-surface elevation.
- the depth dependent splitting method is stable without filter and very close to the analytic solution.



Temporal series of free-surface η , top: depth independent splitting + power filter, bottom: depth dependent splitting

Density vertical shape

Influence of the depth dependent density correction on the vertical shape of the density :



Instantaneous plot of $|\rho_{diag} - \rho|$ after 2000 time step

Table of Contents

- 1 Little review of free-surface ocean model development
 - A selected background of numerical schemes for free-surface ocean models
- 2 Normal Modes and Internal waves
 - Linearized system
 - Definition normal modes
 - Magnitudes and splitting motivations
- 3 The splitting method : Rigid-lid / free-surface
 - Principle
 - Depth (in)dependent splitting
 - Stability analysis
 - Implementation of a depth dependent splitting
- 4 Test case and compare
 - Test Case
 - Results
- 5 Conclusion, perspectives

Conclusion, perspectives

CONCLUSIONS:

- The traditional external mode splitting **doesn't allow density correction and is unstable even in a linear case**: it needs a filter correction.
- The implementation of a depth dependent splitting in a density formulation is possible and **works well in a linear case without filter**.
- The work has been extended to the non-linear conservative case with similar conclusions.

PERSPECTIVES:

- Derivation of the barotropic system with a **non-flat** topography.
- Implementation in a **realistic model** and test if this study could, at the end, **reduce the need and effects of filter**.
- Try to re-introduce sound waves in a same way ...