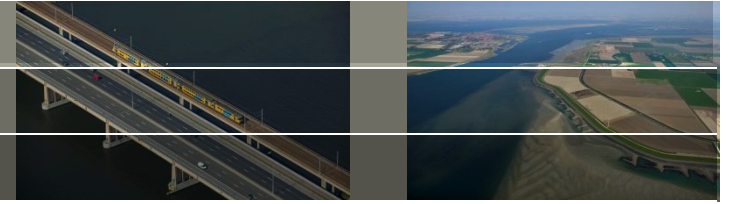




One- two- and three-dimensional hydrodynamic modelling with D-Flow Flexible Mesh

Herman Kernkamp, Sander v/d Pijl, Arthur v Dam,
Wim v Balen, Willem Ottevanger, Guus Stelling

D-Flow FM

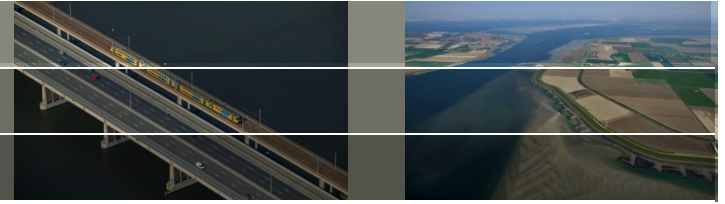


Why DFM?

Specific features of DFM

Some applications

Why DFM



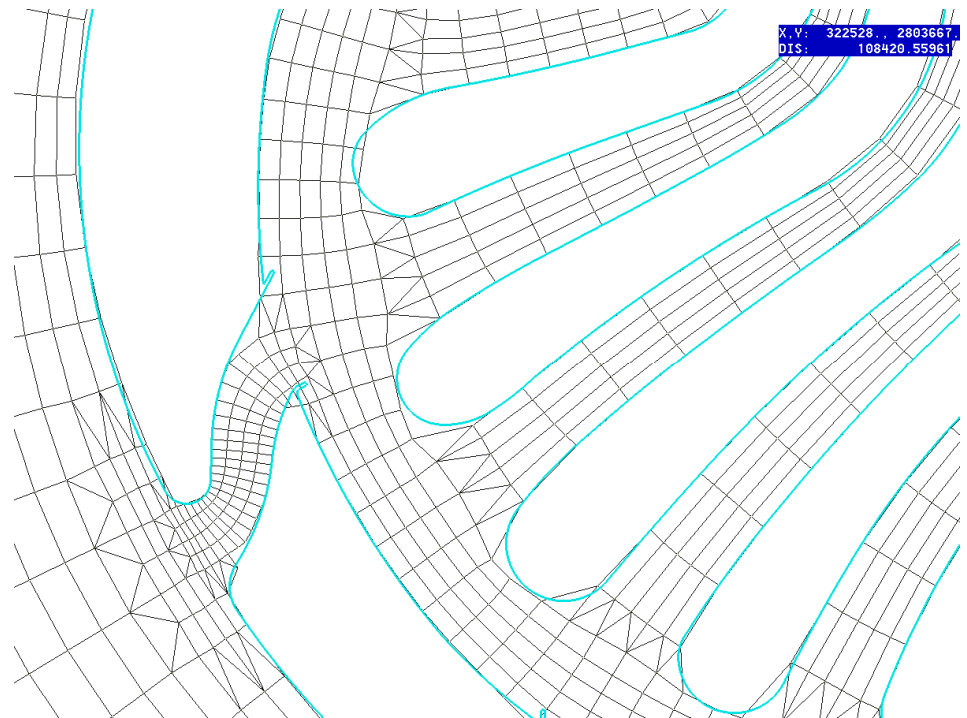
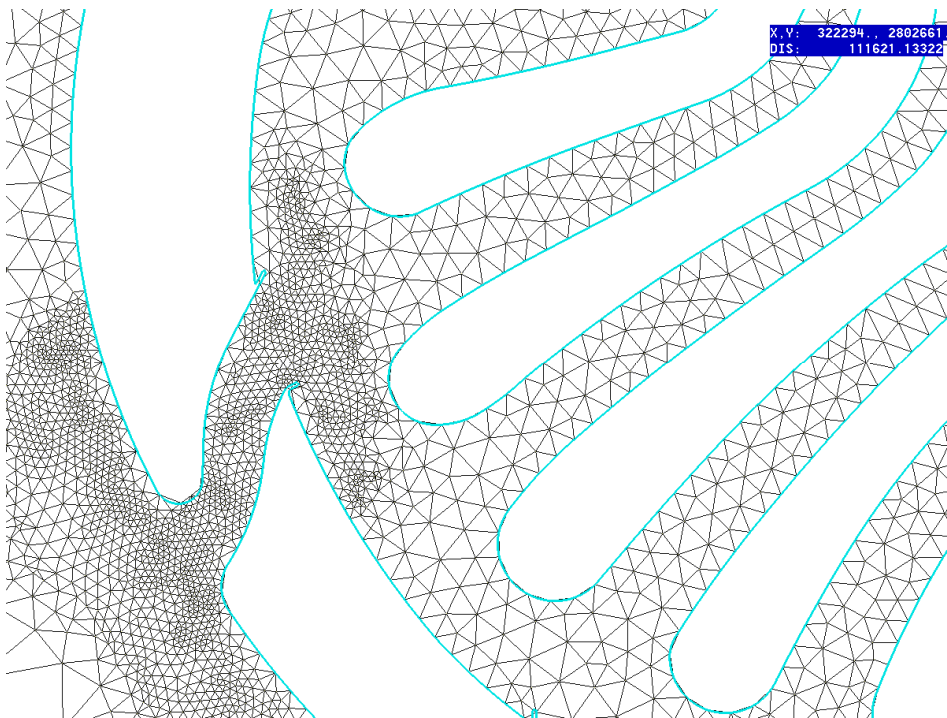
Sobek-1 D2D

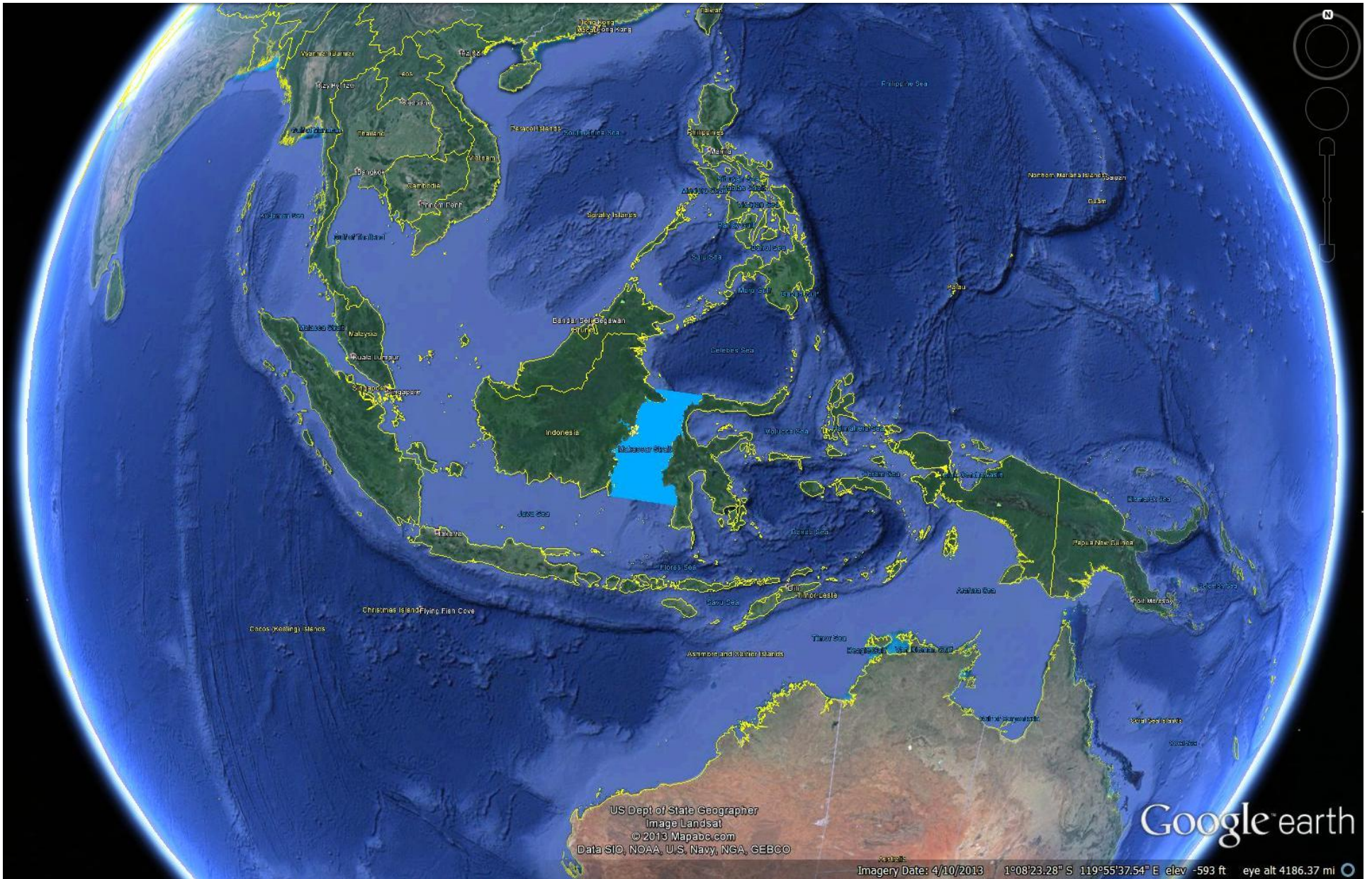


Delft3D/TRIWAQ



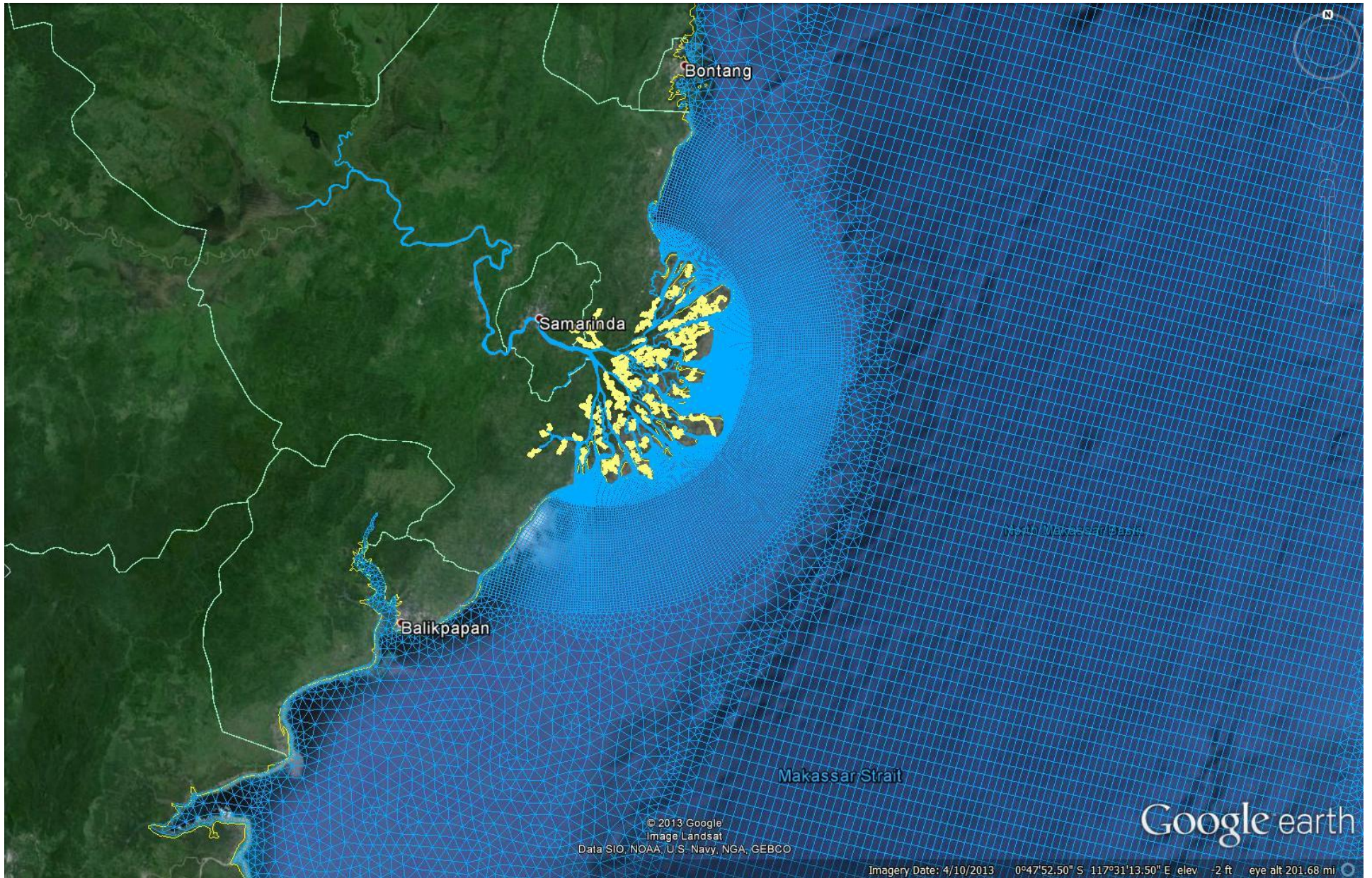
Preferred : Curvilinear + occasional triangle



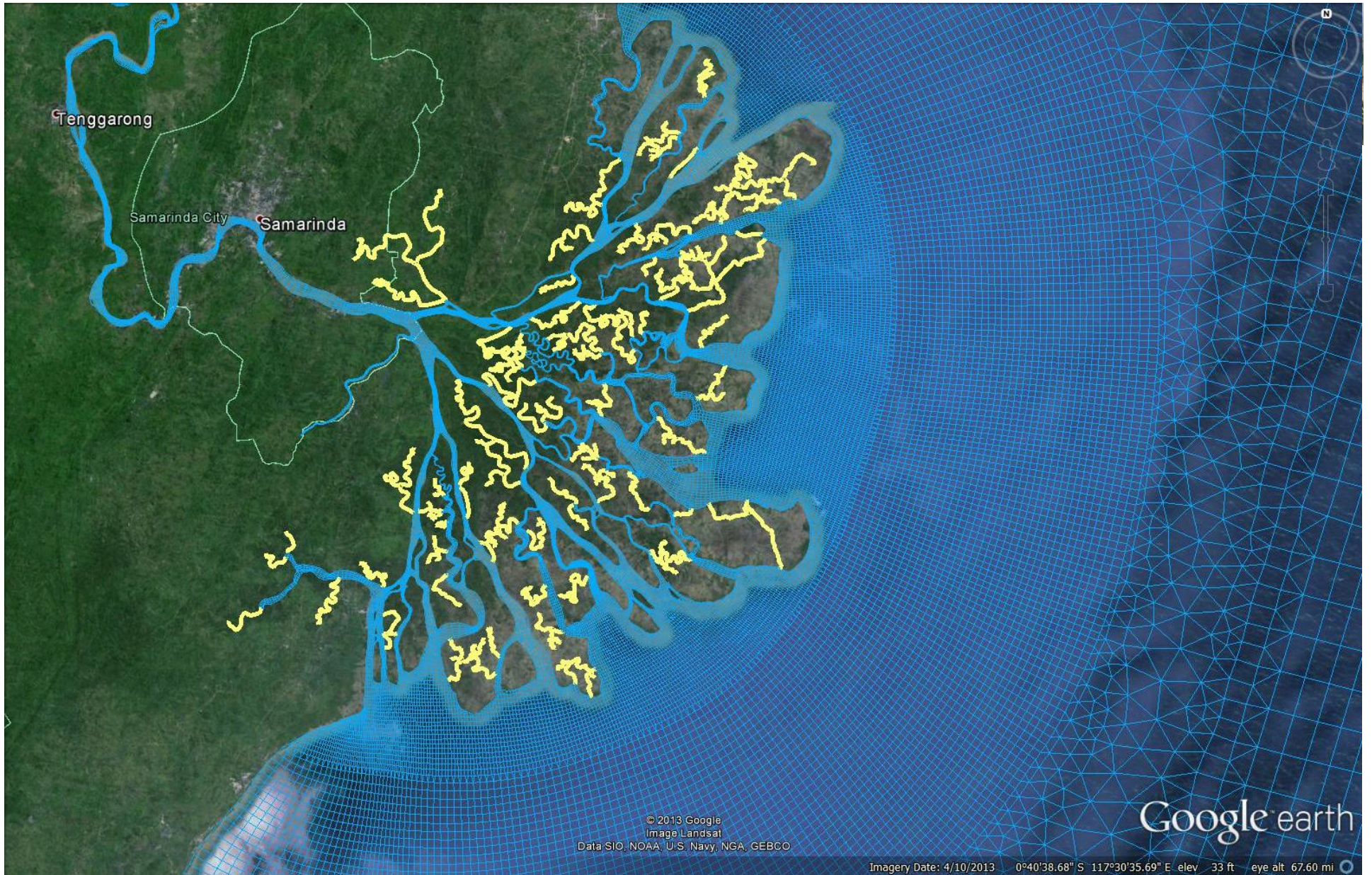


Deltares

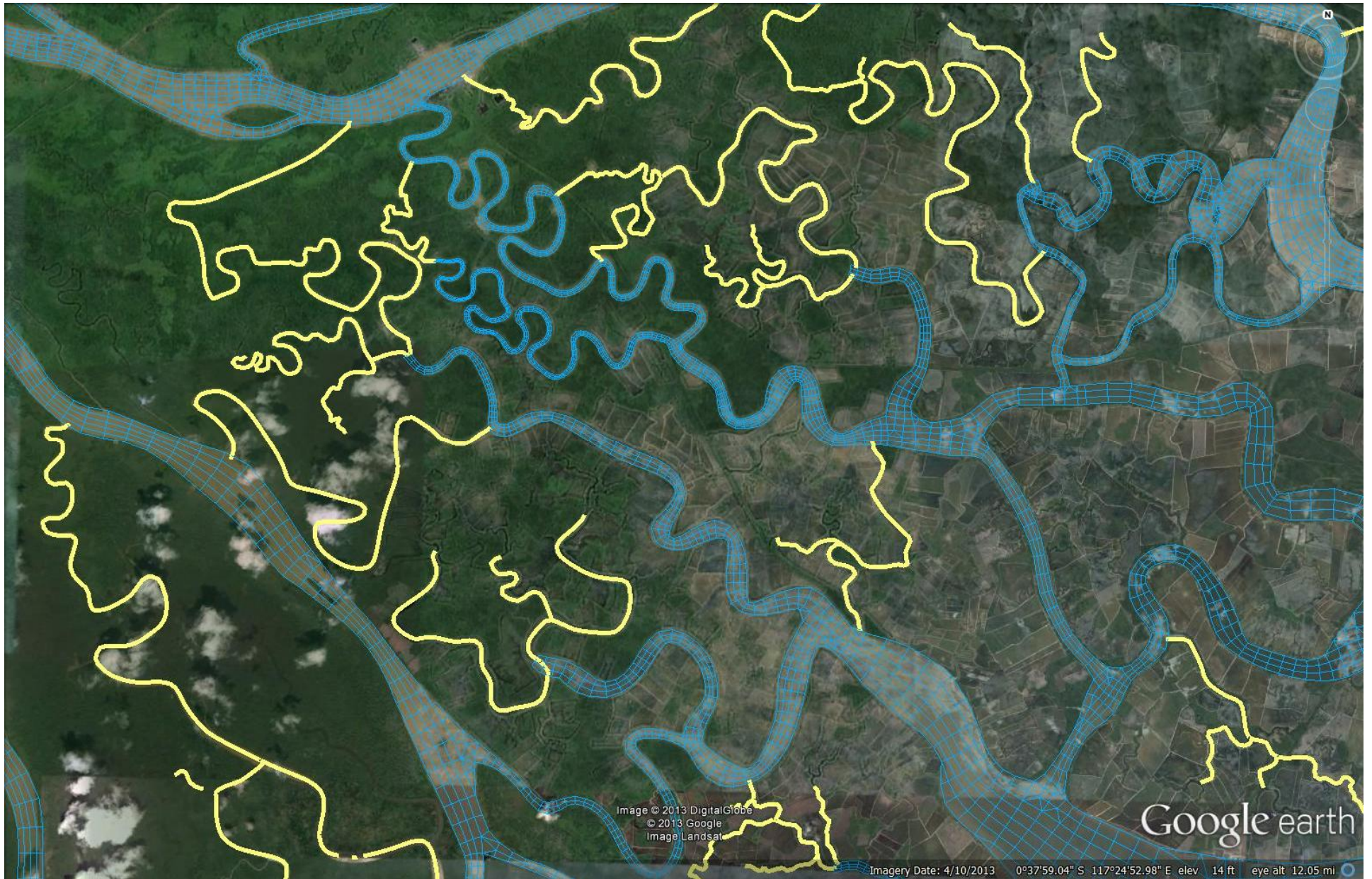




Deltares

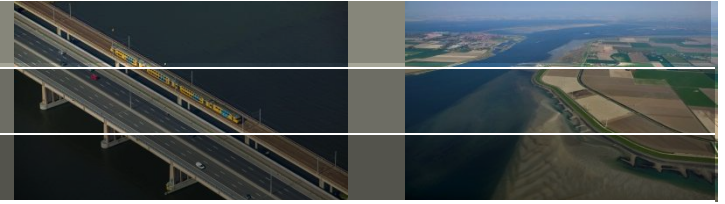


Deltares

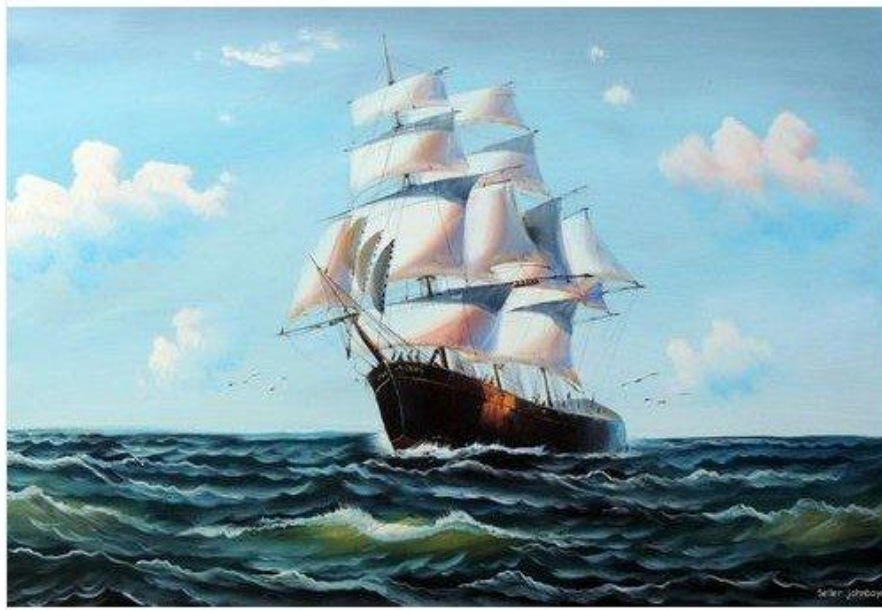
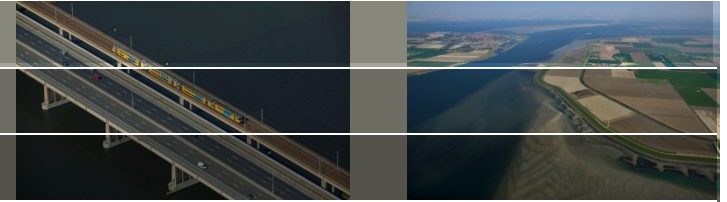


Deltares

Specific features of DFM



Flow speed vs Wave speed

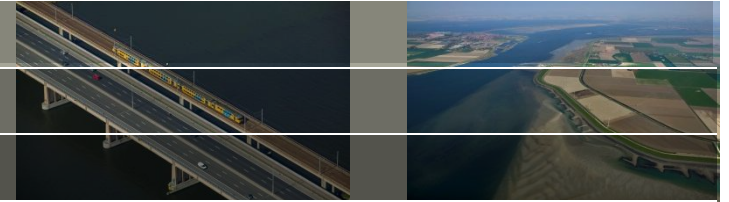


1-2 m/s => Advection explicit



221 m/s => Pressures implicit

Finite volume approach



Conservation of:

$$\frac{\partial V}{\partial t} = \sum_{in\zeta} Q - \sum_{out\zeta} Q$$

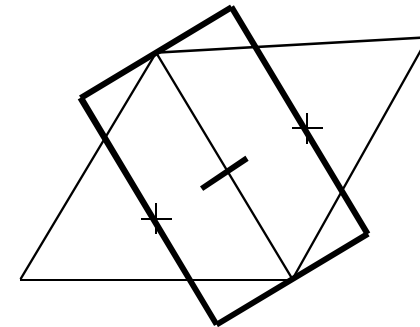
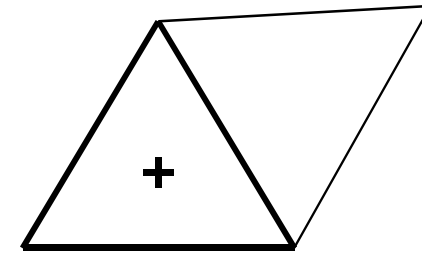
Volume

$$\frac{\partial Vc}{\partial t} = \sum_{in\zeta} Qc_{in} - \sum_{out\zeta} Qc_{out}$$

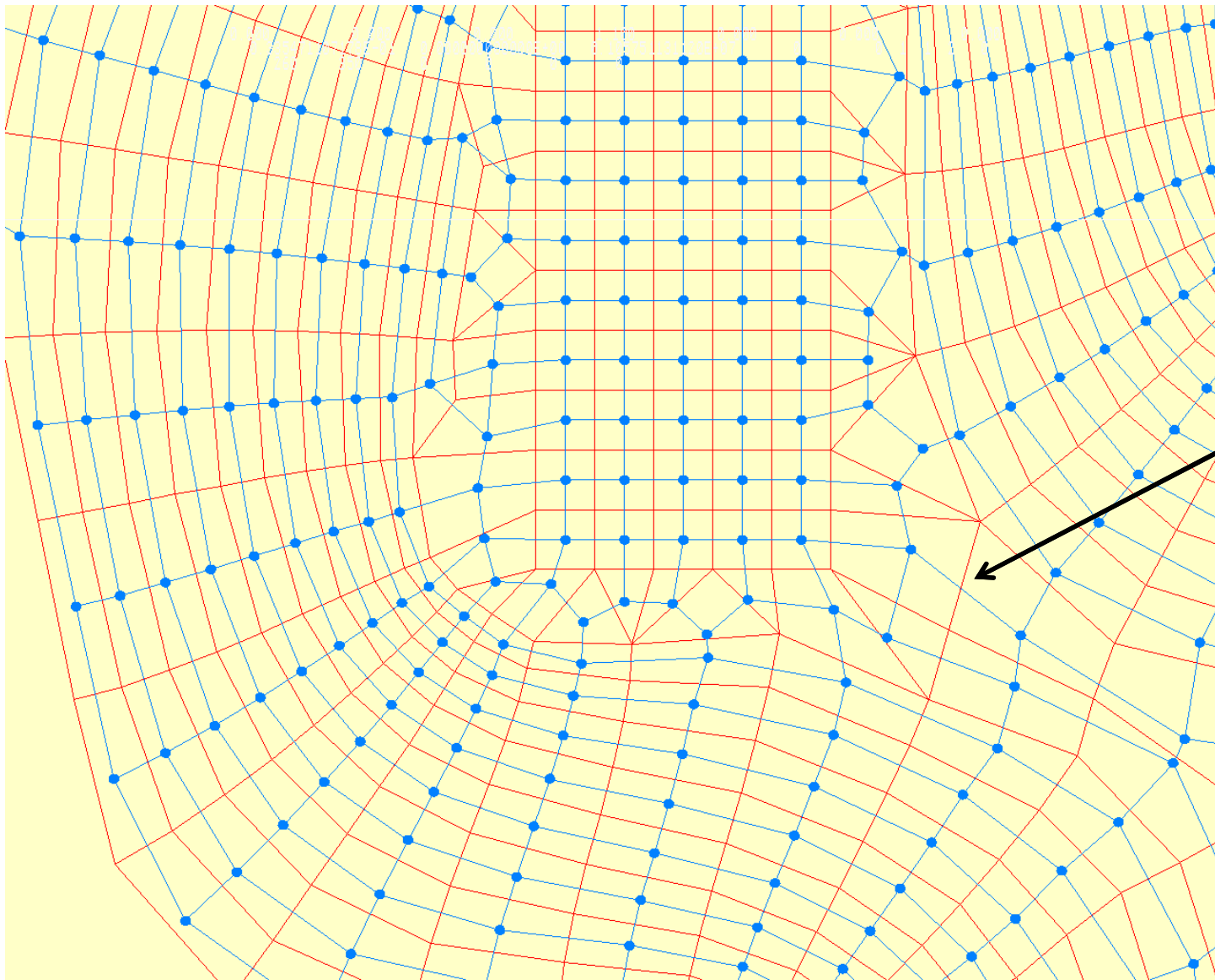
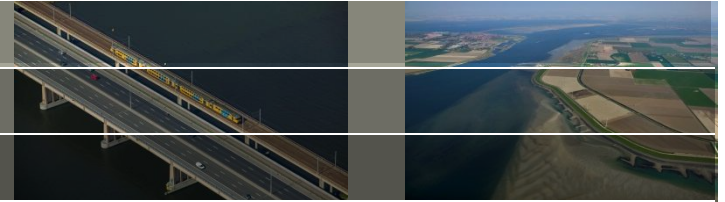
Mass

$$\frac{\partial V_u \rho u}{\partial t} = \sum_{inu} Q \rho_{in} u_{in} - \sum_{outu} Q \rho_{out} u_{out} + \sum F_u$$

Momentum



Not Orthogonal

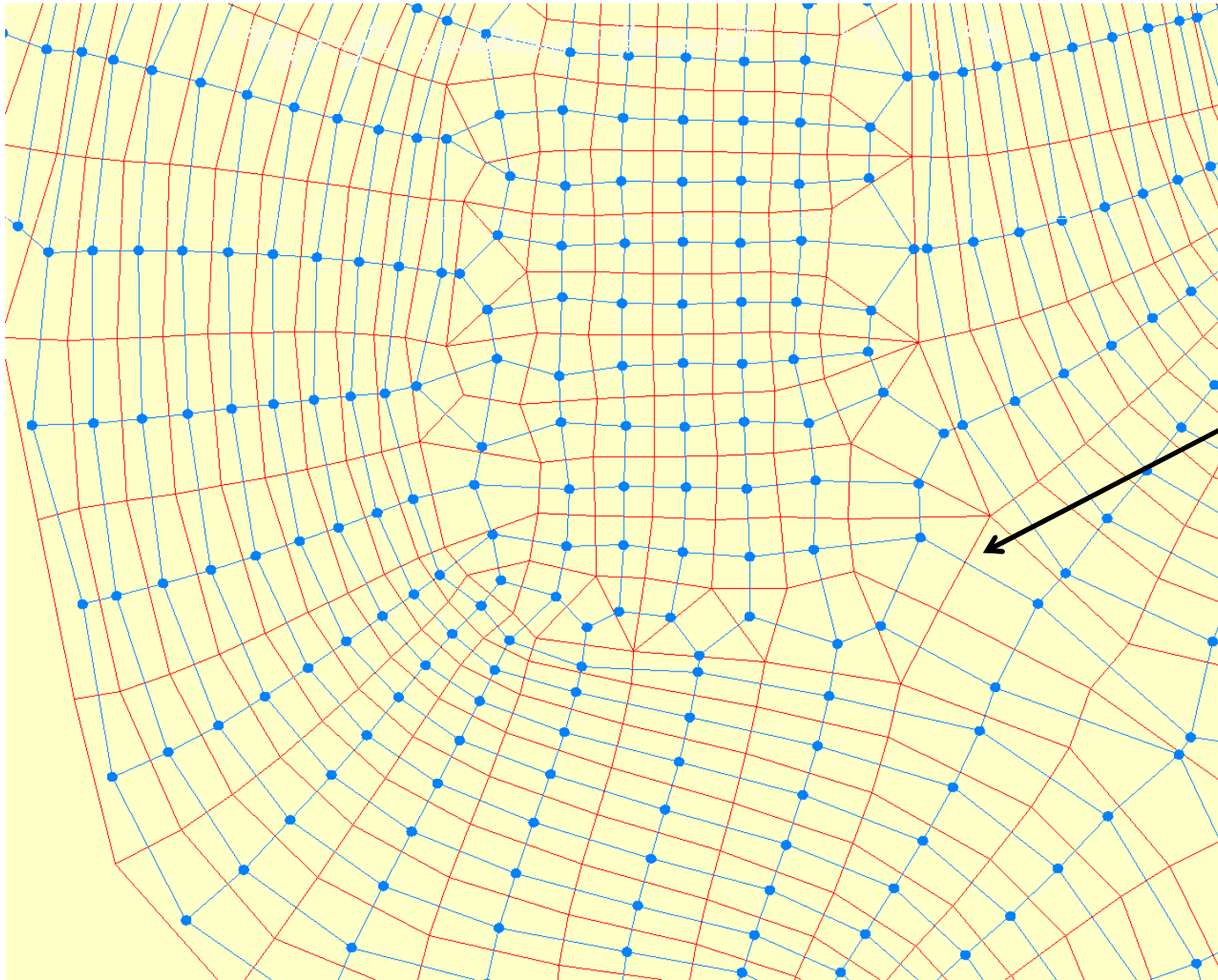
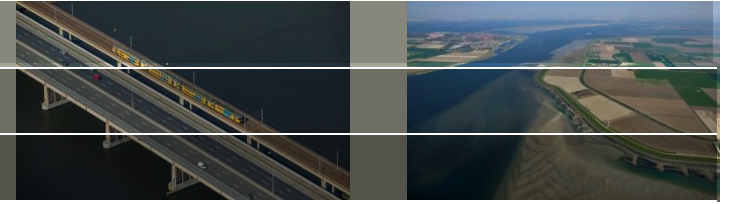


Not o.k.

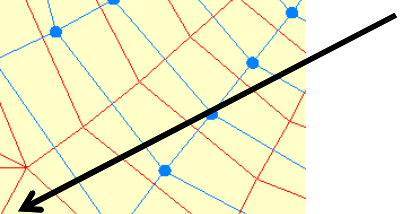
A black arrow points from the text "Not o.k." to a specific point in the grid where the lines are particularly distorted or non-orthogonal.

Deltares

Orthogonal !

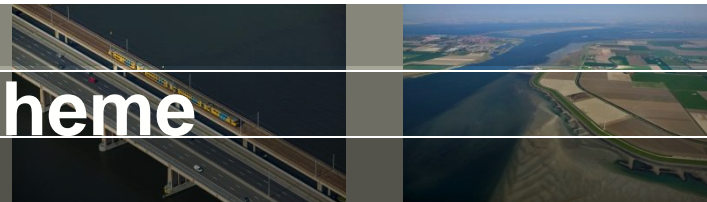


o.k.



Deltares

Shock capturing advection scheme

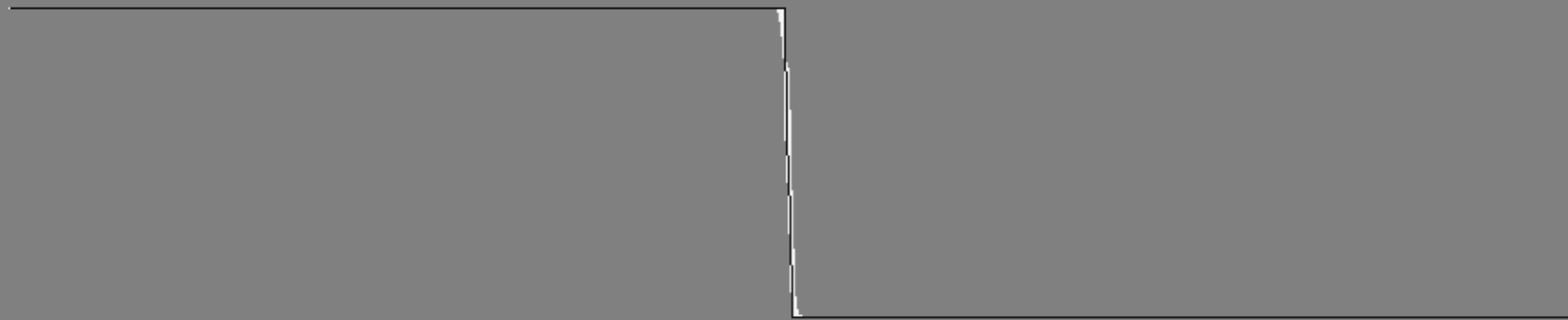


```

20061225_000030 dt: 3.321 Avg.dt: 2.000 CPU/step: 0.010 Tot: 0.2 Sol/Rest: 0.524 Samer: 0.00000000E+00
k/nplot: 1 2 znod(nn) 2.0000000 Uo11: 0.25562155E+09 U1er: -.29802322E-07 #setb: 0 #dt: 15 #itsol: 7
#CG: 4670 #Gauss: 11028 #expl: 0 #wet: 15698 #chkadvd: 0 #nodneg: 0 #slit: 0 runid: wetbed

```

3.010



-0.020

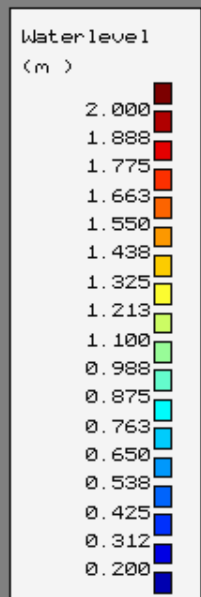
-0.120E+03

0.661E+05

```

Ave Difference (m) = 0.0008
Rms Difference (m) = 0.0130
Max Difference (m) = 0.6964
Cum Difference (m) = 0.0006

```



X

```

20061225_000030 dt: 3.321 Avg.dt: 2.000 CPU/step: 0.207 Tot: 2.9 Sol/Rest: 0.016 Samer: 0.00000000E+00
k/nplot: 1 2 znod(nn) 2.0000000 Uo11: 0.25562155E+09 U1er: 0.00000000E+00 #setb: 0 #dt: 15 #hitsol: 7
#CG: 4670 #Gauss: 11028 #expl: 0 #wet: 15698 #chkadvd: 0 #nodneg: 0 #slit: 0 runid: wetbed3d

```

3.010-



-0.020+

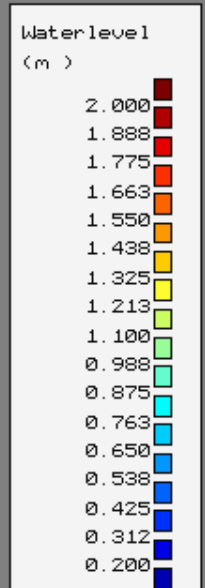
-0.120E+03

0.661E+05

```

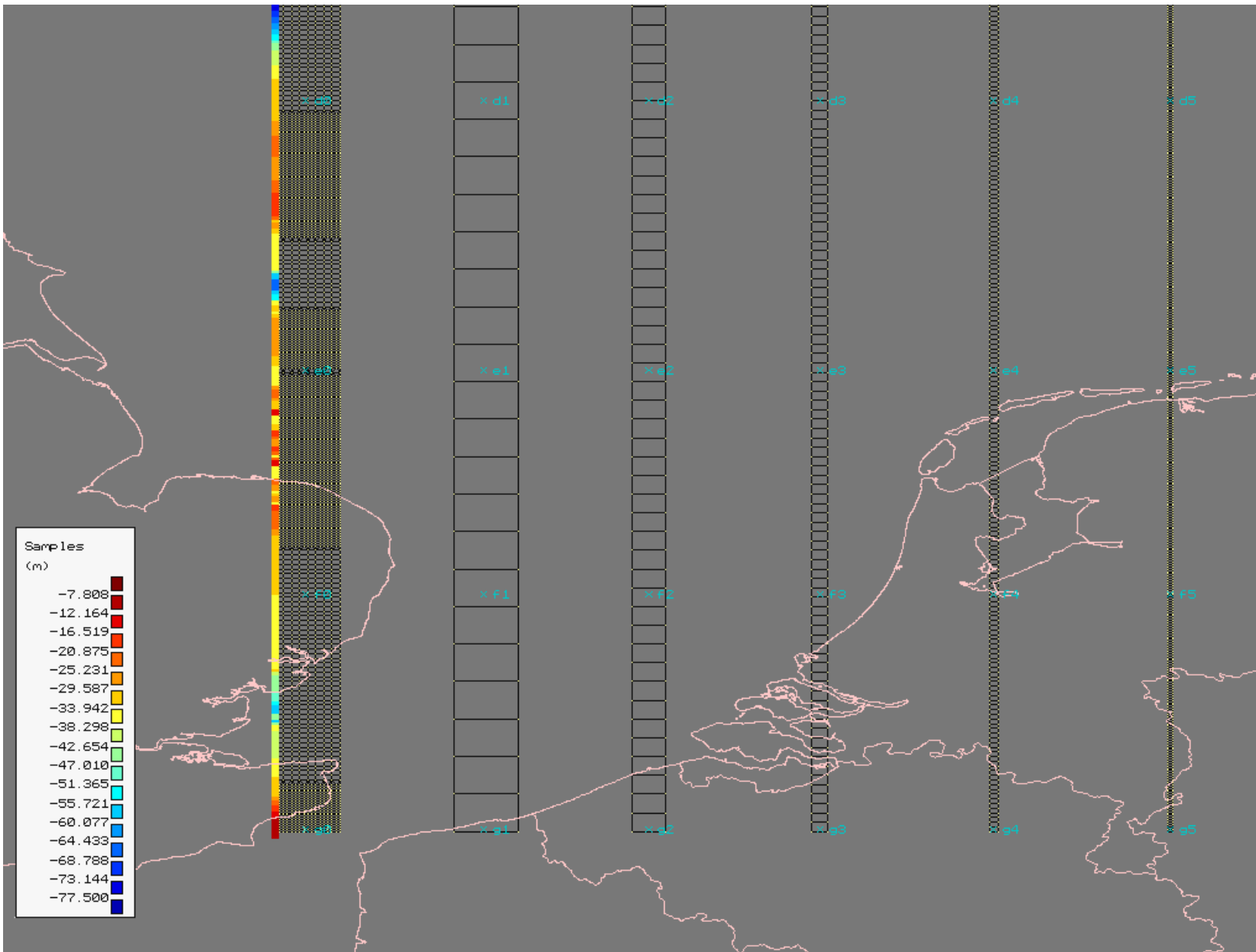
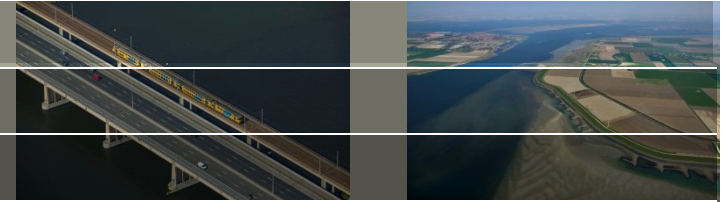
Ave Difference (m) = 0.0008
Rms Difference (m) = 0.0130
Max Difference (m) = 0.6964
Cum Difference (m) = 0.0006

```

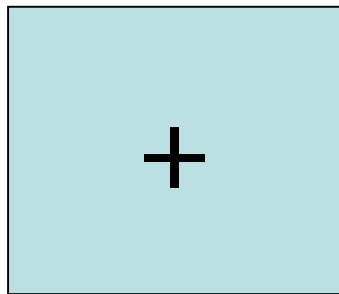
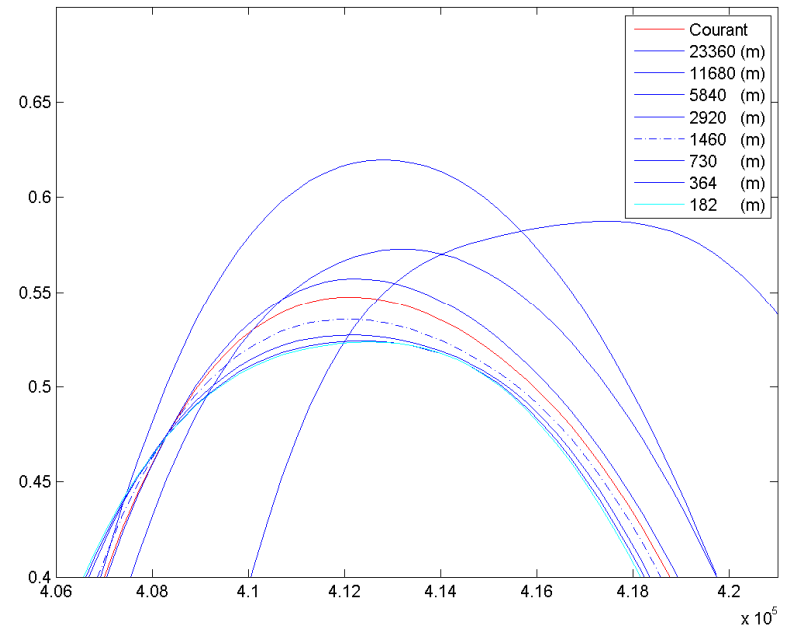
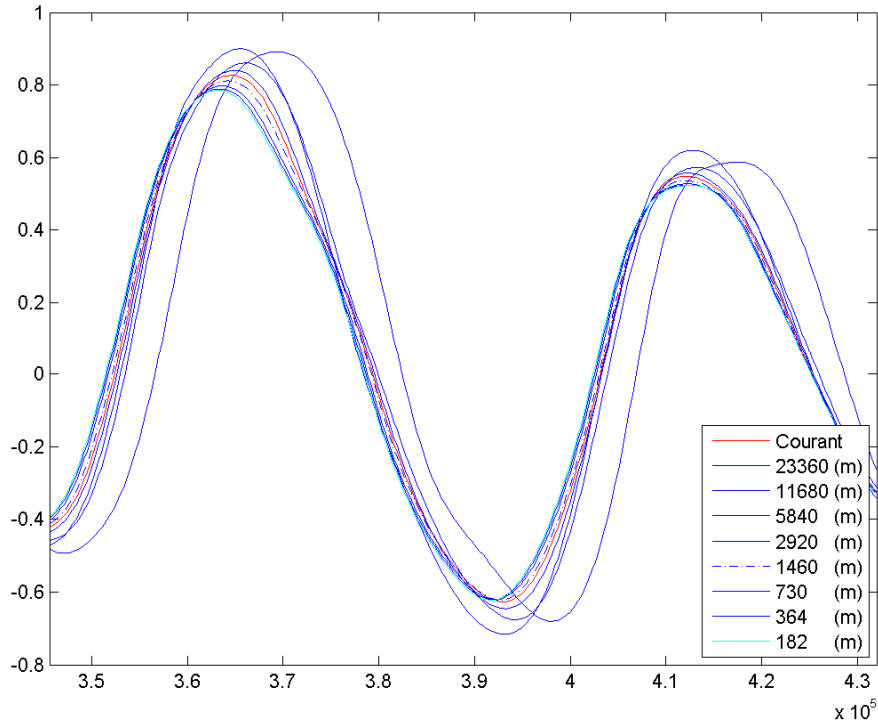
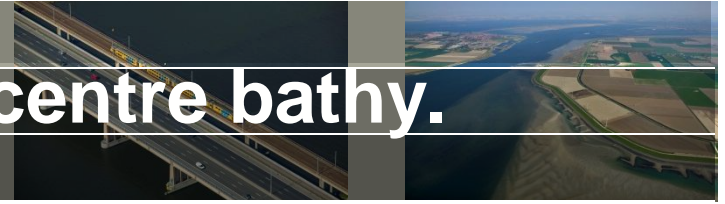


X

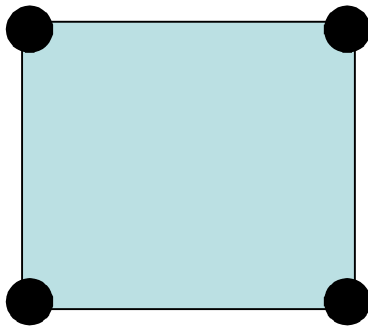
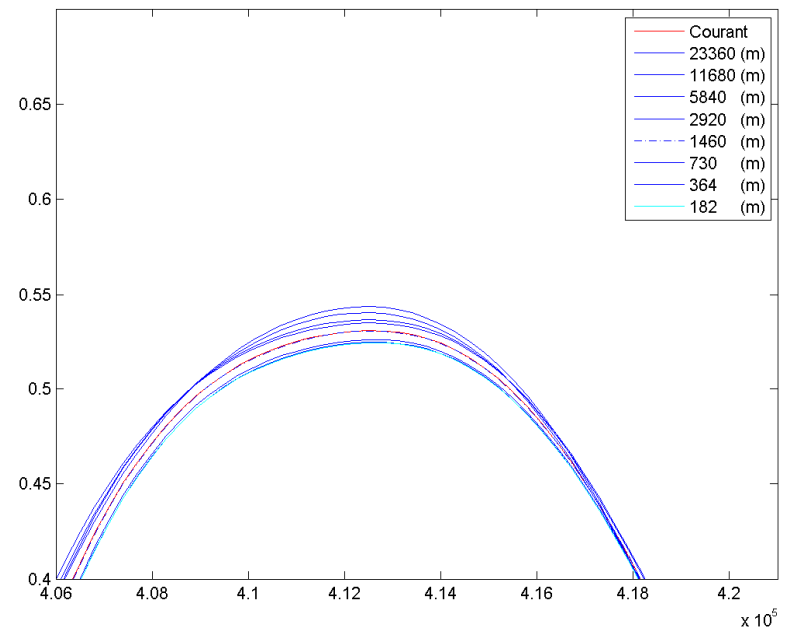
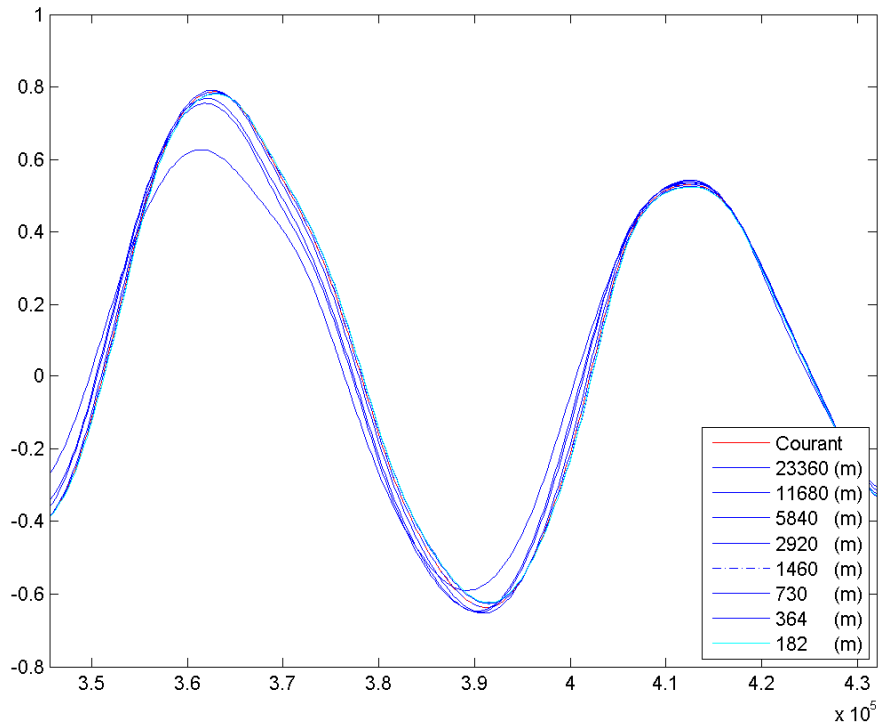
Spatial convergence



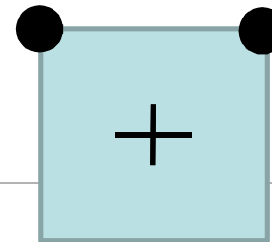
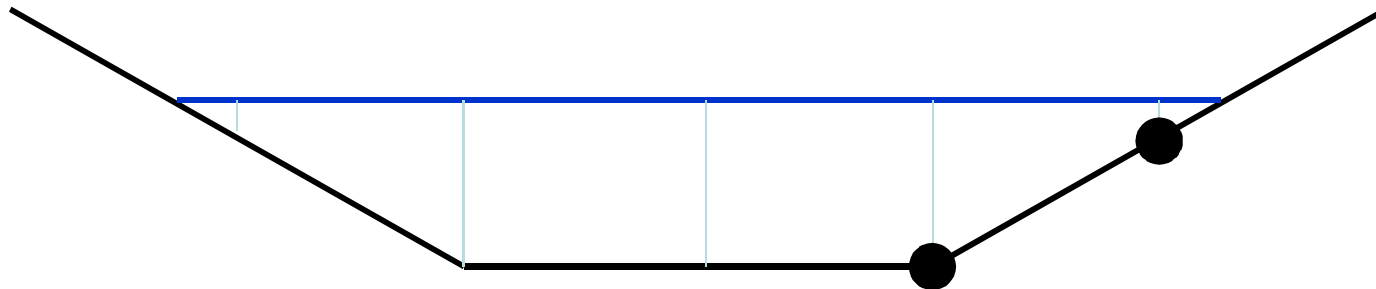
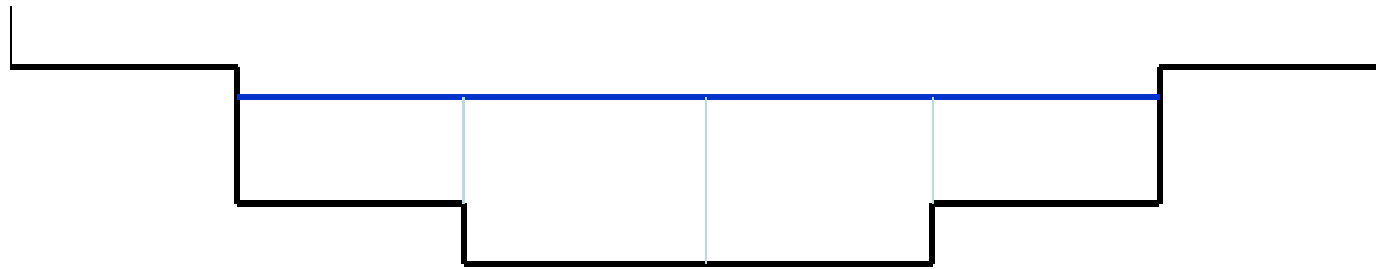
Grid convergence parallel: cell centre bathy.



Grid convergence parallel: netnode bathy.



Continuous wet area => more gradual drying & flooding



Deltares

peak flows ~ 6 m/s



Subgrid: Analytic 2D Conveyance approach

$$\frac{uU}{C^2R} = i, U = \frac{u}{\beta^2}$$

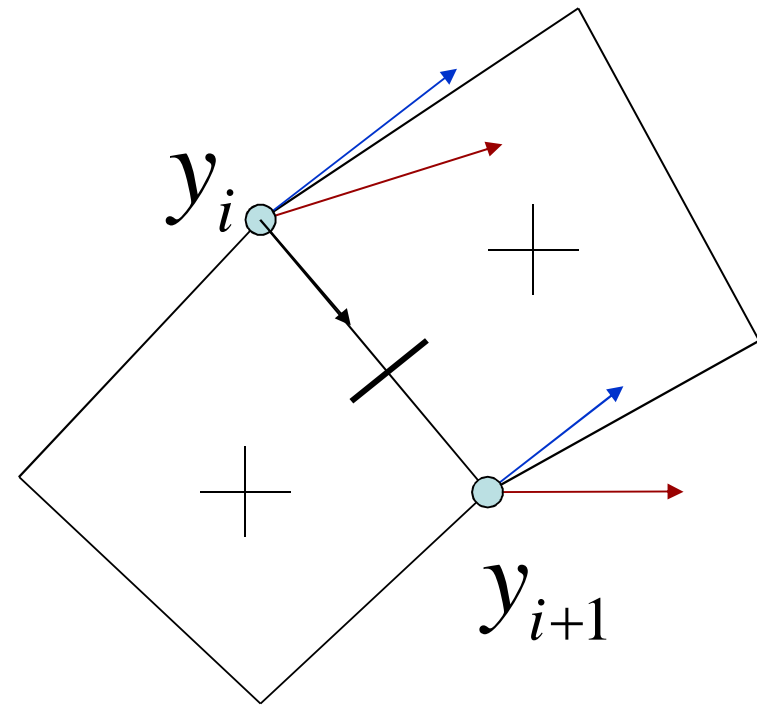
$$u_j = \beta C \sqrt{R_j} \sqrt{i}, K_\beta = \frac{\beta A_j R_j^{\frac{2}{3}}}{n}$$

$$\beta = \beta_i - \delta (y - y_i), \delta = \frac{\beta_i - \beta_{i+1}}{y_{i+1} - y_i}$$

$$K_\beta = \int_{y_i}^{y_{i+1}} \frac{\beta_i - \delta (y - y_i)}{n(1 + \alpha_i^2)^{\frac{1}{4}}} (h_i - \alpha_i (y - y_i))^{\frac{5}{3}} dy$$

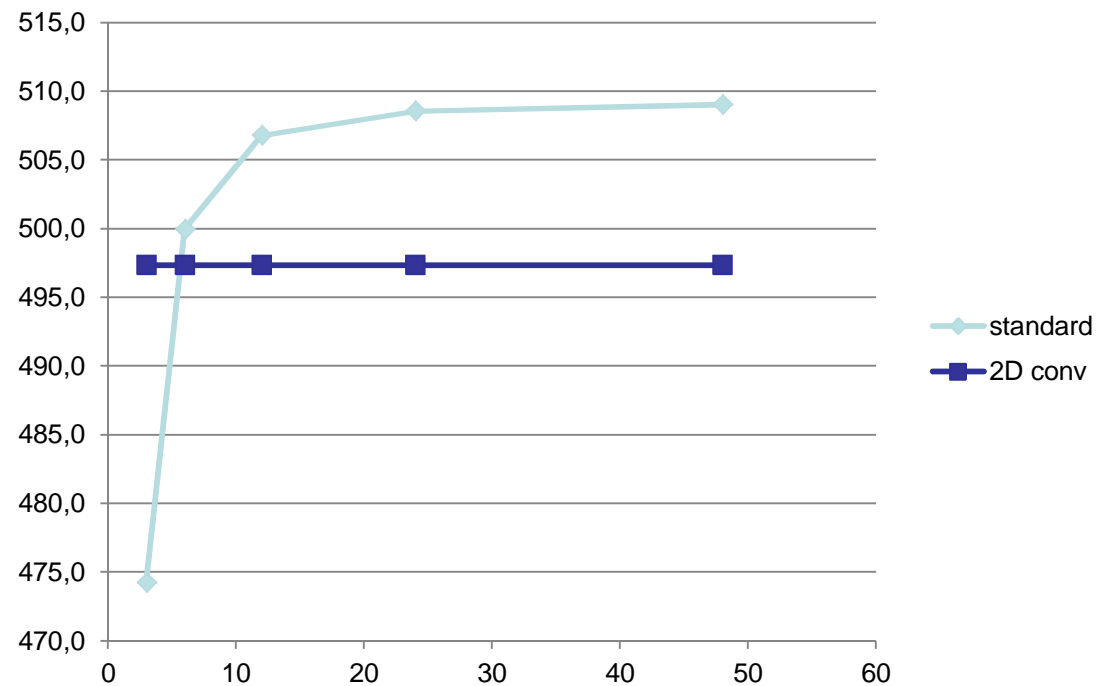
$$K_\beta = \frac{T}{n(1 + \alpha_i^2)^{\frac{1}{4}}}$$

$$T = \int_{y_i}^{y_{i+1}} (\beta_i - \delta (y - y_i)) (h_i - \alpha_i (y - y_i))^{\frac{5}{3}} dy$$



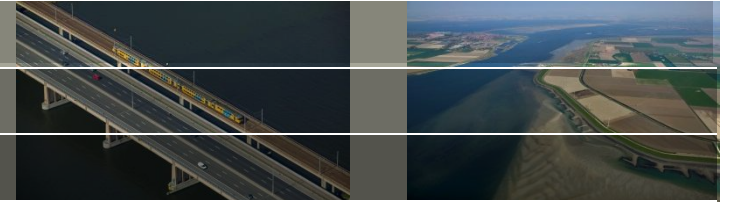
Subgrid, grid convergence flow perpendicular

Discharge m³/s



Nr of cells in cross-sectional direction.

Subgrid: non-linear volumes



$$\frac{dV}{dt} + \sum_{out} Q - \sum_{in} Q = 0$$

$$\frac{V^{n+1} - V^n}{\Delta t} + \sum_{out} A_u u - \sum_{in} A_u u = 0$$

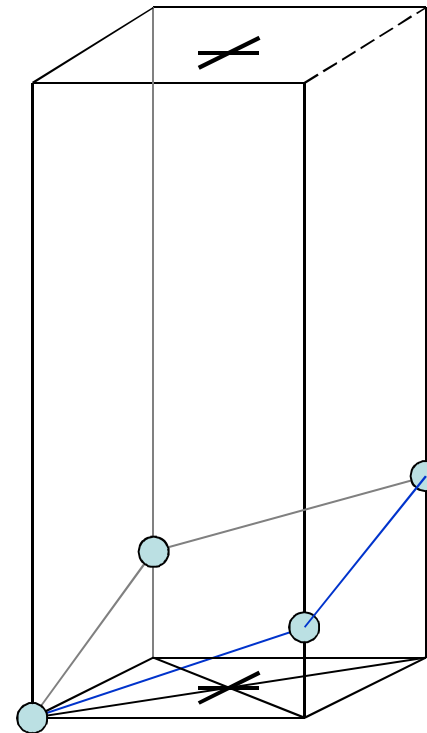
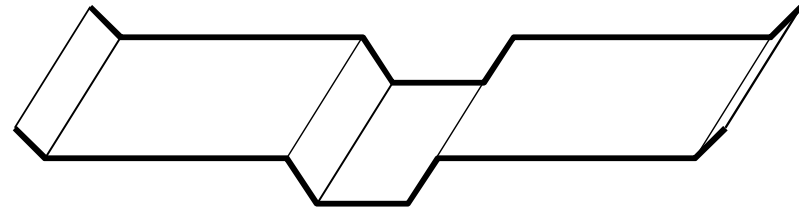
Large change of volume
with waterlevel:

Newton iteration

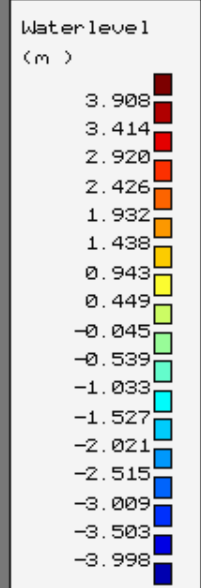
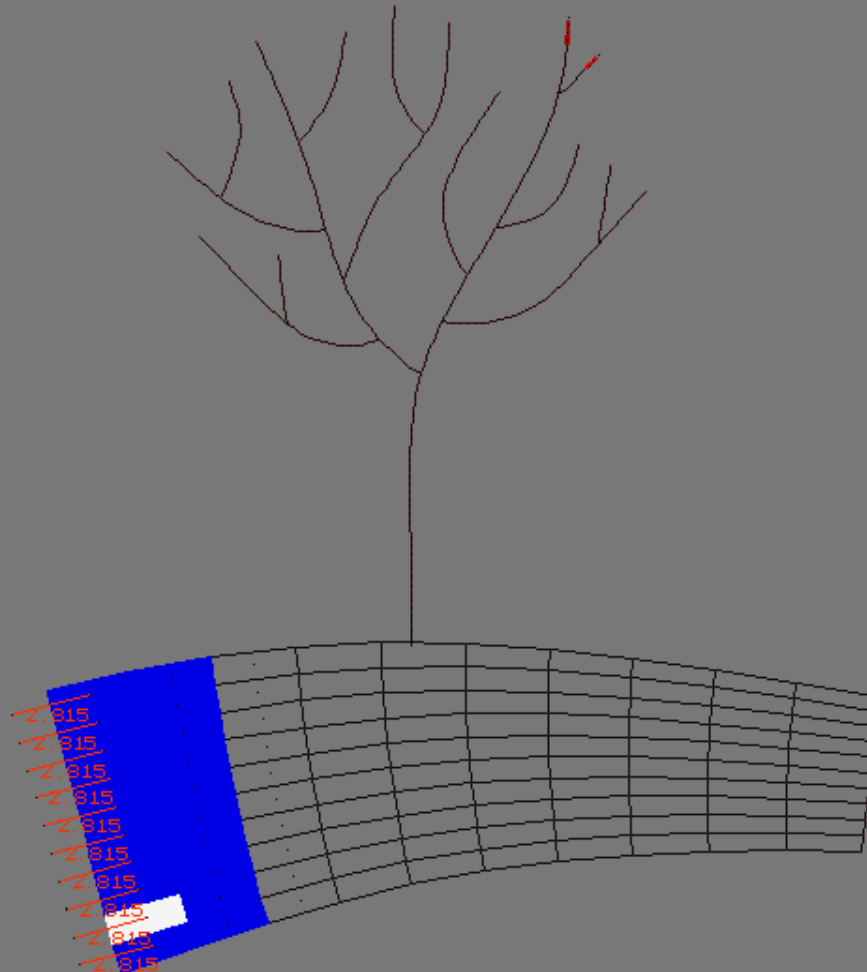
$$V^{p+1} = V^p + (\zeta^{p+1} - \zeta^p) \frac{\partial V^p}{\partial \zeta}$$

$$V^{p+1} = V^p + (\zeta^{p+1} - \zeta^p) A_\zeta^p$$

$$\frac{V^p - V^n + (\zeta^{p+1} - \zeta^p) A_\zeta^p}{\Delta t} + \sum_{out} A_u u - \sum_{in} A_u u = 0$$

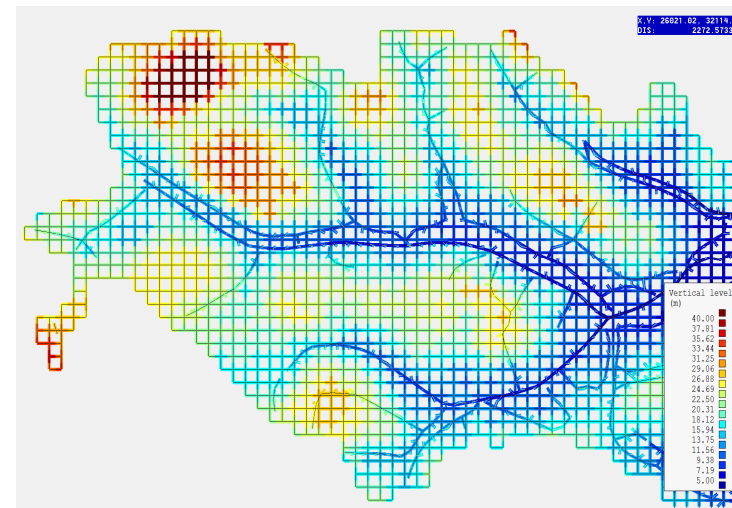


```
19920831_000040 dt: 5.118 Avg.dt: 2.353 CPU/step: 0.000 Tot: 0.0 Sol/Rest: 0.200 Samer: 0.00000000E+00
k/nplot: 1 2 znod(nn) -3.5762265 Uo11: 0.11091880E+07 U1er: 0.30345291E-08 #setb: 0 #dt: 17 #itsol: 0
#CG: 7 #Gauss: 43 #expl: 0 #wet: 50 #chkadvd: 0 #nodneg: 0 #slit: 4 ruid: tree1d2d
```



Nonlinear continuity 1D2D

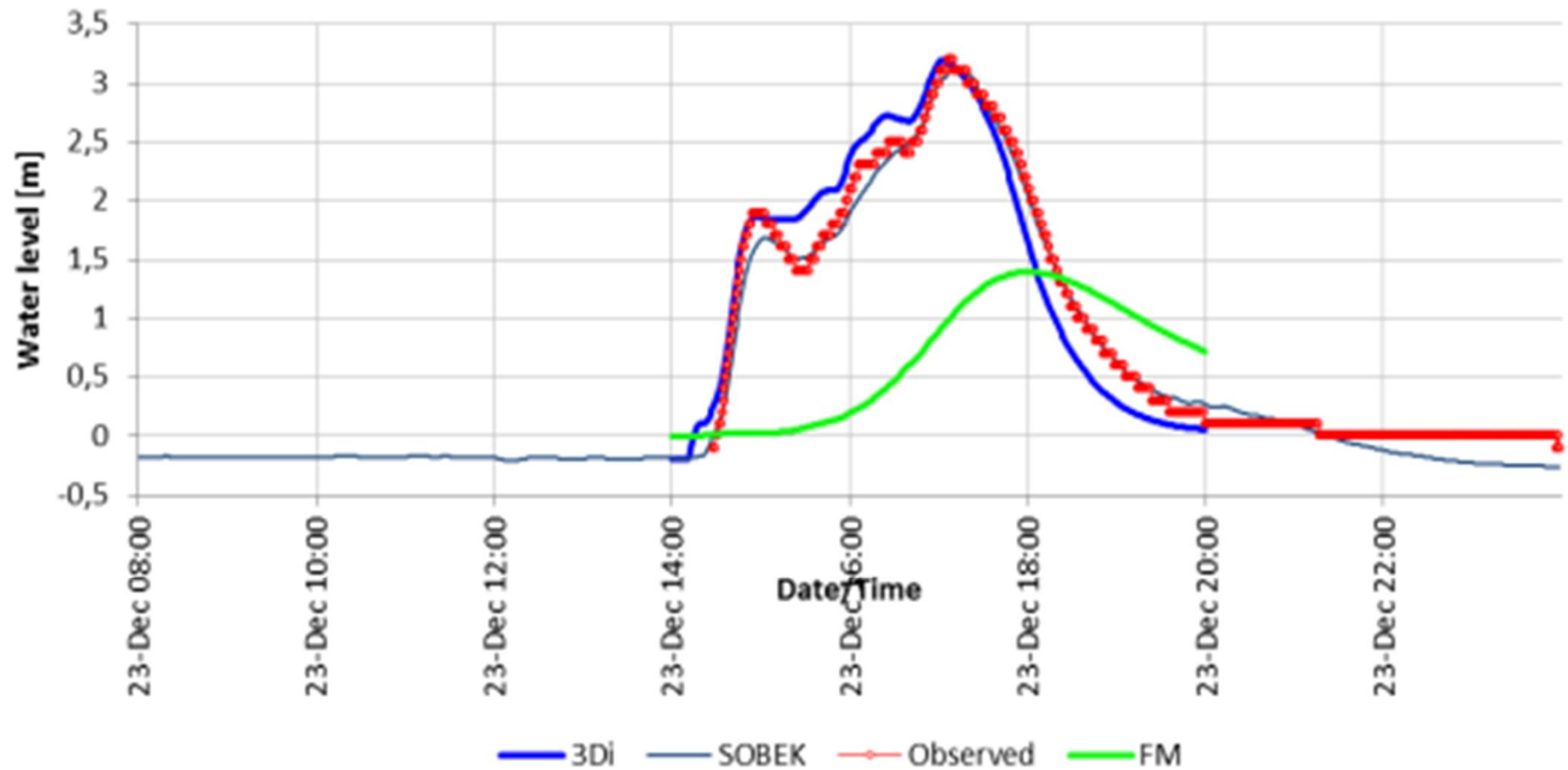
Singapore rainfall runoff: Non-linear volumes



Singapore rainfall runoff: Linear volumes



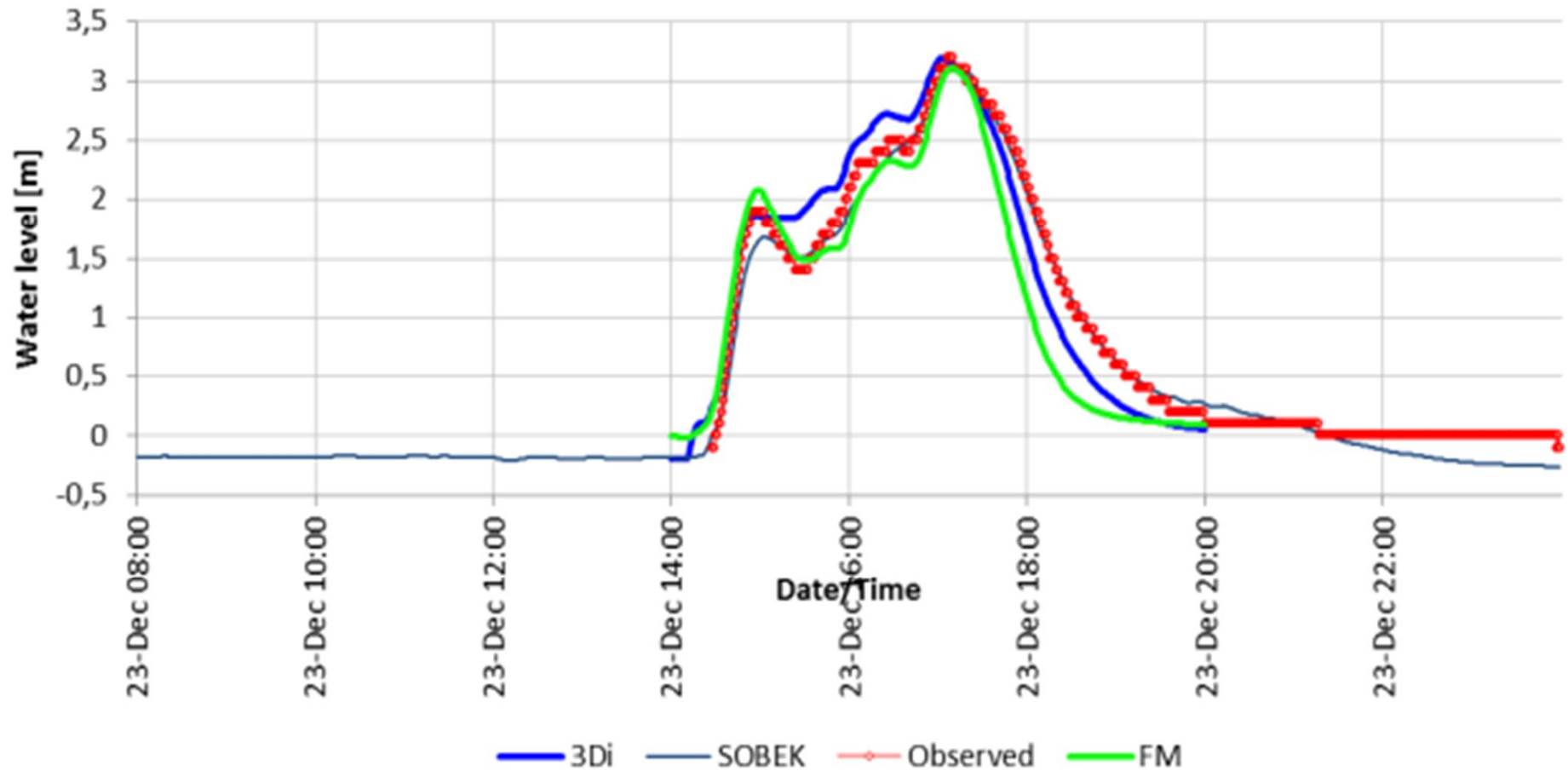
HMC209 Killiney Rd



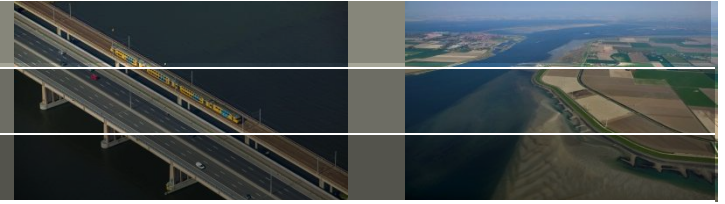
Singapore rainfall runoff: Non-linear volumes



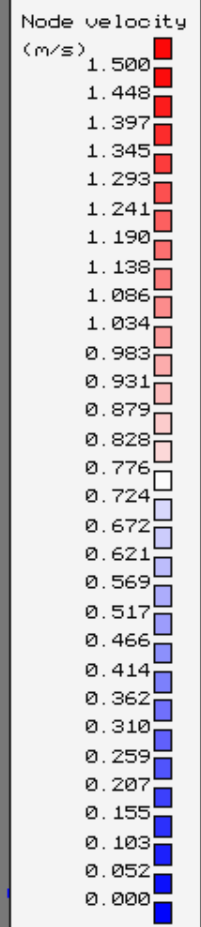
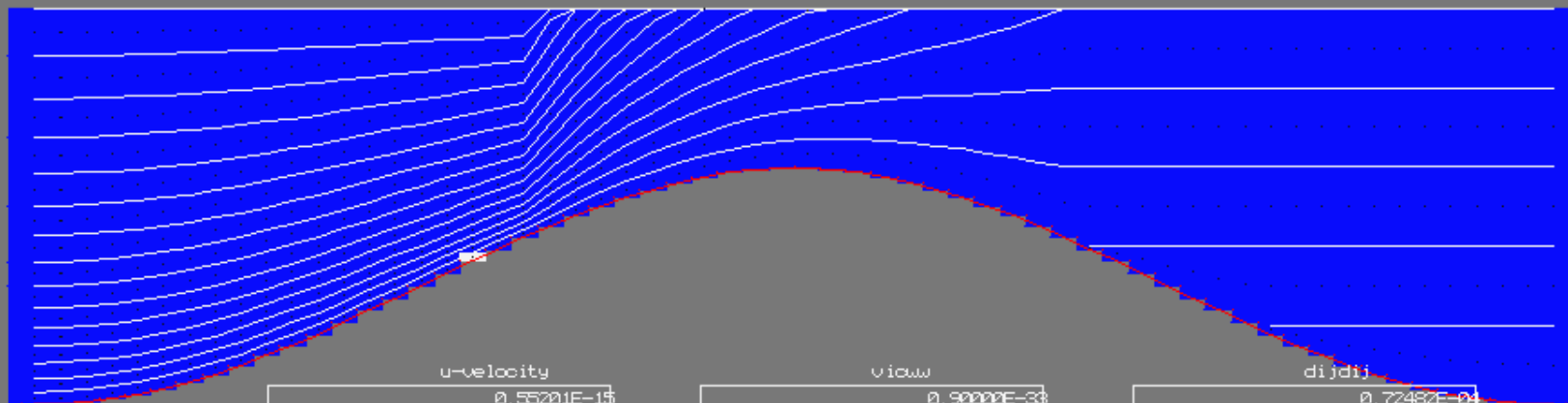
HMC209 Killiney Rd



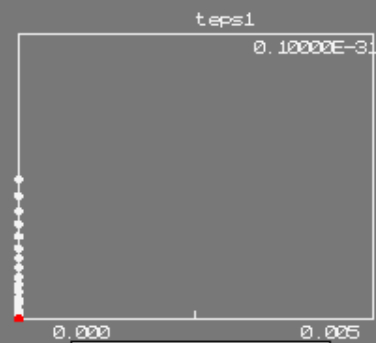
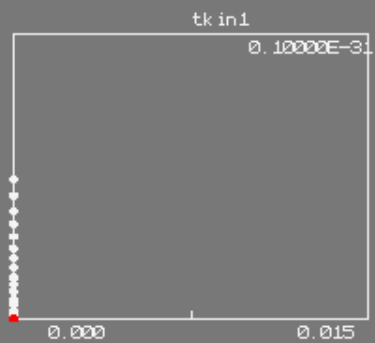
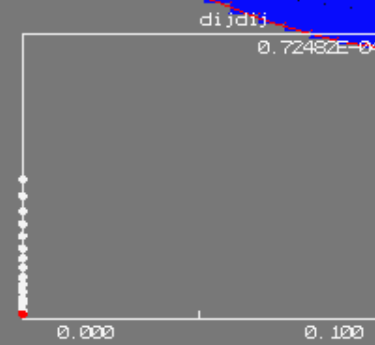
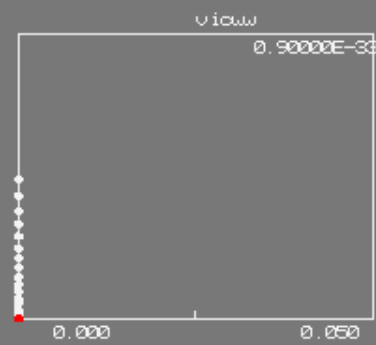
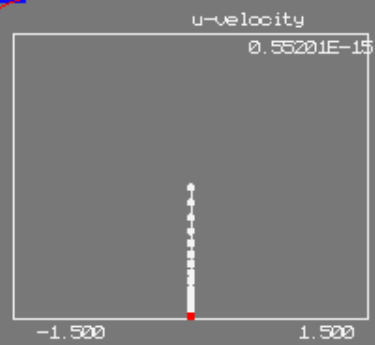
Flexible in vertical



Time S/H/D: 3.000 0.001 0.000 dt: 1.000 Avg. dt: 0.750 CPU/step: 0.000 Tot: 0.0 Sol/Rest: 0.000
 k/nplot: 1 18 znod(nn) 0.000000 Uo11: 0.42600247E+05 U1er: 0.24656840E+00 #setb: 0 #dt: 3 #itsol: 0
 #CG: 0 #Gauss: 62 #expl: 0 #wet: 62 #chkadv: 0 #nodneg: 0 #slit: 0



-10.0+
-1.20



k-eps sanctum

0.000 m3/s

X

Epsilon b.c. : Flux mid layer ~ Delft3D
Ustar : Layer integrated unlike Delft3D



D3D

$$\varepsilon = c_{ew} \text{all}^* \left(\frac{u_*^2}{\sqrt{c_\mu}} \right)^{1.5} / z_0$$

$$U_{t(\Delta z/2)} = \kappa u_* z_0$$

DPM, DFM

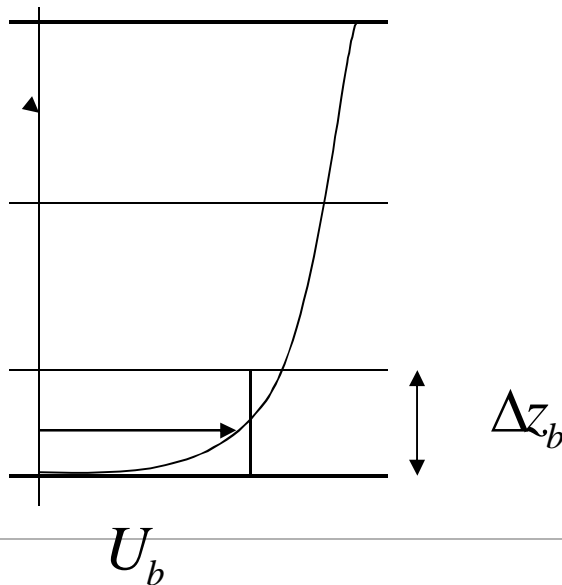
$$\frac{\partial \varepsilon}{\partial z} = \frac{(\varepsilon_{b+1} - \varepsilon_b)}{\Delta z_b} = \frac{u_*^3}{\kappa \left(\frac{\Delta z_b}{2} + 9 \right)^2}$$

Mid layer

Layer integrated

Delft3D, DPM

DFM, TRIWAQ



$$u_* = \frac{\kappa U_b}{\ln \left(\frac{\Delta z_b}{2 z_0} + 1 \right)}, \quad \text{or} \quad u_* = \frac{\kappa U_b}{\ln \left(\frac{\Delta z_b}{e z_0} + 1 \right)}$$

Log profile: Friction vs Pressure

slope.mdu

$$L=610 \text{ m}$$

$$i=5e-5$$

$$H=5 \text{ m}$$

$$C=60 \text{ m}^{0.5}/\text{s}$$

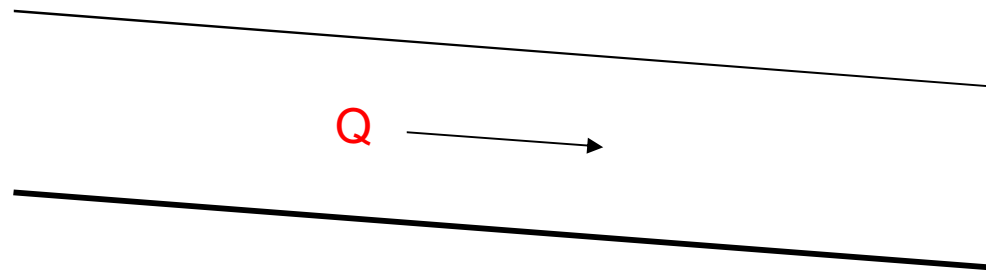
$$Dx=Dy=10 \text{ m}$$

$$U=C(Hi)^{0.5}=0.94868 \text{ m/s}$$

$$Q=47.434 \text{ m}^3/\text{s}$$

$$u_* = Ug^{0.5}/C=0.0495 \text{ m/s}$$

$$K= u_*^2/cm\mu^{0.5}=0.00816 \text{ m}^2/\text{s}^2$$



Constant

$$v_\tau = \kappa u_* H / 6 = 0.0169 \quad (\text{m}^2 / \text{s})$$

Parabolic

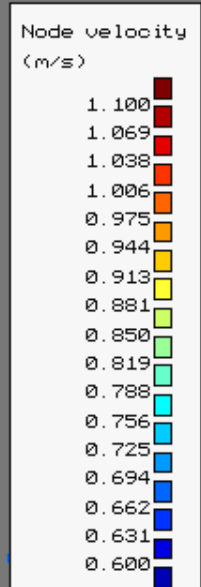
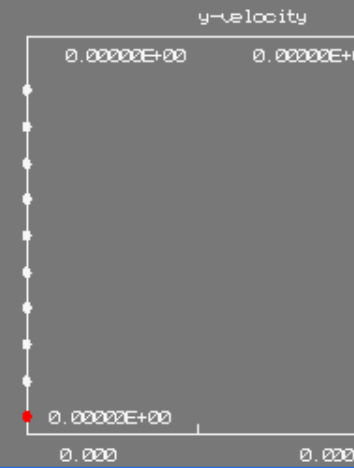
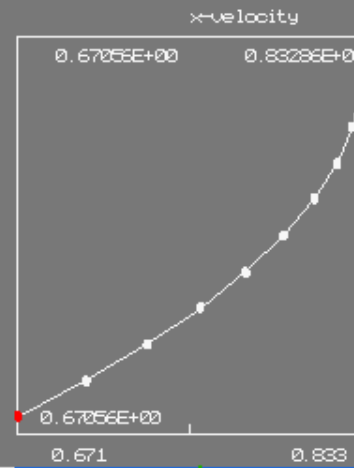
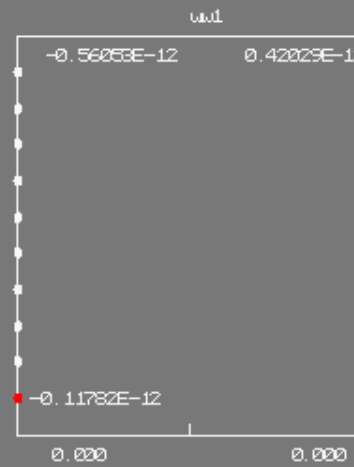
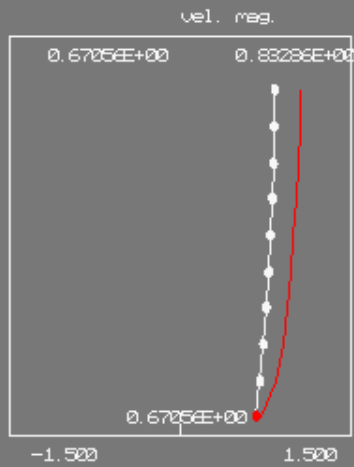
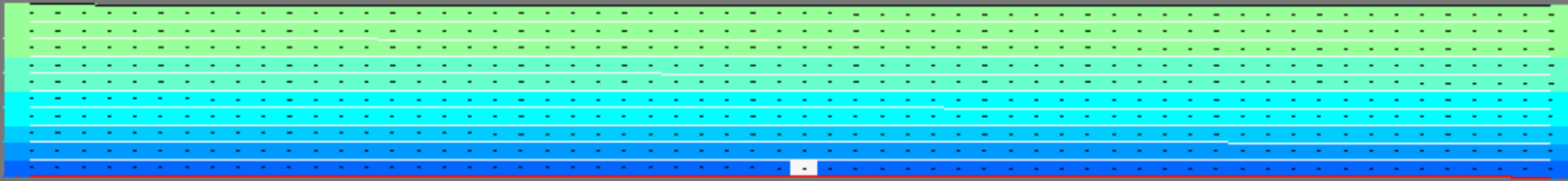
$$v_\tau(z) = \kappa u_* z \left(1 - \frac{z}{H}\right) \quad ; \quad v_\tau(H/2) = 0.0253 \quad (\text{m}^2 / \text{s})$$

K-epsilon

$$v_\tau(H/2) = c_\mu \frac{k_{H/2}^2}{\varepsilon_{H/2}} = 0.0189 \quad (\text{m}^2 / \text{s})$$

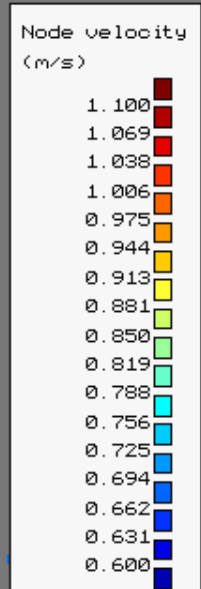
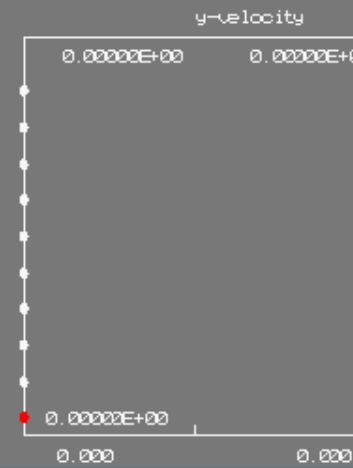
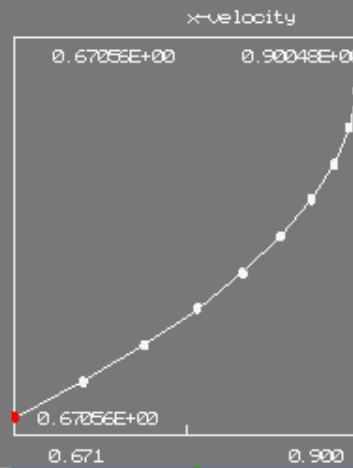
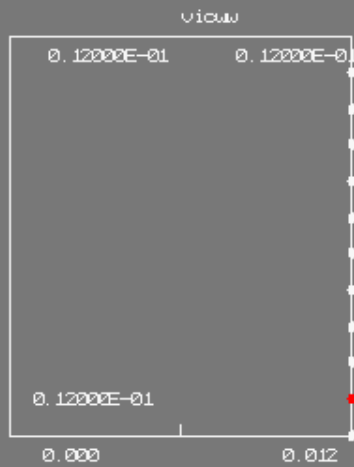
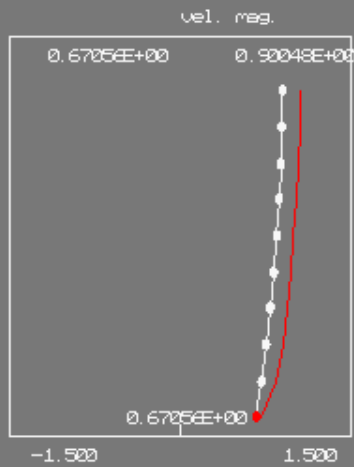
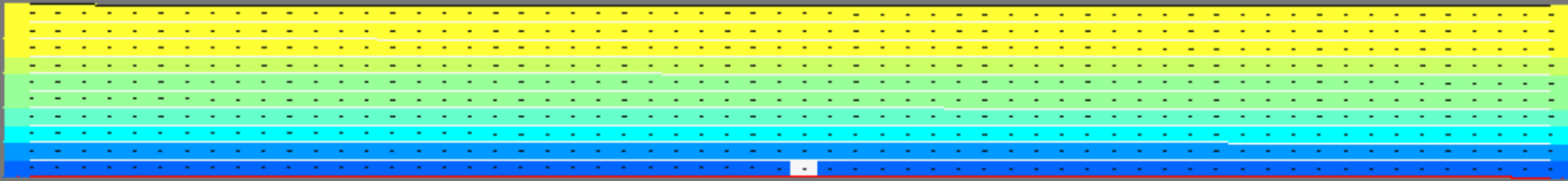
Constant eddy viscosity Elder: $Q = 38.667 \text{ m}^3/\text{s}$

($47.434 \text{ m}^3/\text{s}$)



Constant eddy viscosity Elder*2/3: $Q = 40.809 \text{ m}^3/\text{s}$

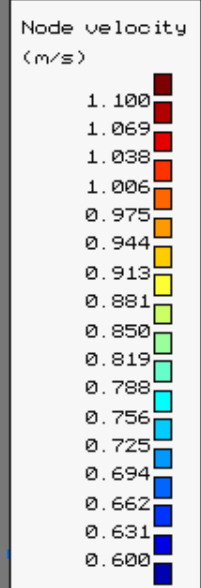
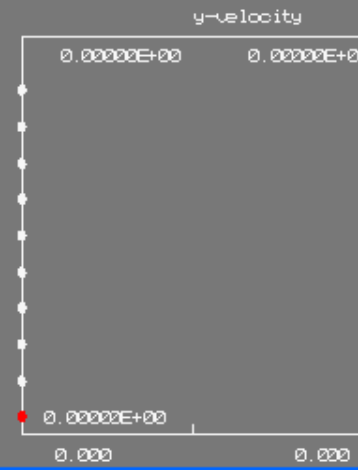
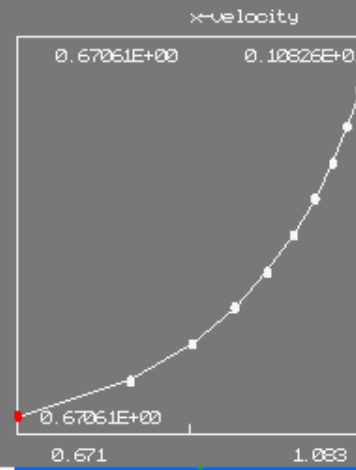
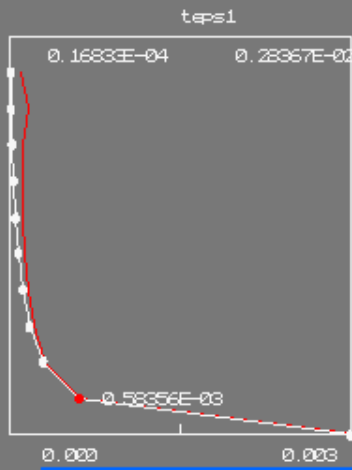
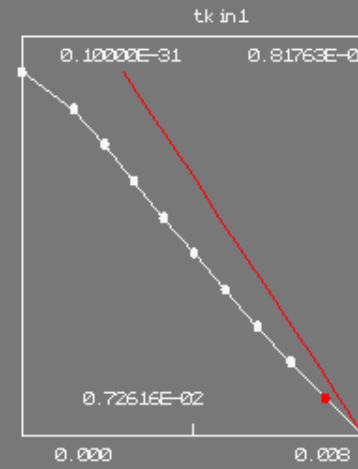
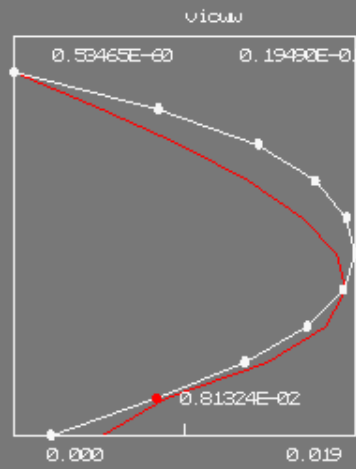
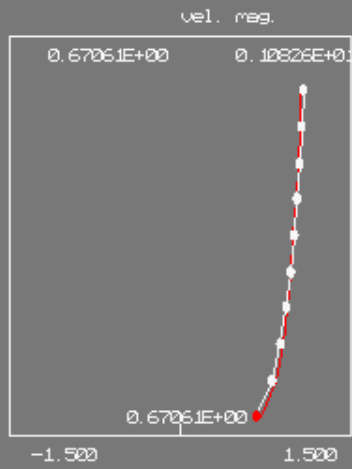
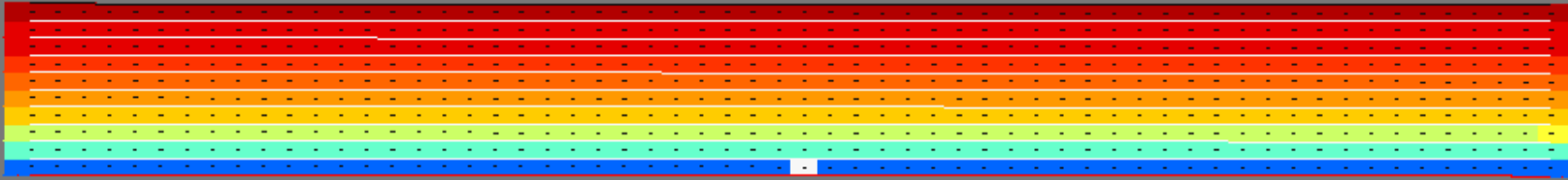
(47.434 m^3/s)



K-epsilon sigma 10 layers : 47.466 m3/s

(47.434 m3/s)

0.000E+00
2159 #itsol: 0
slope



47.466 m3/s

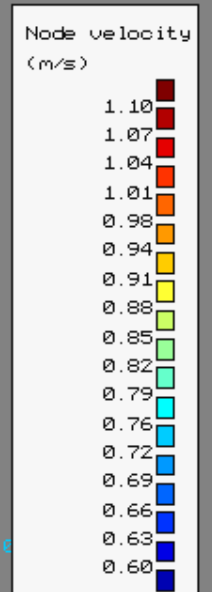
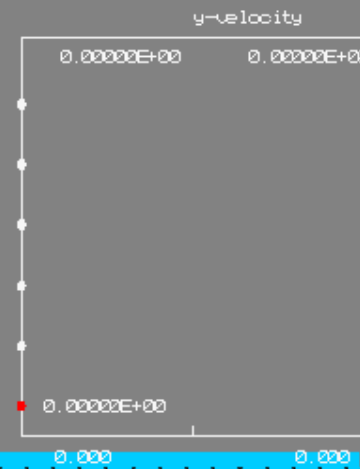
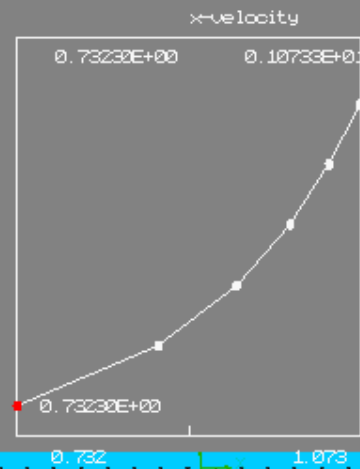
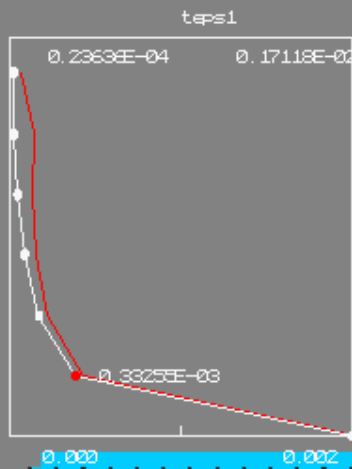
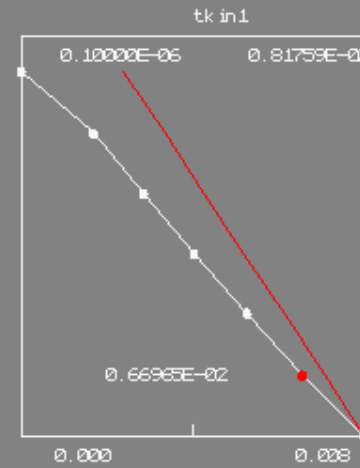
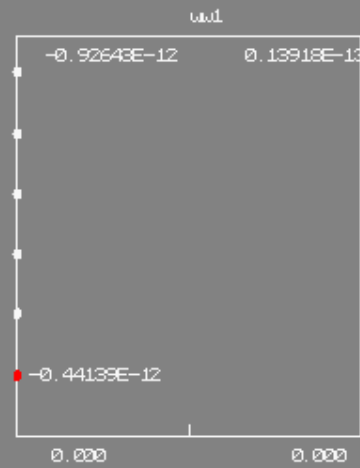
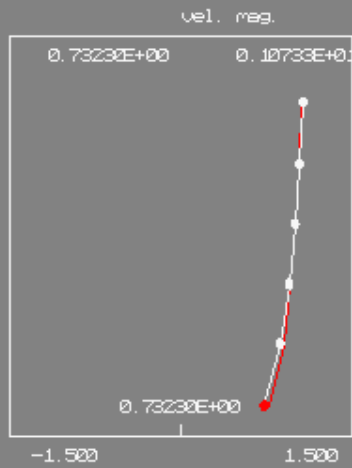
X

K-epsilon sigma 6 layers : 47.290 m3/s

(47.434 m3/s)

000000E+00 Samtot:0.00000000E+00
: 4374 #itsol: 0

#ndx: 62 #Inx: 61 #kx: 6 #CG: 0 #Gauss: 62 #slit: 0 iad: 30 5 runid: slope



47.290 m3/s

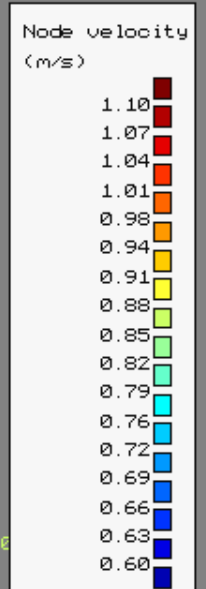
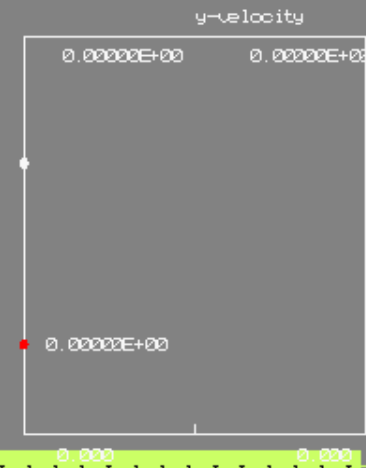
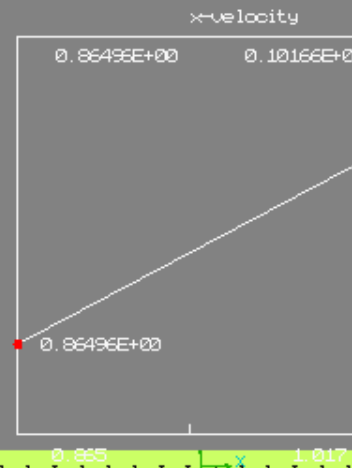
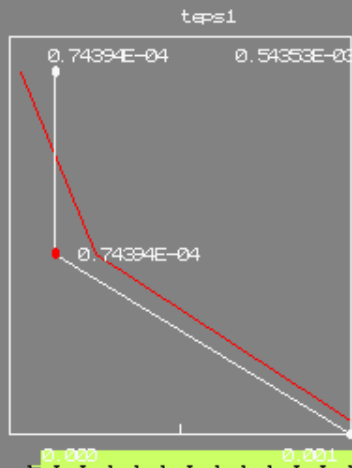
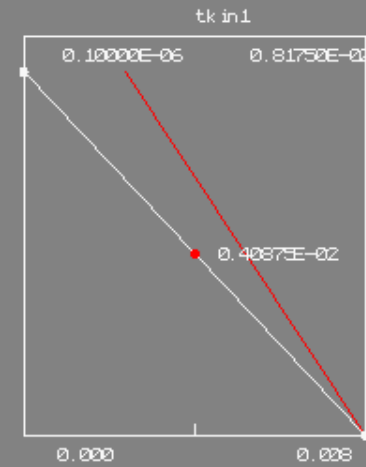
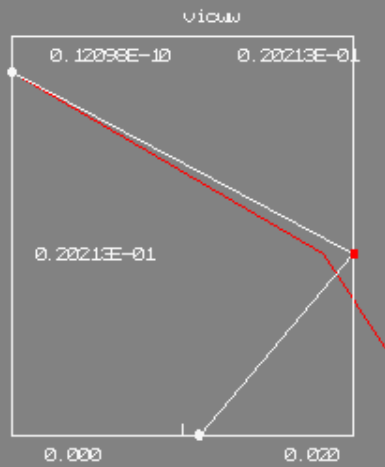
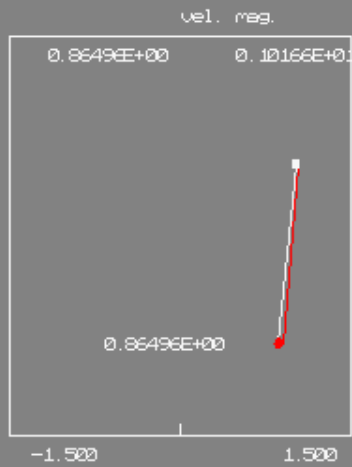
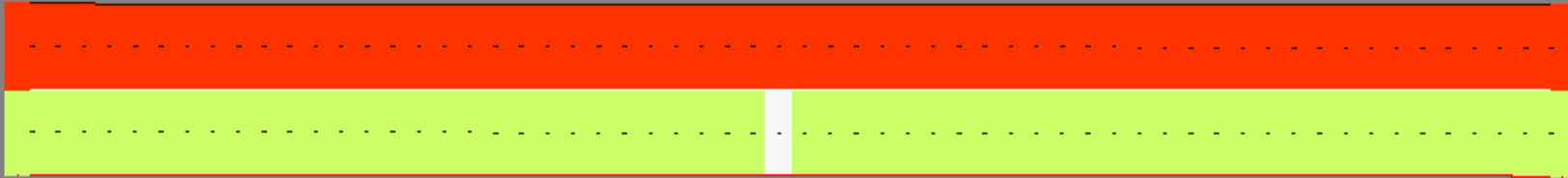
X

K-epsilon sigma 2 layers : 47.040 m3/s

(47.434 m3/s)

0.000000E+00 Samtot:0.00000000E+00
4065 #itsol: 0

#ndx: 62 #Inx: 61 #krm : 2 #CG: 0 #Gauss: 62 #slit: 0 iad: 30 5 runid: slope

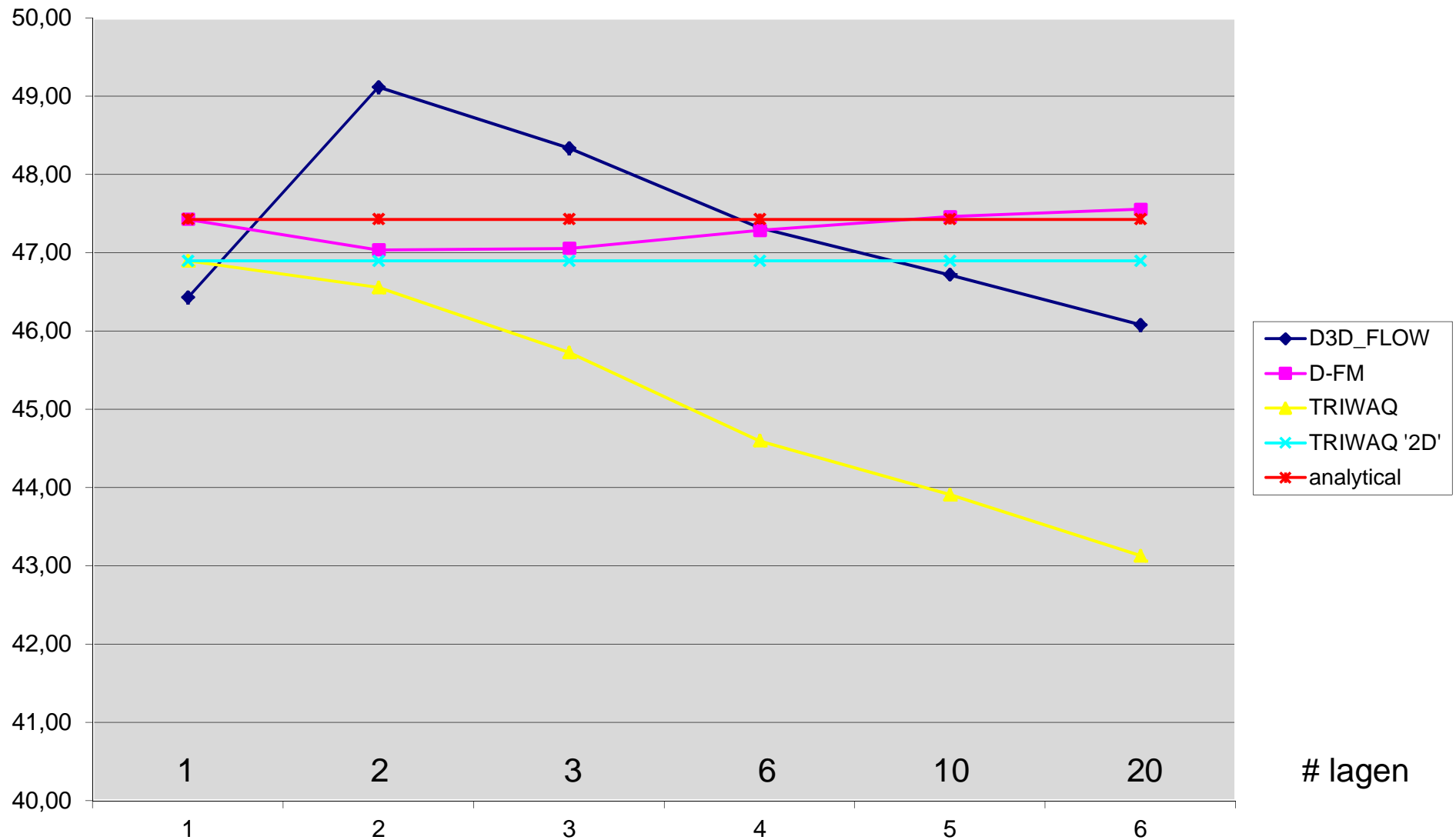


47.040 m3/s

X

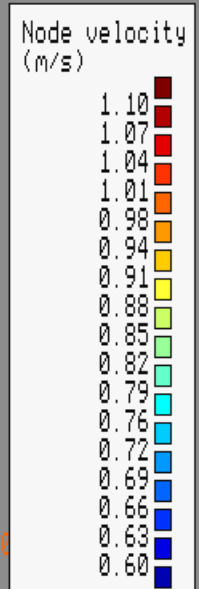
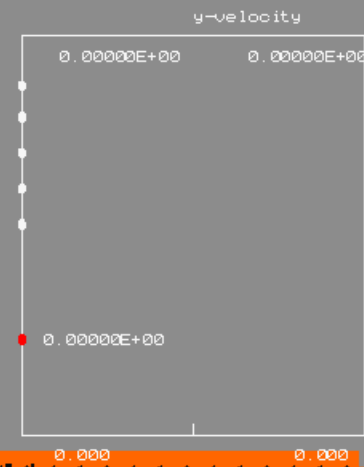
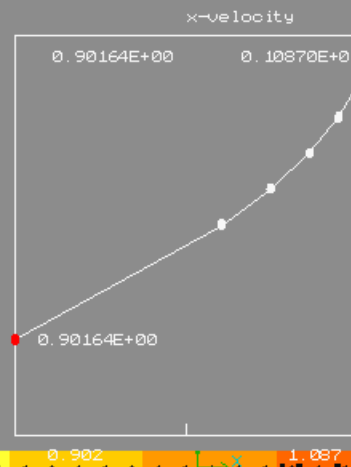
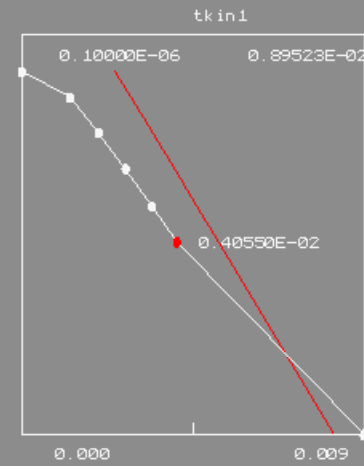
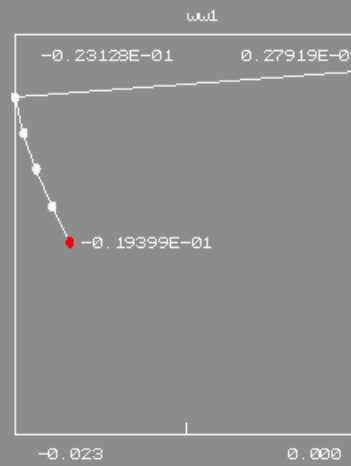
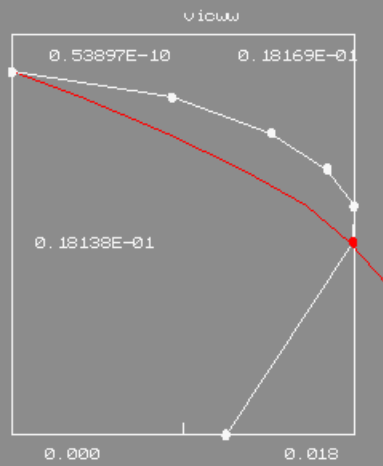
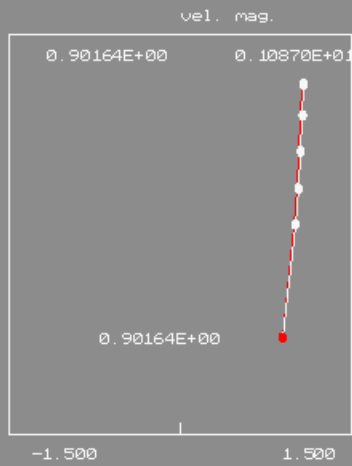
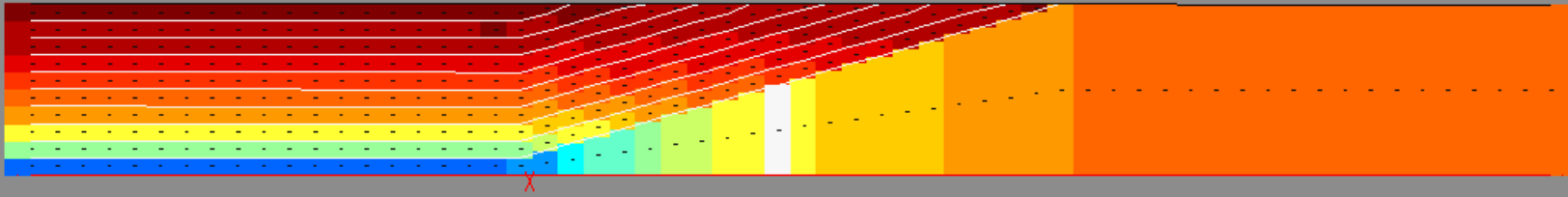
K-eps : Debiet - # lagen D3D, DFM, TRIWAQ

Discharge m³/s



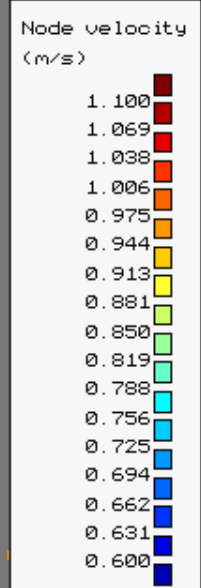
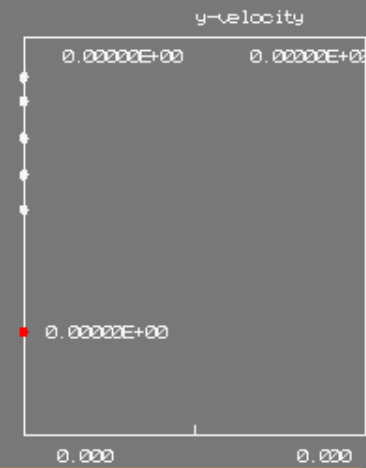
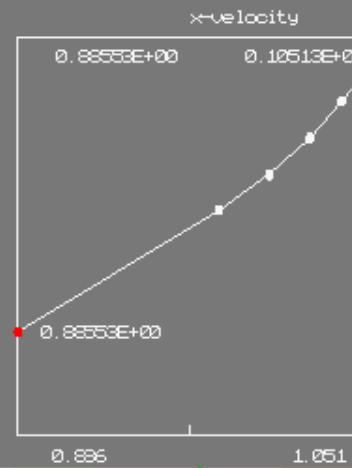
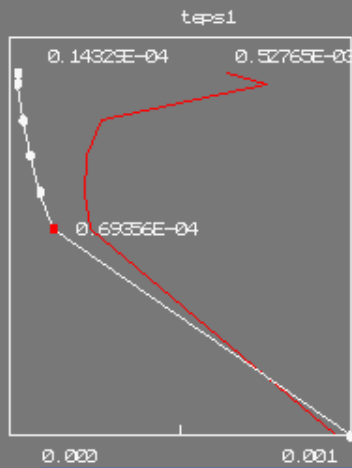
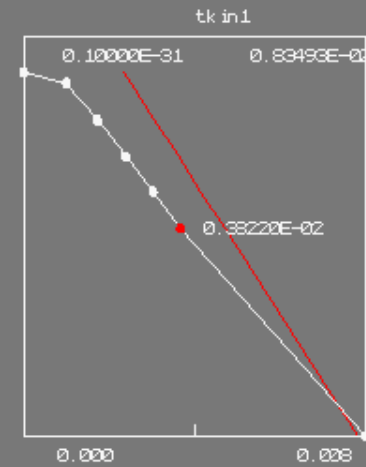
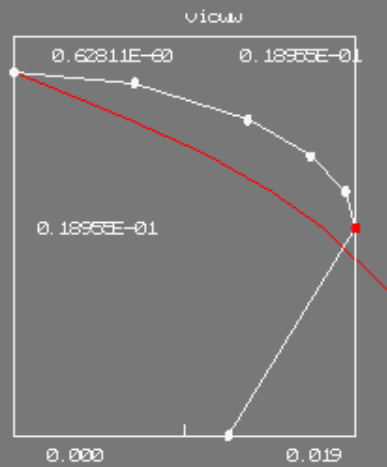
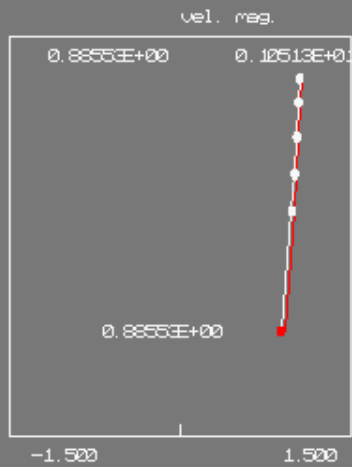
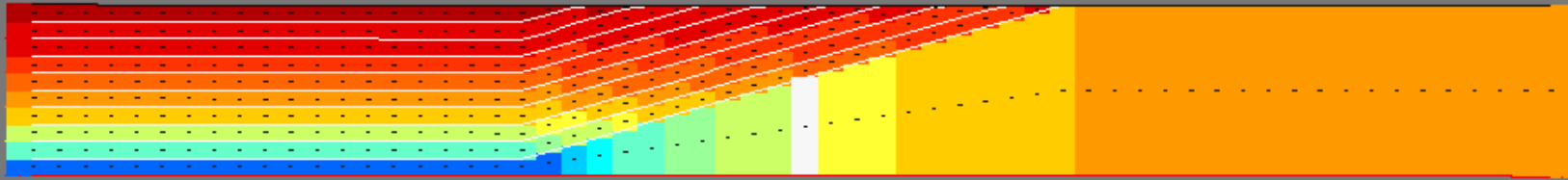
K-epsilon ustar layer integral mixed layers, : Q = 48.878 m³/s (47.434 m³/s)

#ndx: 6Z #Inx: 61 #kmx: 10 #CG: 0 #Gauss: 6Z #slit: 0 rad: 30 5 runid: slope



48.878 m³/s

K-epsilon ustar layer integral mixed layers, noadv : Q = 47.287 m³/s (47.434 m³/s

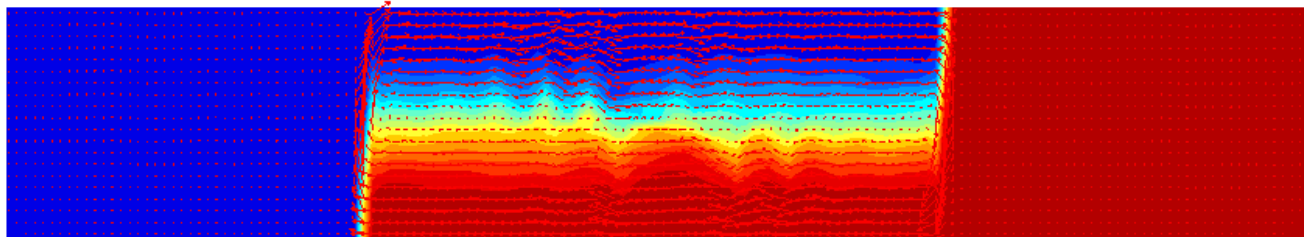
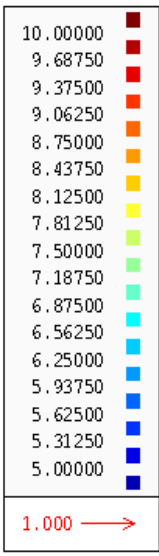


X

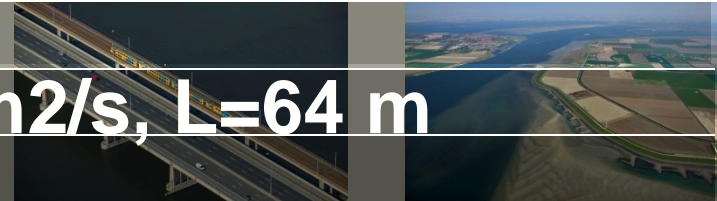
47.287 m³/s

Lock exchange Delft3D $\nu=0.01 \text{ m}^2/\text{s}$, $L=50 \text{ m}$

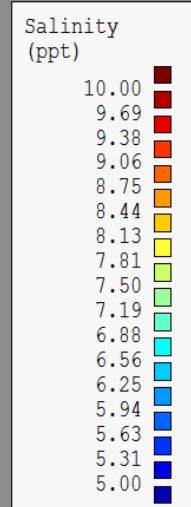
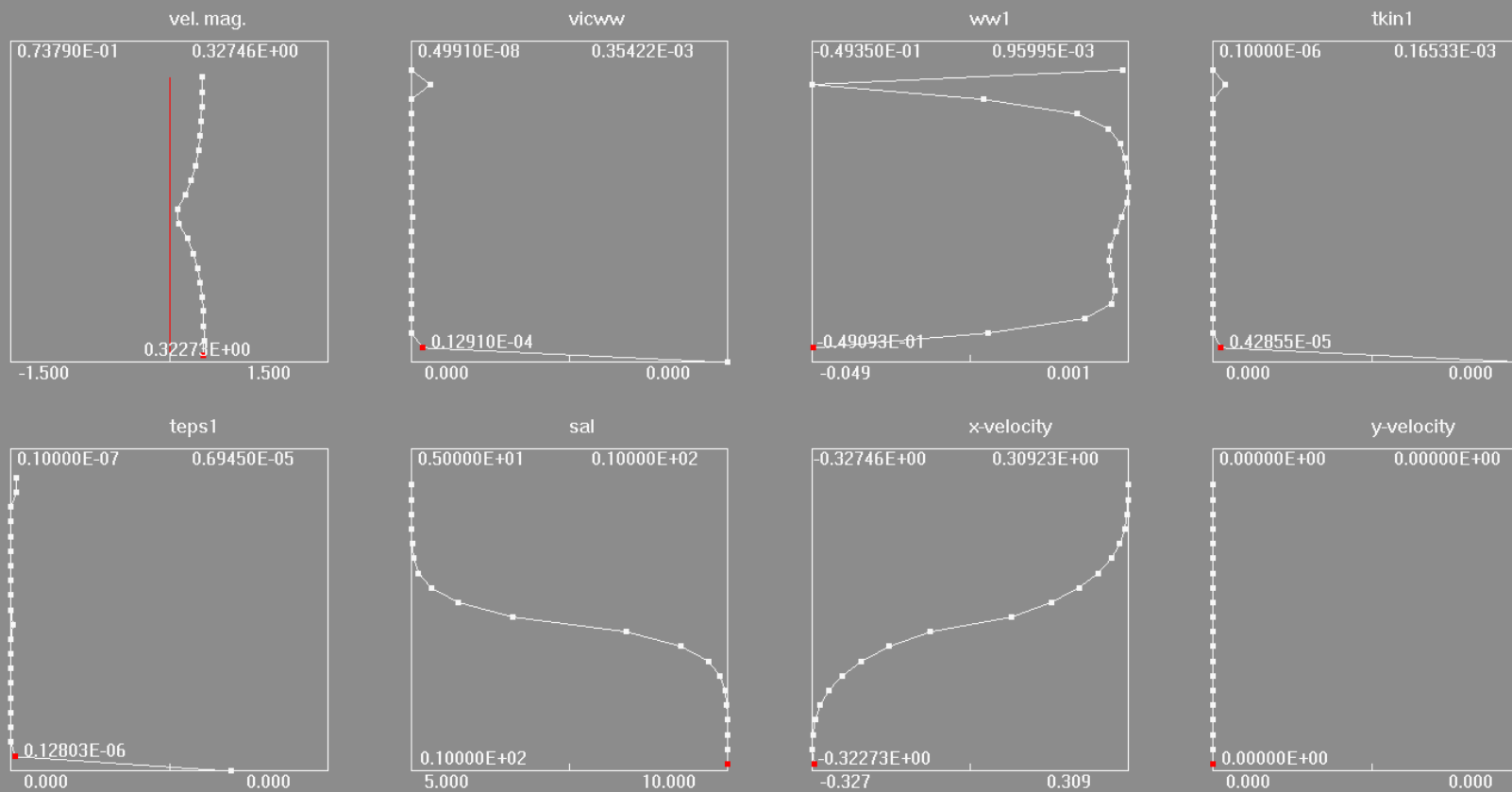
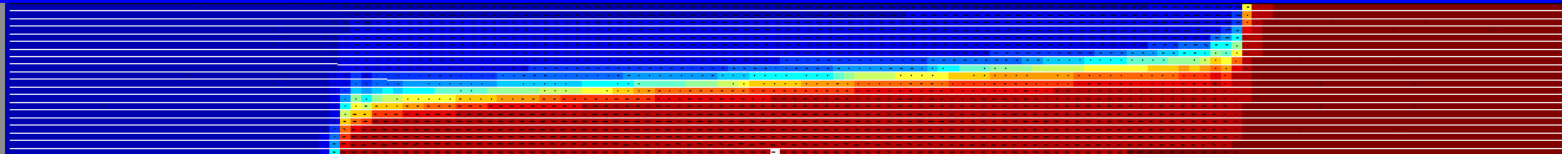
Date : 1998-02-10
Time : 00:02:00
runid : loc
Cross-sect. at N: 2
Salinity

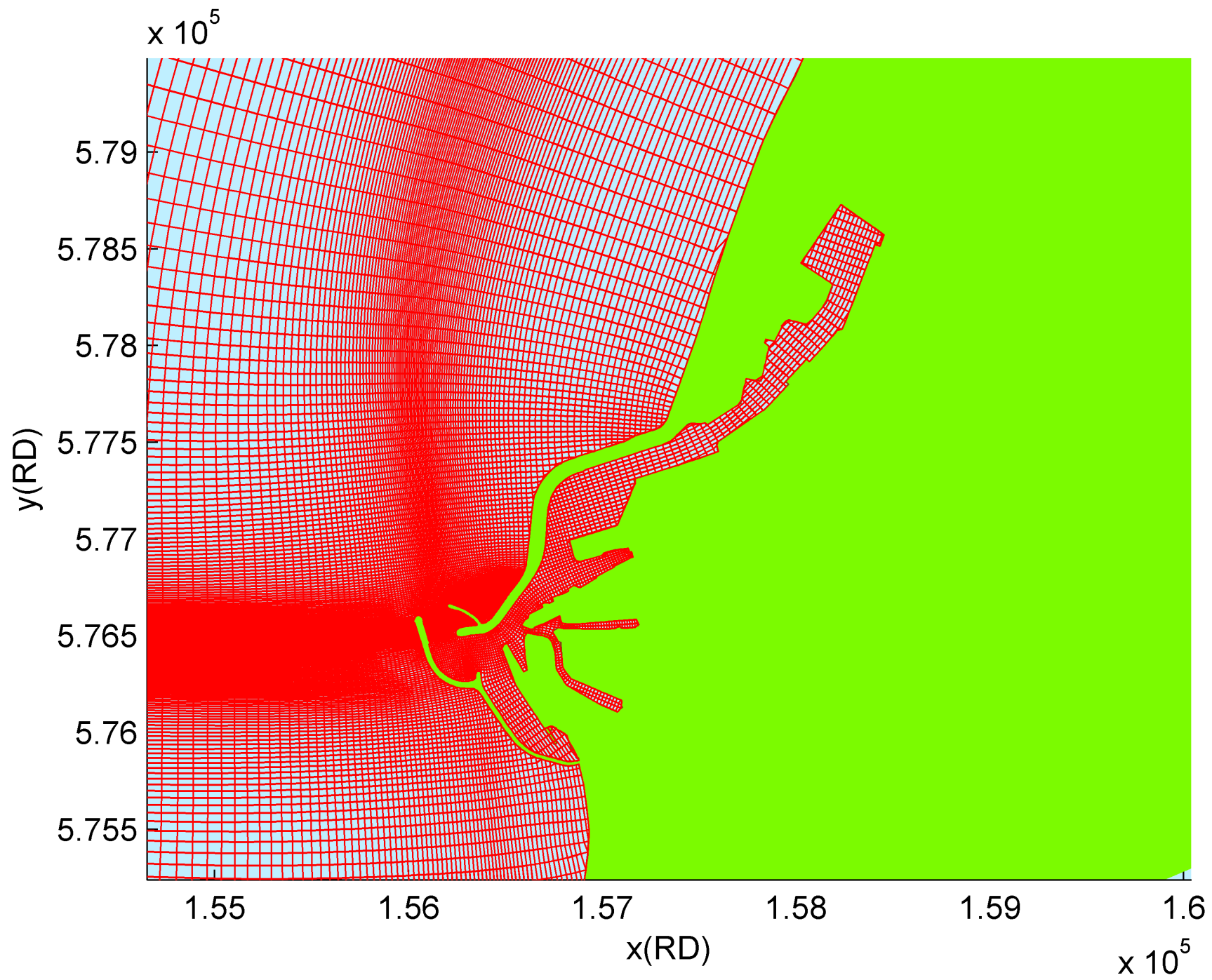


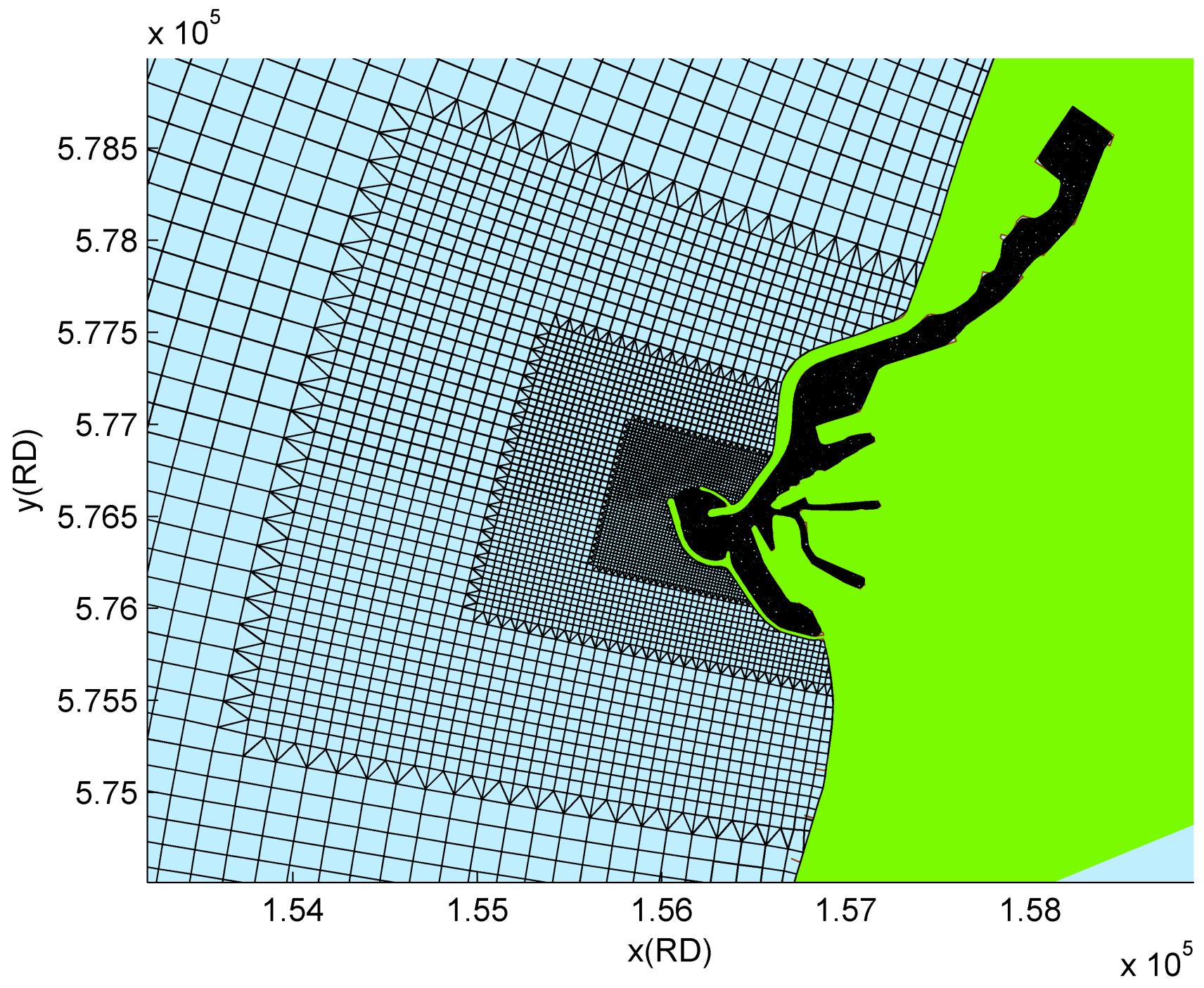
Lock exchange DFM, $v=0.01 \text{ m}^2/\text{s}$, $L=64 \text{ m}$

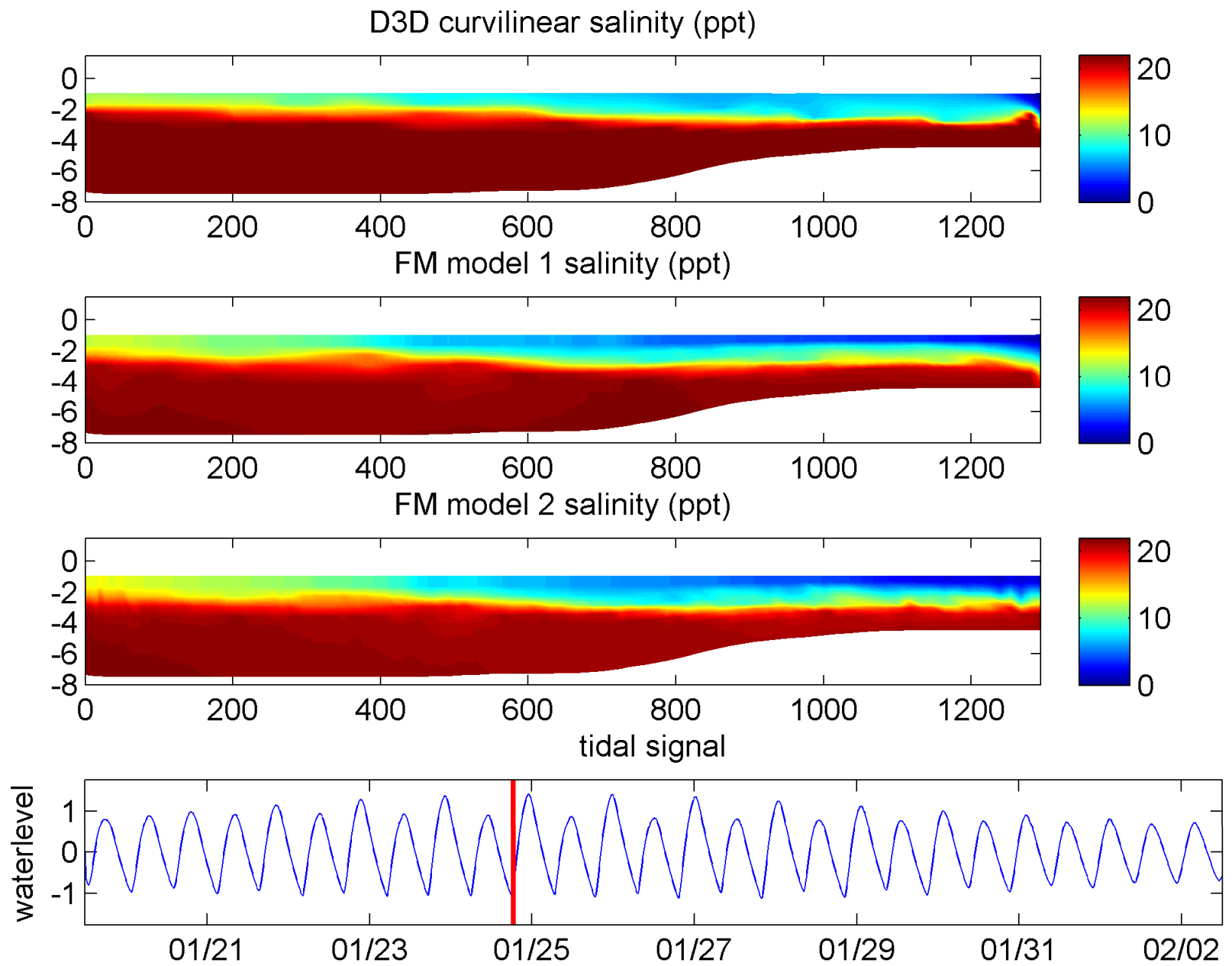


20010101_000200 dt: 0.750 Avg.dt: 0.686 CPU/step: 0.002 Tot: 0.3 Sol/Rest:.76E-02 Samer: -.25465852E-10 Samtot:0.84375000E+04
 k/nplot: 1 74 znod(nn): 0.99999742E+01 Voll: 0.56250000E+02 Vler: 0.92370556E-13 #setb: 0 #dt: 175 #itsol: 0
 #ndx: 150 #lnx: 149 #kmx: 20 #CG: 0 #Gauss: 150 #slit: 0 iad: 34 45 runid: locxx

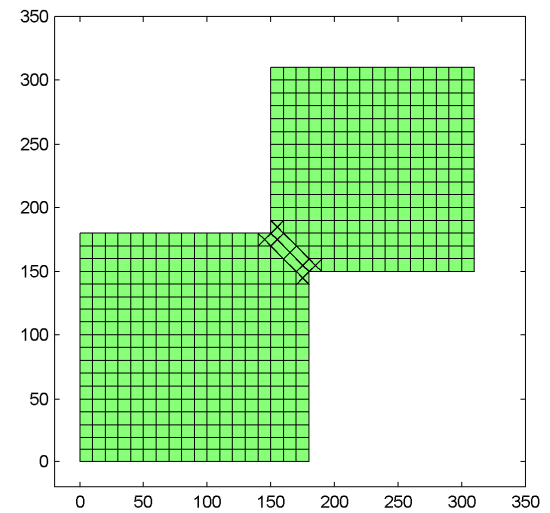
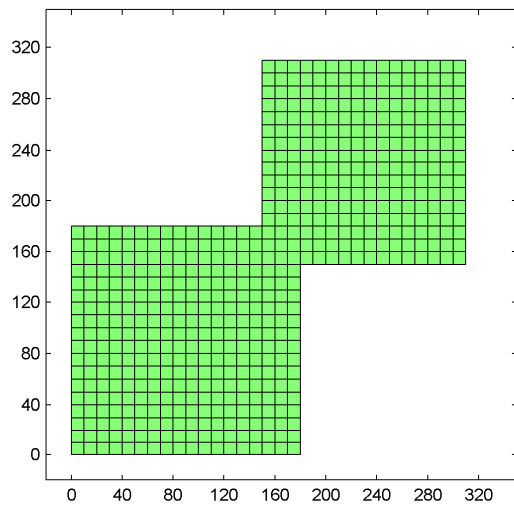
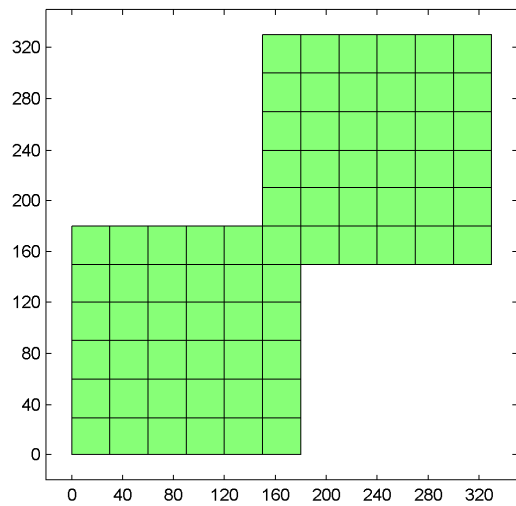
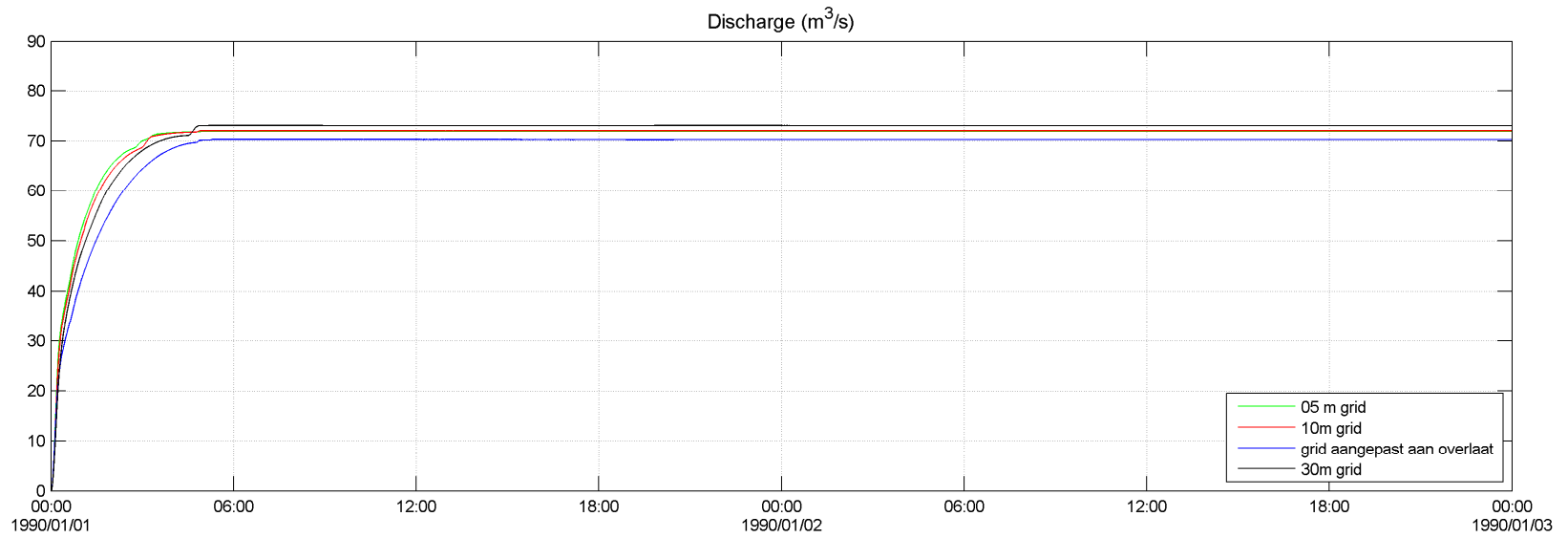
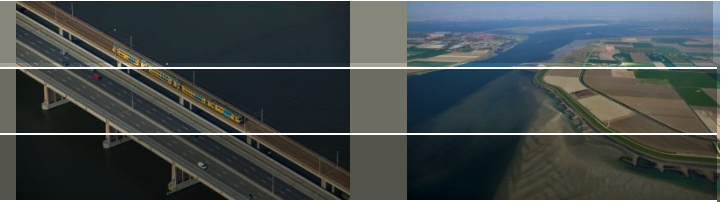








Subgrid weir



20111202_083300 dt: 6.803 Avg.dt: 2.609 CPU/step: 1.624 Tot: 37.9 Sol/Rest: 0.032 Same: -.11046404E+04
 k/np/plot: 1 65838 znod(nn): 0.31364967E+02 Vol1: 0.51187481E+11 U1er: -.13179675E-03 #setb: 0 #dt: 23 #itsol: 9
 #ndx: 175872 #lnx: 342702 #krx: 12 #CG: 68020 #Gauss: 70201 #slit: 0 iad: 3444 runid: zee6

